



NEH7110

Inductorless energy harvesting PMIC with battery protection, LDO and USB charging

Rev. 1 — 17 December 2024

Product data sheet

1. General description

The NEH7110 is a high-performance power management IC (PMIC) for energy harvesting solutions in low-power applications. It has a rich set of auxiliary features, such as storage element protection, USB charging and LDO / load switch.

The NEH7110 is optimized to harvest energy from light sources (from a wide range of indoor and outdoor PV cells). Other energy sources can also be used, such as kinetic (movement, vibrations), thermal variation and electromagnetic, but might need external auxiliary components. The NEH7110 gathers energy from a suitable harvester to charge a storage element, such as a rechargeable battery or a supercapacitor.

Nexperia's advanced maximum power point tracking (MPPT) uses an embedded hill-climbing algorithm to deliver maximum power to the storage element. The MPPT is compatible with any suitable harvester, and optimizes efficiency as frequent as every second for excellent performance in rapidly changing harvesting conditions.

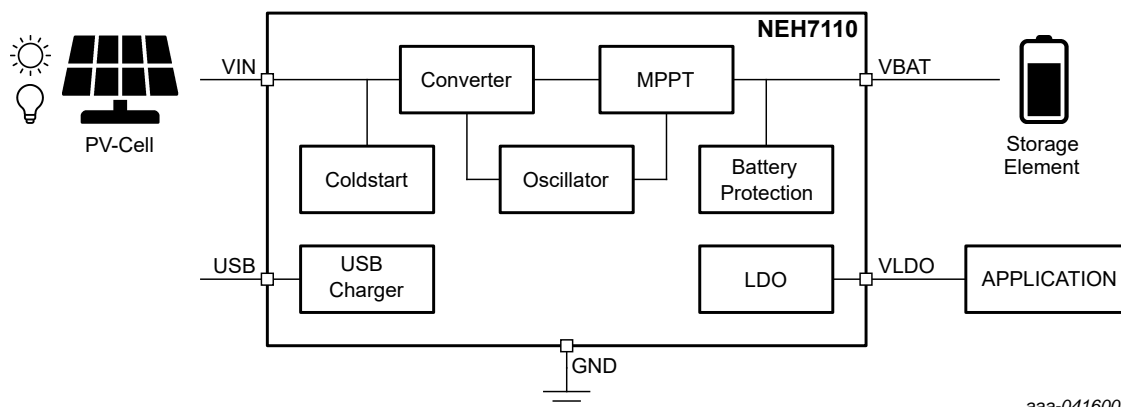
The NEH7110 is available in 28-lead, 4 mm x 4 mm HVQFN28 package.

2. Features and benefits

- Harvesting power range: 15 μ W to 50 mW
- Ultra-fast MPPT interval
- Battery protection features:
 - Over-voltage protection (OVP)
 - Low-voltage detection (LVD)
 - Over-current protection (OCP)
- USB charging up to 200 mA
- LDO with configurable output voltage
- Configurable via hard-coding
- Coldstart, supporting "battery-less" design
- Small BOM with no inductor required
- Suitable for batteries, supercapacitors and hybrid capacitors

3. Applications

- Smart remote controls: TV, gaming, AV control, key-fob
- Wireless PC devices: keyboard, mouse, headphones
- Industrial sensors: electronic shelf labels, asset trackers and beacons
- Tire pressure sensors
- Wearable devices: watch, body band and health devices



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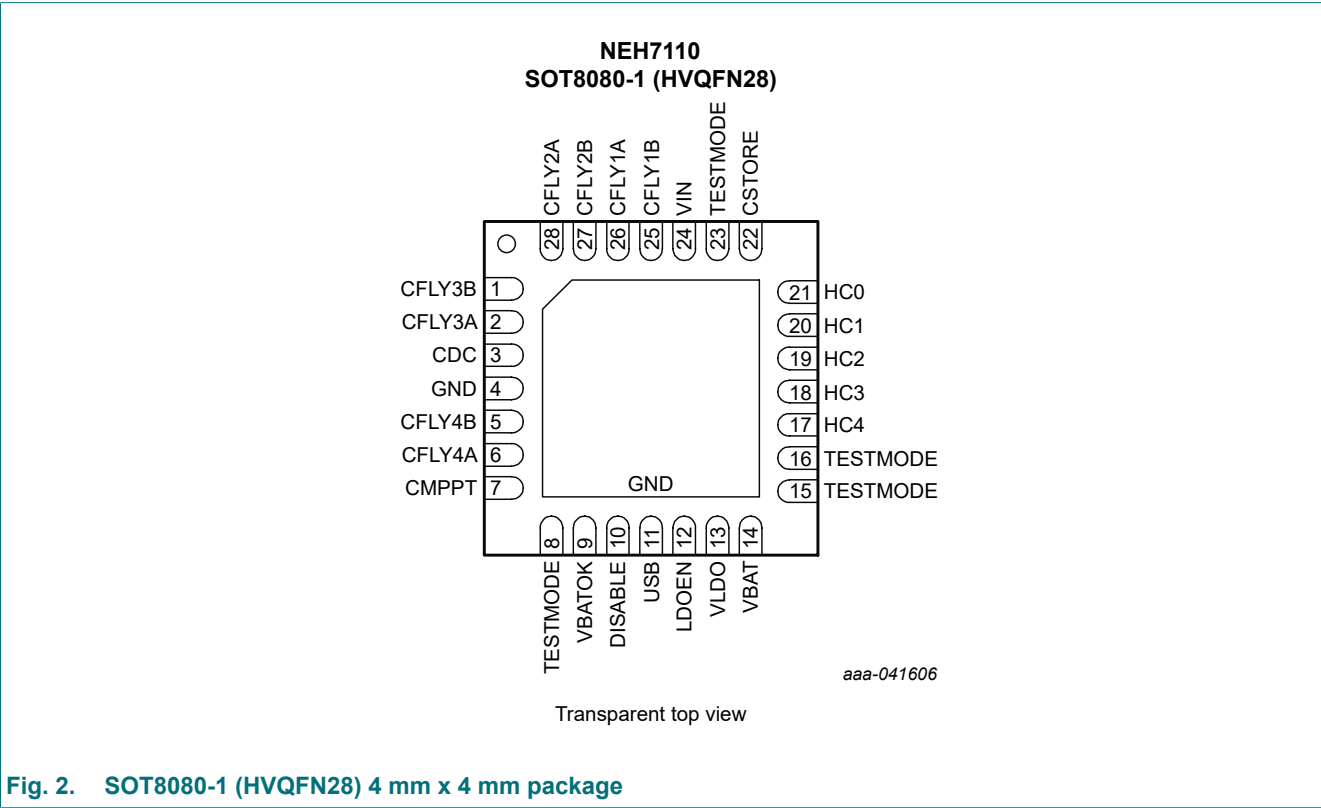
Fig. 1. NEH7110 typical solar energy harvesting system

4. Ordering information

Type number	Package			
	Temperature range	Name	Description	Version
NEH7110BU	-40 °C to 85 °C	HVQFN28	plastic, leadless thermal enhanced very thin quad flat package; 28 terminals;0.4 mm pitch; 4 mm x 4 mm x 0.85 mm body	SOT8080-1

5. Pinning information

5.1. Pinning configuration



5.2. Pinning description

Table 2. Pinning description

Pin	Symbol	Description
1	CFLY3B	flying-capacitor terminal B, 3rd stage
2	CFLY3A	flying-capacitor terminal A, 3rd stage
3	CDC	boost converter filter capacitor
4	GND	ground
5	CFLY4B	flying-capacitor terminal B, 4th stage
6	CFLY4A	flying-capacitor terminal A, 4th stage
7	CMPPT	filter capacitor for MPPT
8	TESTMODE	reserved; should be left floating
9	VBATOK	indicates if battery voltage is above configured LVD level
10	DISABLE	active high. Disable mode sets the device in low-power consumption. Connect to GND to enable, connect to V _{BAT} to disable.
11	USB	USB 5V input for charging storage element connected to V _{BAT} .
12	LDOEN	LDO enable, active high. Connect to V _{BAT} level to enable. Connect to GND to disable
13	VLDO	LDO output. LDO input is internally connected to VBAT. Connect to application load.
14	VBAT	output of the energy harvester and power supply for PMIC. Connect storage element to this pin.
15	TESTMODE	reserved; should be connected to GND
16	TESTMODE	reserved; should be connected to GND
17	HC4	hard-code bit [4]. Connect to GND for a logic low, to CSTORE for a logic high
18	HC3	hard-code bit [3]. Connect to GND for a logic low, to CSTORE for a logic high
19	HC2	hard-code bit [2]. Connect to GND for a logic low, to CSTORE for a logic high
20	HC1	hard-code bit [1]. Connect to GND for a logic low, to CSTORE for a logic high
21	HC0	hard-code bit [0]. Connect to GND for a logic low, to CSTORE for a logic high
22	CSTORE	internal supply pin
23	TESTMODE	reserved; should be left either floating or connected to GND
24	VIN	input for connecting a harvester
25	CFLY1B	flying-capacitor terminal B, 1st stage
26	CFLY1A	flying-capacitor terminal A, 1st stage
27	CFLY2B	flying-capacitor terminal B, 2nd stage
28	CFLY2A	flying-capacitor terminal A, 2nd stage
PAD	GND	ground pad, should be connected to ground plane with vias

6. Specifications

6.1. Absolute maximum ratings

Table 3. Absolute maximum ratings

In accordance with the Absolute Maximum Rating System (IEC 60134). Voltages are referenced to GND (ground = 0 V).

Symbol	Parameter	Conditions	Min	Max	Unit
V _{PC}	power converter pins: CFLY1x, CFLY2x		-0.3	2.0	V
	power converter pins: CFLY3x, CFLY4x, CDC, CMPPT, CSTORE		-0.3	5.5	V
V _{CONFIG}	configuration pins: DISABLE, LDOEN, HCx		-0.3	5.5	V
V _{IN}	input pin: VIN	using bench power supply with low series resistance	-0.3	2.0	V
		using PV-cell or current-limited source	-0.3	5.5	V
V _{POWER}	power pins: VBAT, USB		-0.3	5.5	V
I _{IN}	input current (VIN pin)		-	140	mA
T _j	junction temperature		-50	+125	°C
T _{stg}	storage temperature		-65	+150	°C

6.2. ESD ratings

Table 4. ESD ratings

Symbol	Parameter	Conditions	Value	Unit
V _{ESD}	electrostatic discharge voltage	HBM: ANSI/ESDA/JEDEC JS-001	± 2000	V
		CDM: ANSI/ESDA/JEDEC JS-002	± 500	V

6.3. Recommended operating conditions

Table 5. Recommended operating conditions

Symbol	Parameter	Conditions	Min	Typ	Max	Unit
V _{BAT}	battery voltage		0	-	4.5	V
T _{amb}	ambient temperature		-40	-	+85	°C

6.4. Thermal information

Table 6. Thermal characteristics

Symbol	Parameter	SOT8 080-1	Unit
R _{θ(ja)}	junction-to-ambient thermal resistance	57.8	°C/W
R _{θ(jc)}	junction-to-case (top) thermal resistance	73.4	°C/W
Ψ _(jt)	junction-to-case (top) thermal characterization parameter	25.1	°C/W

6.5. Electrical characteristics

Table 7. Electrical characteristics

$V_{BAT} = 3.7\text{ V}$. Typical values specified at $T_{amb} = 25\text{ }^{\circ}\text{C}$, Min and Max values specified at $T_{amb} = -40\text{ }^{\circ}\text{C}$ to $85\text{ }^{\circ}\text{C}$. Voltages are referenced to GND (ground = 0 V). V_{MPP} represents the maximum power point voltage at V_{IN} .

Symbol	Parameter	Conditions	Min	Typ	Max	Unit
Supplies and start-up						
V_{BAT}	battery voltage	To start device with input power on V_{IN}	0		4.5	V
		Minimum voltage to start device without input power on V_{IN}	-	2.9	3.6	V
		Minimum voltage required to keep device running after start and without power on V_{IN}	-	2	-	V
$I_{DISABLE}$	disable mode current	$V_{DISABLE} = V_{BAT}$	-	13	150	nA
I_Q	quiescent current (LDO disabled)	no input power, V_{IN} is floating; LDO disabled	-	1.5	5	μA
$I_{Q(LDO)}$	quiescent current (LDO enabled)	no input power, V_{IN} is floating; LDO enabled	-	2.1	6.5	μA
t_{start}	start-up time	time from applying V_{BAT} to rising edge of $VBATOK$; No input power on V_{IN}	-	720	-	ms
Power converter						
η	nominal efficiency	$V_{MPP} = 2\text{ V}$	-	94	-	%
		$V_{MPP} = 1\text{ V}$	-	90	-	%
		$V_{MPP} = 0.5\text{ V}$	-	85	-	%
		$V_{MPP} = 0.25\text{ V}$	-	75	-	%
$P_{IN(low)}$	input power range, low end	efficiency = 70%; $V_{MPP} = 2\text{ V}$	-	65	-	μW
		efficiency = 60%; $V_{MPP} = 1\text{ V}$	-	55	-	μW
		efficiency = 50%; $V_{MPP} = 0.5\text{ V}$	-	45	-	μW
		efficiency = 40%; $V_{MPP} = 0.25\text{ V}$	-	53	-	μW
$P_{IN(high)}$	input power range, high end	efficiency = 70%; $V_{MPP} = 2\text{ V}$	-	69	-	mW
		efficiency = 60%; $V_{MPP} = 1\text{ V}$	-	52	-	mW
		efficiency = 50%; $V_{MPP} = 0.5\text{ V}$	-	23	-	mW
		efficiency = 40%; $V_{MPP} = 0.25\text{ V}$	-	10	-	mW
$V_{IN(min)}$	minimum input voltage	Main converter active, cold start inactive; efficiency $\geq 40\%$. $I_{IN} = 1\text{ mA}$	-	0.23	-	V
$f_{CONV(low)}$	frequency at low-end power		-	30	-	kHz
$f_{CONV(high)}$	frequency at high-end power		-	1.1	-	MHz
t_{MPPT}	MPPT interval		-	1	-	sec
$t_{MPPT(acc)}$	MPPT interval inaccuracy		-	10	-	%
Cold start						
$V_{IN(CS)}$	minimum V_{IN} cold start voltage	$P_{IN} > 12\text{ }\mu\text{W}$	-	270	-	mV
$P_{IN_CS(min)}$	minimum cold start input power	$V_{IN} = 270\text{ mV}$	-	12	-	μW

Inductorless energy harvesting PMIC with battery protection, LDO and USB charging

Symbol	Parameter	Conditions	Min	Typ	Max	Unit
Battery protection						
V _{BAT_OVP}	over-voltage protection (OVP)	Set via hardcoding (see Table 8)	3.1	-	4.2	V
V _{BAT_LVD}	low-voltage detection (LVD)	Set via hardcoding (see Table 8)	2.2	-	3.5	V
V _{BAT(acc)}	over-voltage protection (OVP) and low-voltage detection (LVD) threshold inaccuracy		-	-1	-	%
V _{LVD(hys)}	low-voltage detection (LVD) hysteresis	Voltage difference between LVD falling and rising threshold	-	150	-	mV
USB features						
USB_OVP	USB over-voltage	Set via hardcoding (see Table 8)	3.1	-	4.2	V
USB_OCP	USB over-current	Set via hardcoding (see Table 8)	2	-	200	mA
I _{BAT}	storage element charging current via USB		-	0.8 × setting	-	mA
V _{BAT(acc)}	storage element over-voltage inaccuracy via USB	5 V on USB pin	-	-1	-	%
I _{BAT(acc)}	storage element charging current inaccuracy	5 V on USB pin; relative to 0.8 × setting	-	-6	-	%
LDO features						
V _{LDO}	LDO voltage	Set via hardcoding (see Table 8)	1.2	-	3.3	V
V _{LDO(acc)}	LDO voltage inaccuracy	I _{LDO} = 1 mA	-	-1	-	%
I _{LDO(max)}	maximum LDO output current	V _{BAT} = V _{LDO_nom} + 0.5 V; V _{BAT(min)} = 2.5 V	-	200	-	mA
V _{LDO(drop)}	LDO dropout voltage	I _{LDO} = 200mA	-	130	-	mV
t _{LDO_on}	LDO turn-on time	from LDO_EN rising edge until V _{LDO} = 95%; I _{LDO} = 200 mA; V _{LDO} = 3.3 V; V _{BAT} = 4 V	-	0.5	-	s
ΔV _{LDO(line)}	LDO line regulation	V _{LDO} inaccuracy over V _{BAT} range. I _{LDO} = 1 mA; 2.5 V < V _{BAT} < 4.5 V and V _{BAT} > V _{LDO} + 0.5 V	-	0.2	-	%
ΔI _{LDO(load)}	LDO load regulation	V _{LDO} inaccuracy over I _{LDO} range. I _{LDO} < 200 mA; V _{BAT} = V _{LDO(nom)} + 0.5 V; V _{BAT(min)} = 2.5 V	-	-1.5	-	%
Logic levels						
V _{OL_BATOK(low)}	VBATOK output logic low level	I _{sink} = 1 mA	-	-	0.2	V
V _{OH_BATOK(high)}	VBATOK output logic high level	I _{source} = 1 mA	V _{BAT} - 0.4	-	-	V
V _{IL_LDOEN(low)}	LDO enable pin (LDOEN) input logic low level		-	-	0.5	V
V _{IH_LDOEN(high)}	LDO enable pin (LDOEN) input logic high level		1	-	-	V
V _{IL_DIS(low)}	DISABLE input logic low level		-	-	0.4	V
V _{IH_DIS(high)}	DISABLE input logic high level		V _{BAT} - 0.4	-	-	V

6.6. Typical characteristics

At recommended operating conditions; $V_{BAT} = 3.7\text{ V}$; typical values are at 25°C (unless otherwise noted). V_{MPP} represents the maximum power point voltage at V_{IN} .

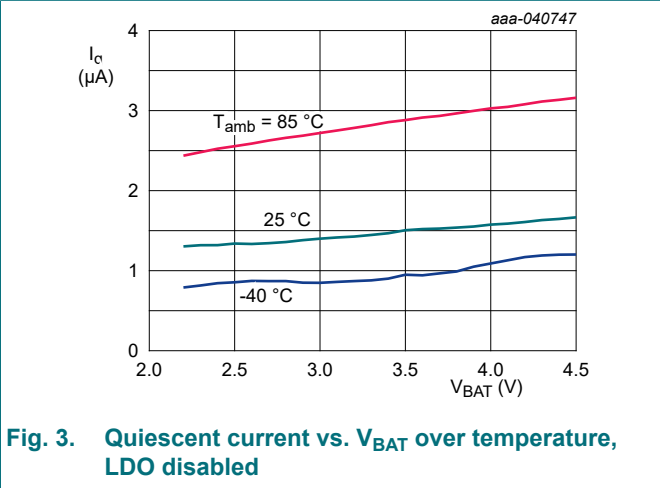


Fig. 3. Quiescent current vs. V_{BAT} over temperature, LDO disabled

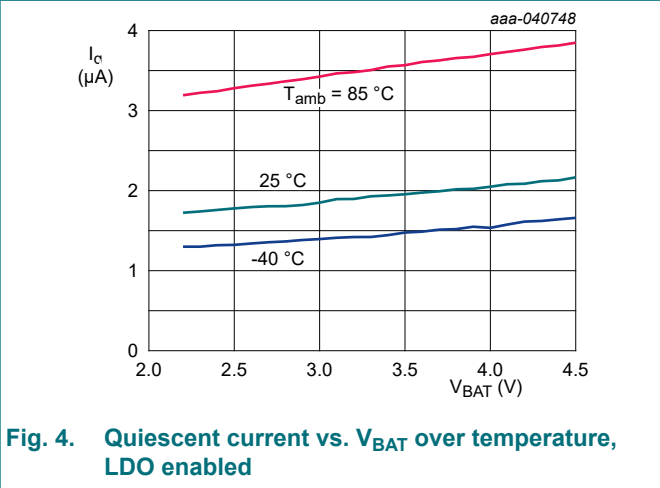


Fig. 4. Quiescent current vs. V_{BAT} over temperature, LDO enabled

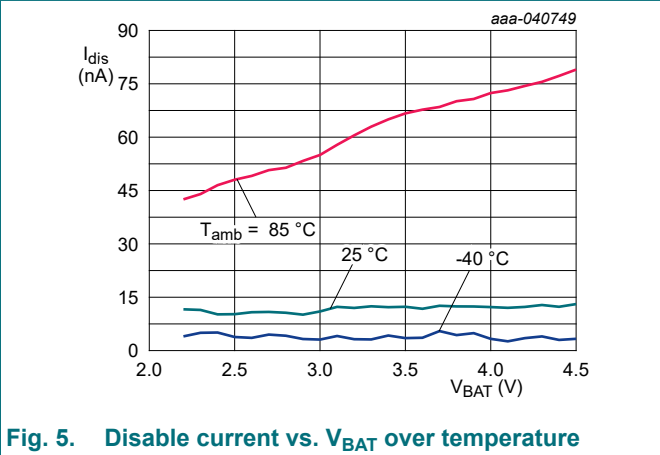


Fig. 5. Disable current vs. V_{BAT} over temperature

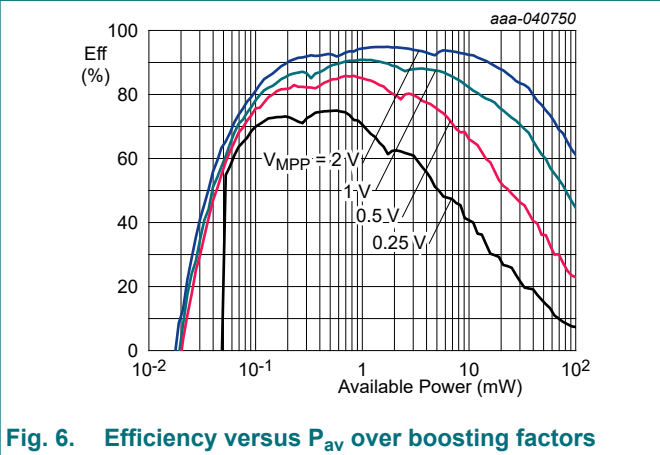


Fig. 6. Efficiency versus P_{av} over boosting factors

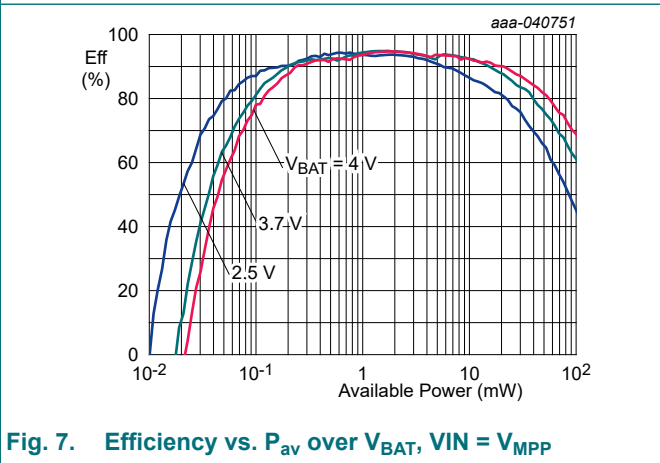


Fig. 7. Efficiency vs. P_{av} over V_{BAT} , $V_{IN} = V_{MPP}$

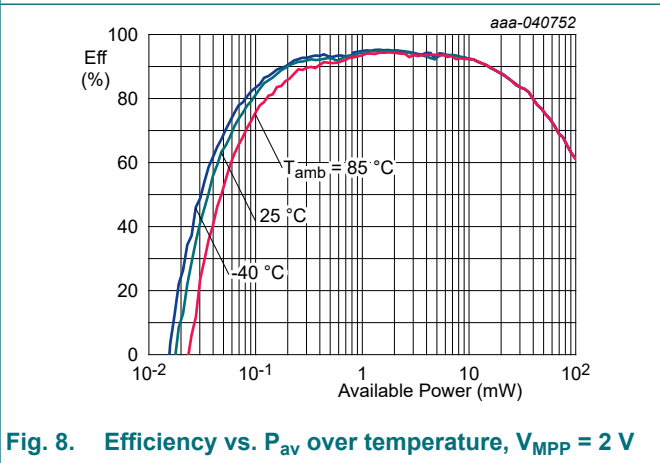


Fig. 8. Efficiency vs. P_{av} over temperature, $V_{MPP} = 2\text{ V}$

Inductorless energy harvesting PMIC with battery protection, LDO and USB charging

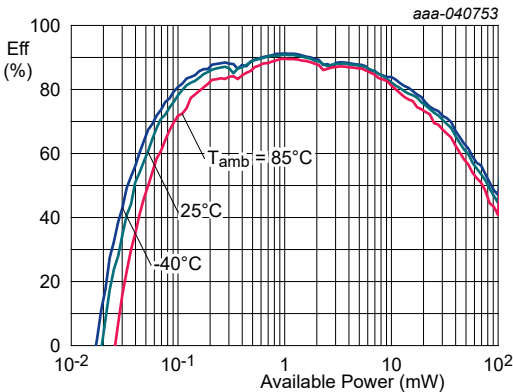


Fig. 9. Efficiency vs. P_{av} over temperature, $V_{MPP} = 1\text{ V}$

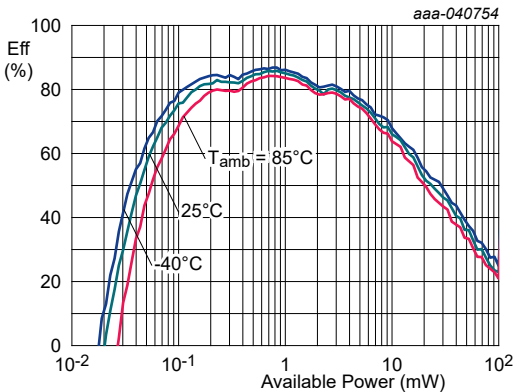


Fig. 10. Efficiency vs. P_{av} over temperature, $V_{MPP} = 0.5\text{ V}$

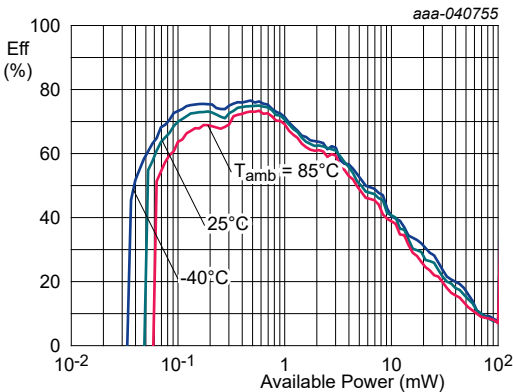


Fig. 11. Efficiency vs. P_{av} over temperature, $V_{MPP} = 0.25\text{ V}$

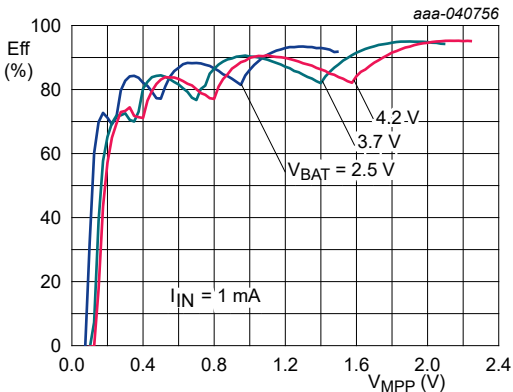


Fig. 12. Efficiency vs. V_{MPP} over V_{BAT}

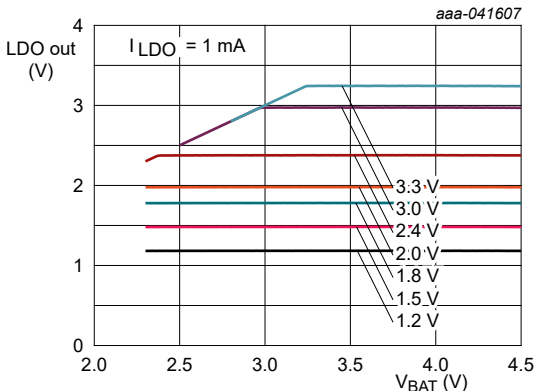


Fig. 13. V_{LDO} vs. V_{BAT} over LDO set voltages

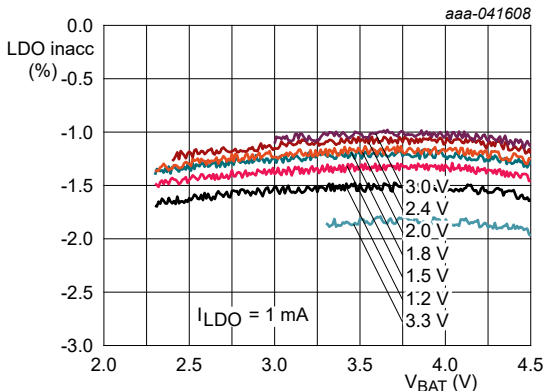


Fig. 14. LDO inaccuracy vs. V_{BAT} over LDO set voltages

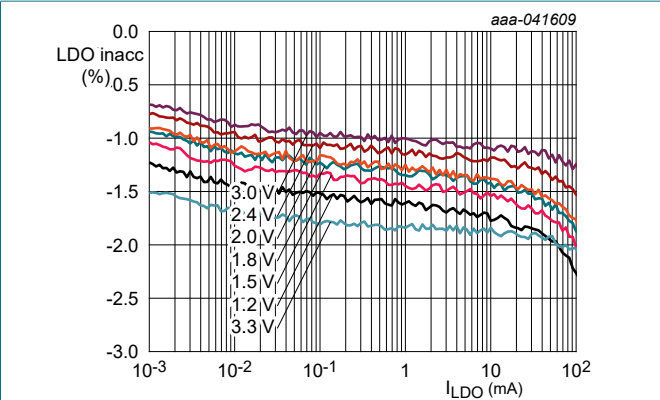


Fig. 15. LDO inaccuracy vs. I_{LDO} over LDO set voltages

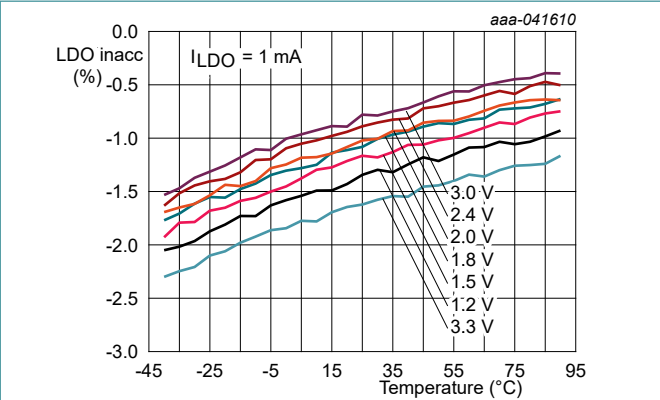


Fig. 16. LDO inaccuracy vs. temperature over LDO set voltages

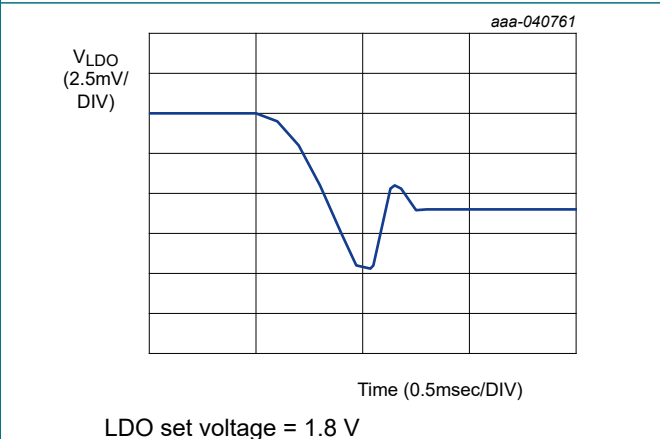


Fig. 17. LDO load transient vs. time

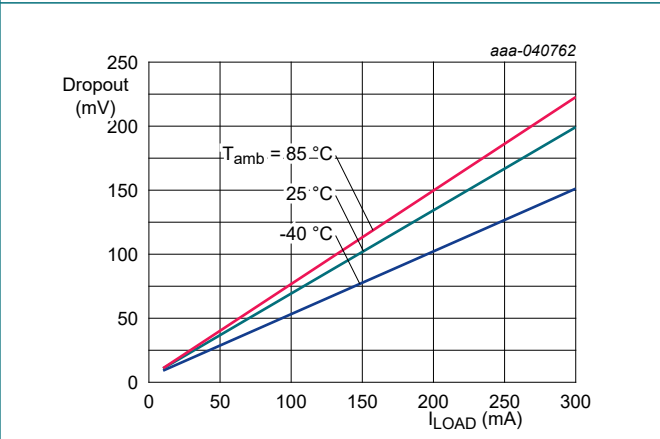


Fig. 18. LDO dropout voltage vs. I_{LDO} over temperature

7. Detailed description

7.1. Overview

NEH7110 is an energy harvesting PMIC with a wide variety of auxiliary features as shown in the block diagram in [Fig. 19](#). The converter boosts the input voltage at VIN of the NEH7110 to a level suitable to charge the storage element connected to VBAT. The MPPT block searches for the best configuration of the power converter for the highest output power. The storage element is protected against over charging by OVP circuitry. Similarly, the LVD circuit indicates when the storage element voltage is too low. In case the storage element is empty, the NEH7110 can resume operation via coldstart. As an alternative to energy harvesting, the storage element can also be charged via USB. The integrated LDO connected to VBAT provides a stable, regulated output voltage for the application. The NEH7110 can be configured via hard-code pins.

7.2. Block diagram

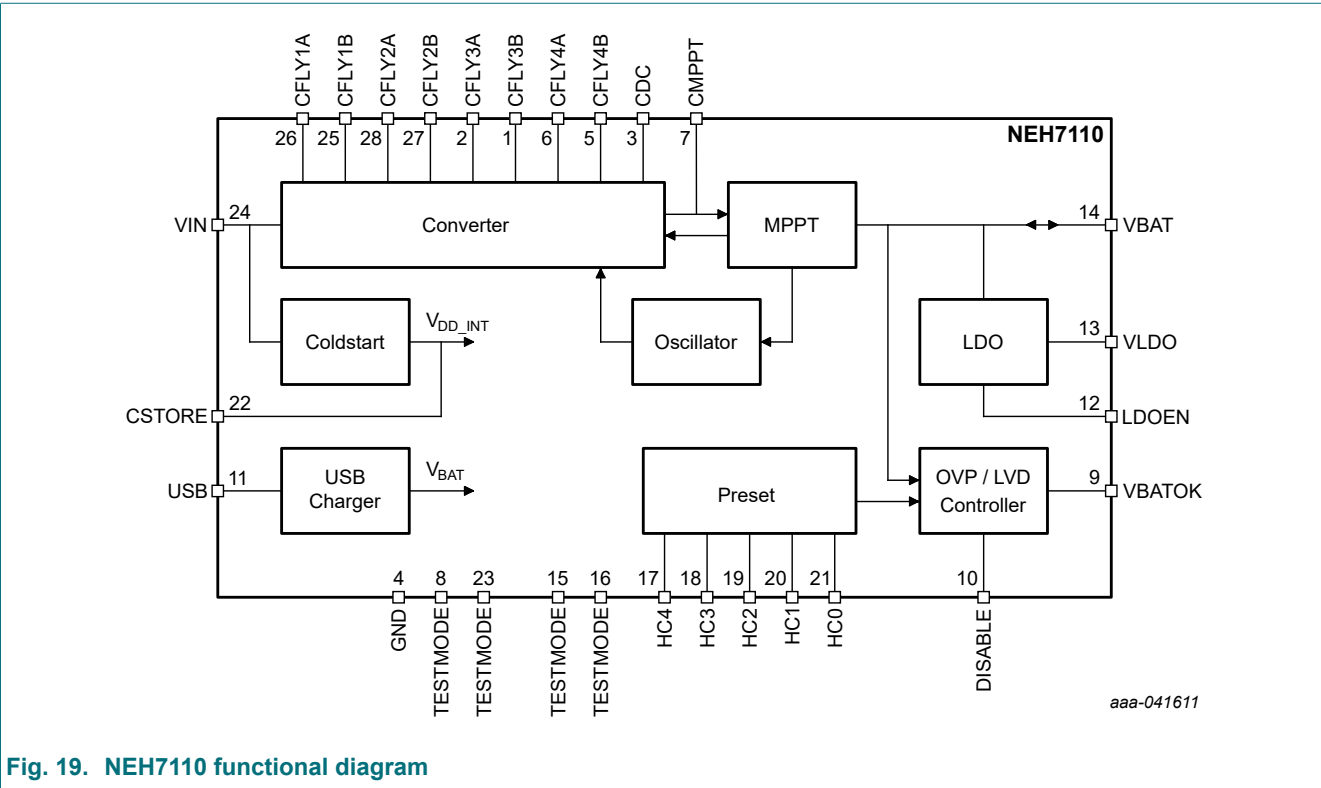


Fig. 19. NEH7110 functional diagram

7.3. Feature descriptions

7.3.1. Converter / MPPT

The main converter of the NEH7110 boosts the input voltage, V_{IN} , to the storage element voltage, V_{BAT} . In normal operation, V_{STORE} is internally connected to V_{BAT} . Boosting factor and switching frequency of the converter are dynamically chosen by the MPPT hill-climbing algorithm for the best efficiency. Regularly, the MPPT engine checks whether a better configuration is available. The MPPT procedure is performed once per second.

7.3.2. Coldstart

Normally, the NEH7110 operates from the storage element, connected to V_{BAT} . In case the storage element is depleted, the NEH7110 can resume operation via its coldstart feature. The device will collect energy from the harvester to power itself (via C_{STORE}) and subsequently charge the storage element (via V_{BAT}). The coldstart feature of the NEH7110 implements a controlled process, see Fig. 20. It needs a minimum input voltage of 270 mV and a minimum available input power of 12 μ W to get the device running.

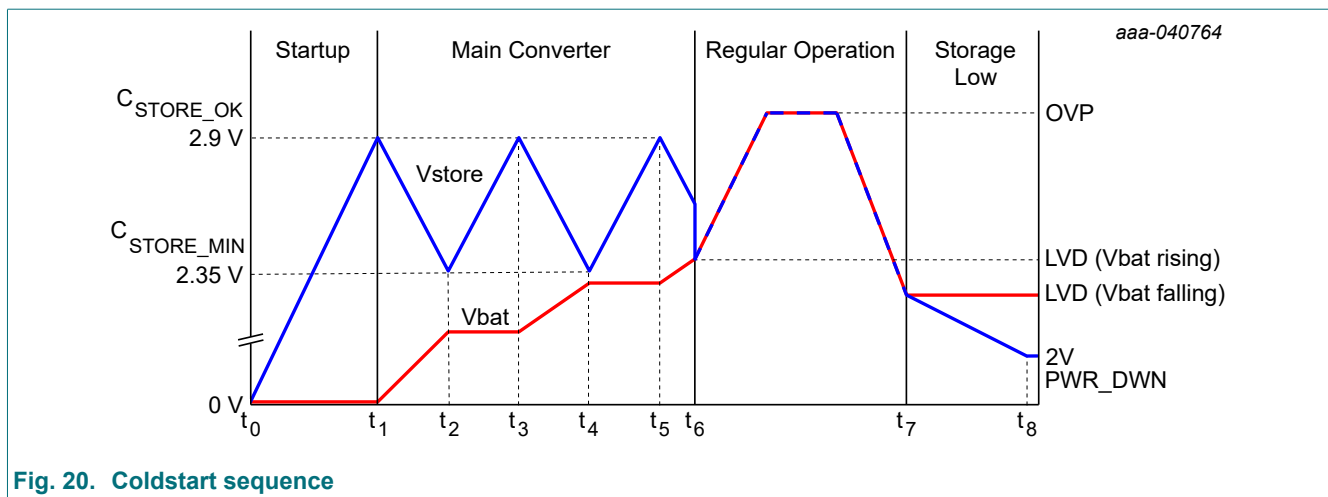


Fig. 20. Coldstart sequence

At the beginning of the coldstart operation, the coldstart power converter charges C_{STORE} using energy available from V_{IN} . Once the voltage across C_{STORE} reaches 2.9 V (C_{STORE_OK}) at t_1 , the device starts up. At this moment, the coldstart power converter is disabled and the main power converter is enabled. The main power converter starts charging the storage element at V_{BAT} , C_{STORE} is not being charged anymore. Since the main power converter consumes current from C_{STORE} , V_{STORE} starts to go down. At t_2 , when it reaches 2.35 V (C_{STORE_MIN}) the main power converter switches to charging C_{STORE} . This behavior continues to be repeated until V_{BAT} reaches the LVD(Rising) threshold at t_6 , on which V_{BAT} and C_{STORE} are shorted together.

The main power converter continues to charge V_{BAT} until the OVP threshold is reached. If there is no available energy at V_{IN} , the storage element at V_{BAT} and C_{STORE} will be discharged due to the current consumption of the chip and the application. Once V_{BAT} reaches the LVD(Falling) threshold while discharging, V_{BAT} and C_{STORE} are disconnected from each other. The device is still turned on and checking if there is any available power on V_{IN} . In case power is available at V_{IN} the process as indicated between t_1 and t_6 applies. In case no energy is available at V_{IN} , V_{STORE} keeps on lowering. Finally, if V_{STORE} falls below 2 V (PWR_DWN), the device is turned off. As soon as minimum power and voltage are present at V_{IN} , the device will automatically start the sequence at t_0 .

7.3.3. USB charging

In addition to obtaining energy via the harvester, the storage element can also be charged via the USB pin. The charger can be configured for a certain current limit. NEH7110 USB charging current is defaulted during start up to assume the HC pin configuration. The charging current level is applied according to Table 8. USB charging is automatically enabled when a voltage higher than 4 V is detected on the USB pin. The USB Charger uses CC charging until the OVP limit is reached where the charger changes to CV charging. The nominal USB charging current is equal to 80% of the maximum charging current setting. This is done to ensure that the maximum charging current, due to process and temperature variation, does not exceed the configured level.

7.3.4. Application LDO

To provide the required voltage to the application, an LDO is integrated. The LDO can be enabled and disabled using the LDOEN pin. The LDO output voltage can be set via the hardcode pins [Section 7.3.7](#).

The LDO is supplied from VBAT and can deliver 200 mA with a dropout voltage below 300 mV. Optimal closed-loop stability requires the LDO capacitor value to be 47 μ F. The capacitor should be placed as close as possible to the VLDO pin.

The LDO has a bypass mode to connect the VLDO pin to V_{BAT}. In this case V_{VLDO} will follow V_{BAT} instead of regulating to the set voltage.

7.3.5. Storage element over-voltage protection (OVP)

V_{BAT} of NEH7110 is actively limited to a configurable voltage level to protect the storage element against over-charging. The level should be chosen such that it is close to, but below the allowed maximum charge voltage as specified in the storage element data sheet. This over-voltage protection applies for both charging via energy harvesting and charging via USB port. The OVP level can be set via hardcoding, [Section 7.3.7](#).

7.3.6. Low voltage detection (LVD)

NEH7110 measures the storage element voltage to detect a too low voltage. The LVD threshold voltage can be configured via hardcoding, [Section 7.3.7](#). If the storage element voltage is below the LVD threshold voltage, VBATOK is low. The LVD rising threshold voltage is LVD falling threshold voltage plus 150 mV. When V_{BAT} rises above the LVD rising threshold, the VBATOK pin voltage rises to V_{BAT}.

7.3.7. Hard-code settings

The NEH7110 can be configured by hard-code settings pins HC0 to HC4. The hard-code settings are interpreted at the moment of power-up, V_{STORE} reaching C_{STORE_OK} level of the device, and are not read again until the next power cycle. The HC input should be either connected to a logic "0" (GND) or "1" (V_{STORE}). It is required to use V_{STORE} , rather than VBAT, as a logic "1" or "HIGH" reference to guarantee correct HC settings during coldstart operation. The hard-code configuration options can be found in [Table 8](#).

Table 8. Hard-code settings

HC4	HC3	HC2	HC1	HC0	OVP (V)	LVD (V)	LDO (V)	OCP (mA)
0	0	0	0	0	4.2	3.5	3.3	200
0	0	0	0	1		3.2	3.0	
0	0	0	1	0		2.6	2.4	
0	0	0	1	1		2.2	2.0	
0	0	1	0	0			1.8	
0	0	1	0	1			1.5	
0	0	1	1	0			1.2	
0	0	1	1	1			By-pass	
0	1	0	0	0	4.0	3.5	3.3	100
0	1	0	0	1			50	
0	1	0	1	0		3.3	3.0	100
0	1	0	1	1			2.4	
0	1	1	0	0			2.0	
0	1	1	0	1			1.8	
0	1	1	1	0			50	
0	1	1	1	1			1.5	100
1	0	0	0	0			1.2	10
1	0	0	0	1				
1	0	0	1	0		By-pass	100	
1	0	0	1	1	3.5	2.6	2.4	150
1	0	1	0	0			2.0	
1	0	1	0	1		2.5	1.8	200
1	0	1	1	0				150
1	0	1	1	1			1.5	200
1	1	0	0	0				150
1	1	0	0	1			1.2	
1	1	0	1	0		By-pass		
1	1	0	1	1	3.1	2.2	2.0	2
1	1	1	0	0			1.8	
1	1	1	0	1			1.5	
1	1	1	1	0			1.2	
1	1	1	1	1			By-pass	

8. Application and implementation

8.1. Typical application

A typical PV-cell application is shown in Fig. 21. Table 9 lists the Bill of Materials.

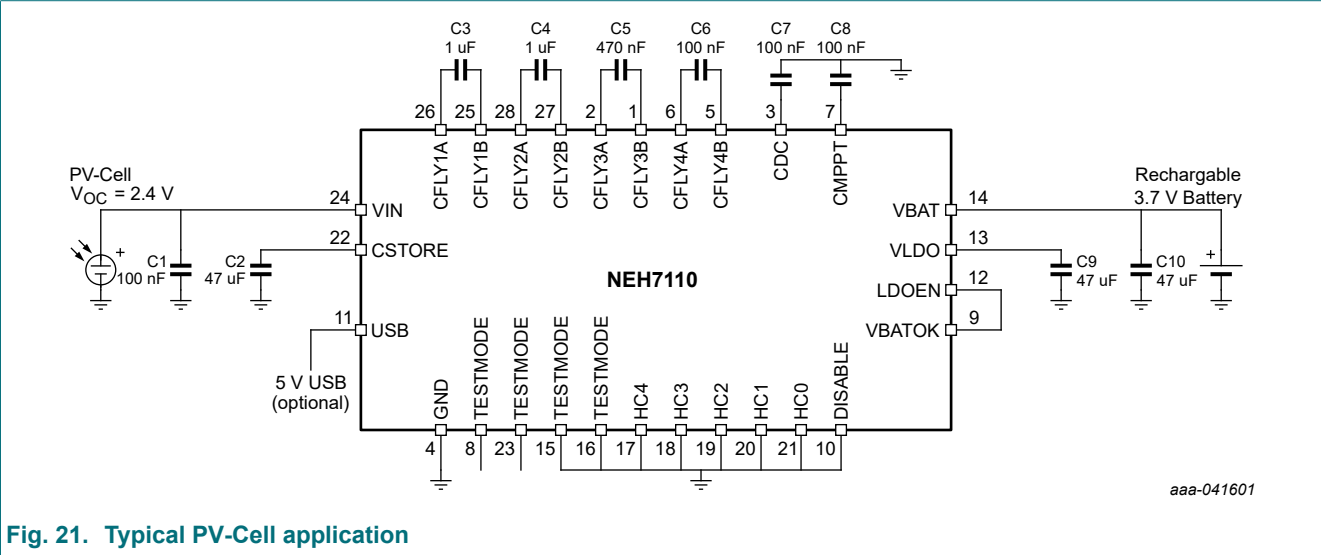


Fig. 21. Typical PV-Cell application

Table 9. Bill of Materials

Quantity	Reference designator	Value	Description	Manufacturer Part Number
1	U1	NEH7110	Energy Harvesting PMIC	NEH7110
4	C1, C6, C7, C8	0.1 μ F \pm 10% 10 V	ceramic capacitor X5R 0402 (1005 Metric)	GRM155R61A104KA01J
3	C2, C9, C10	47 μ F \pm 20% 6.3 V	ceramic Capacitor X5R 0603 (1608 Metric)	GRM188R60J476ME15D
2	C3, C4	1 μ F \pm 20% 10 V	ceramic capacitor X5R 0402 (1005 Metric)	GRM153R61A105ME95D
1	C5	0.47 μ F \pm 10% 10 V	ceramic capacitor X5R 0402 (1005 Metric)	GRM155R61A474KE15D
1	PV-Cell	-	PV-cell with V_{OC} = 2.4 V	-
1	rechargeable battery	-	3.7 V battery	-

8.2. Optimizing application, reducing number of capacitors

The NEH7110 is capable of boosting the input voltage by 2, 4, 8 or 16 times to V_{BAT} . Depending on the used harvester and storage element, not all boosting factors might be needed. In this case one or more boosting factors can be bypassed. The associated capacitor(s) can be removed resulting in a reduced bill-of-material (BOM) and thus cost saving.

For best overall performance, the harvester's maximum-power-point voltage, V_{MPP} , should fit within the configured input voltage range. Fig. 22 depicts the overall efficiency versus the harvester's V_{MPP} given $V_{BAT} = 3.7$ V. In case a harvester is not likely to operate in a part of the input voltage range, the input range might be reduced by excluding boosting factors. The maximum-power-point voltage is a characteristic of a harvester and varies based on environmental conditions such as light intensity and temperature. The V_{MPP} of a harvester is not always explicitly mentioned in its datasheet. For PV-cells, a good indicator for V_{MPP} is the open-circuit voltage (V_{OC}) parameter. The relation between V_{OC} and V_{MPP} :

$$V_{MPP} = 0.7 \dots 0.9 \cdot V_{OC}$$

The typical MPP ratio (V_{MPP}/V_{OC}) of a PV-cell is 0.8.

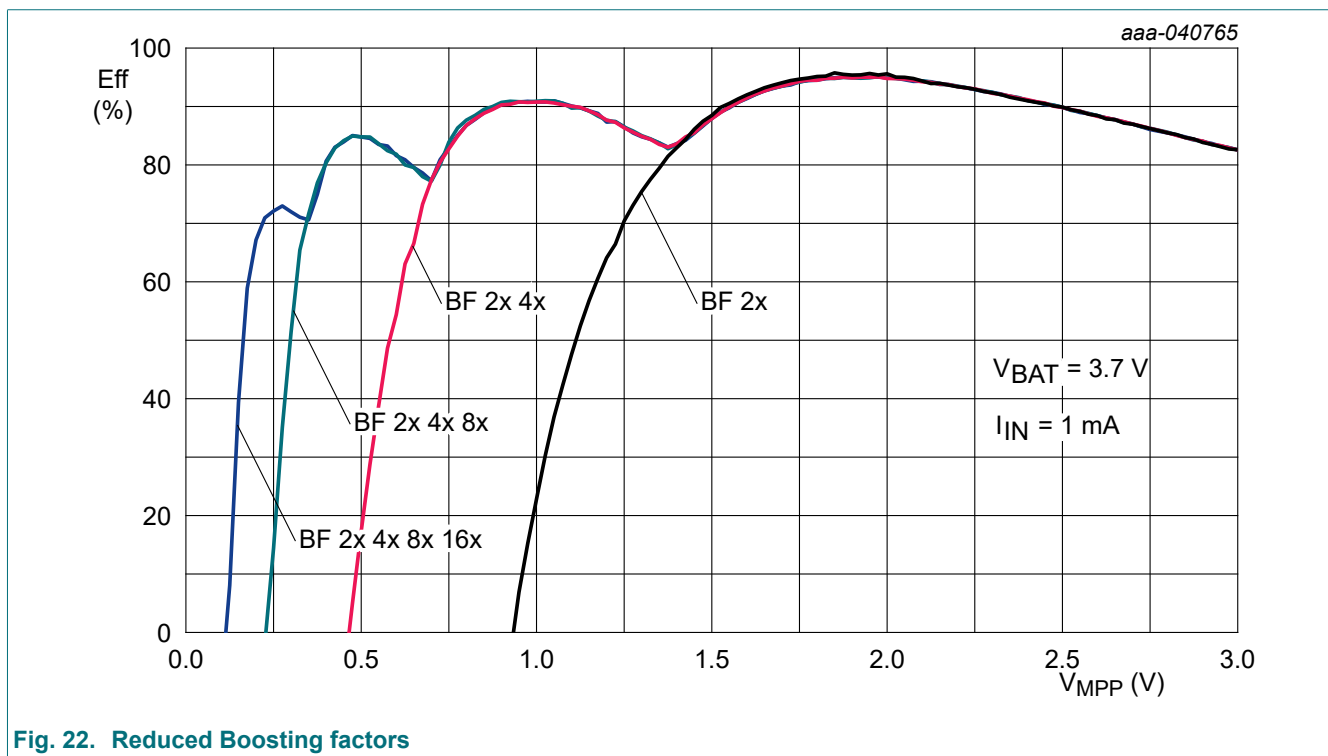


Table 10 provides the overview of V_{MPP} range for each boosting factor combination. The overall efficiency is not affected by reducing boosting factors if the harvester's V_{MPP} fits within the configured voltage range. The recommended V_{OC} range assumes a MPP ratio of 0.8.

Table 10. V_{MPP} range for boosting factor combinations, $V_{BAT} = 3.7$ V

Available Boosting Factors	V_{MPP} (V)	V_{OC} (V)
2, 4, 8, 16	0.15 to 3	0.19 to 3.75
2, 4, 8	0.3 to 3	0.38 to 3.75
2, 4	0.63 to 3	0.78 to 3.75
2	1.25 to 3	1.56 to 3.75

Fig. 23 to Fig. 26 show the four related configurations with different number of boosting factors enabled.

Inductorless energy harvesting PMIC with battery protection, LDO and USB charging

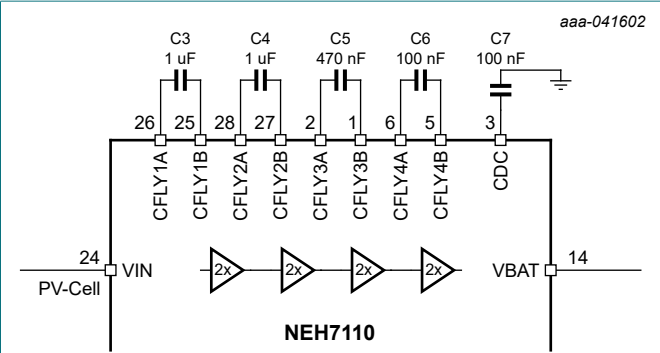


Fig. 23. Boosting factors: 2, 4, 8, 16

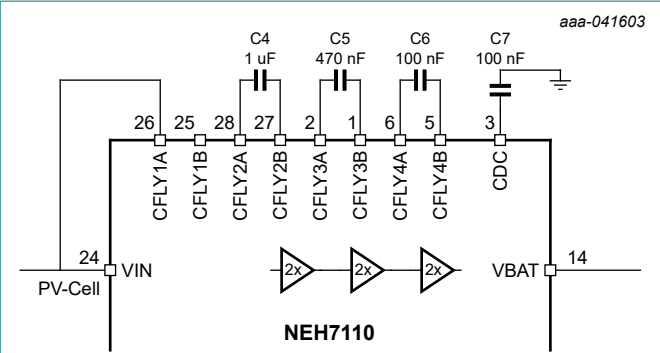


Fig. 24. Boosting factors: 2, 4, 8

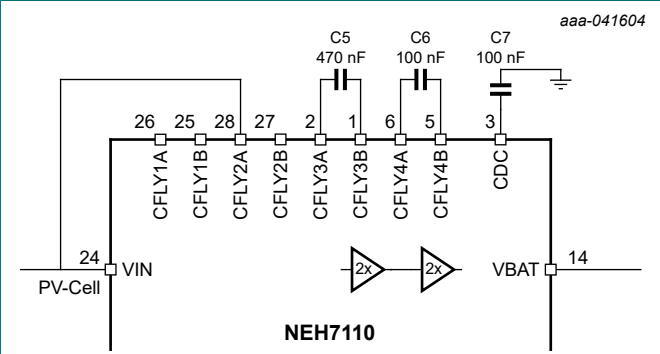


Fig. 25. Boosting factors: 2, 4

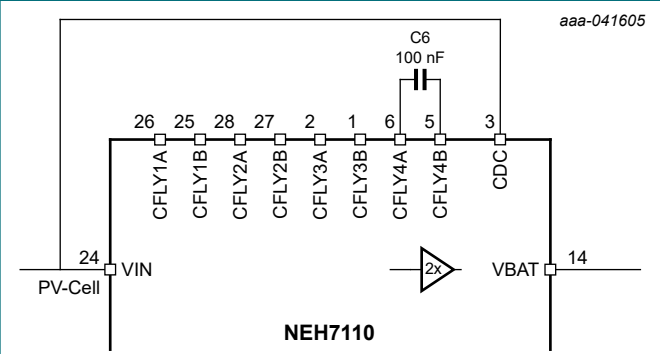


Fig. 26. Boosting factor: 2

Table 11 summarizes which capacitors can be omitted. For the reduced boosting factor configurations, a connection should be made between the input (VIN) and a particular flying-capacitor input pin.

Table 11. Configuration for reduced boosting factors

Available Boosting Factors	Capacitor(s) removed	Connection from VIN to
2, 4, 8, 16	-	-
2, 4, 8	C3	CFLY1A
2, 4	C3, C4	CFLY2A
2	C3, C4, C5, C7	CDC

8.3. Harvesting efficiency

The overall efficiency (Eff) of the NEH7110 in combination with a harvester comprises two components (see Fig. 27):

- 1) $\text{Eff}_{\text{converter}}$ The efficiency of the power converter in the NEH7110
- 2) $\text{Eff}_{\text{match}}$ The matching efficiency between the NEH7110 and the harvester

The total efficiency can be described as:

$$\text{Eff} = \text{Eff}_{\text{converter}} \cdot \text{Eff}_{\text{match}}$$

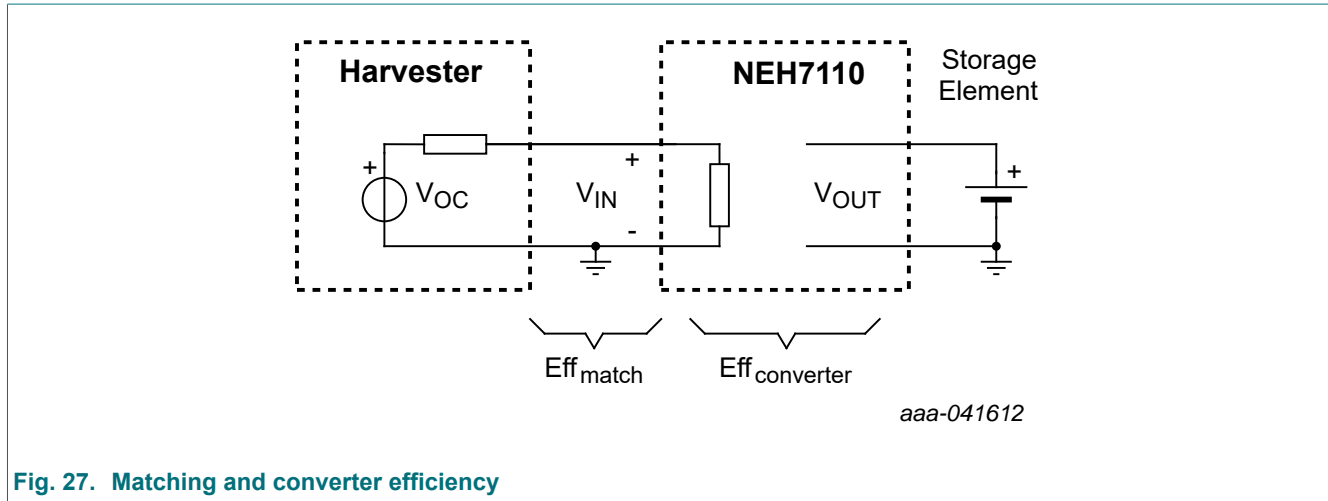


Fig. 27. Matching and converter efficiency

8.3.1. Power converter efficiency

In practice, a power converter has losses from input power (P_{IN}) to output power (P_{OUT}). The ratio of the output power and input power is typically referred to as the power-converter efficiency:

$$\text{Eff}_{\text{converter}} = \frac{P_{\text{OUT}}}{P_{\text{IN}}} \cdot 100 \%$$

For common inductive and capacitive power converters this efficiency is in the range of 80 % to 95 %. Several characteristics can have an impact on this efficiency, such as: ratio of the output voltage and input voltage, quality and size of the converter capacitors. In its targeted power range the converter efficiency of the NEH7110 is about 94 %.

8.3.2. Matching efficiency

In general, power transfer between components is optimized by matching the receiving input impedance with the transmitting output impedance. In a harvesting system it is also important to transfer power from harvester to the power converter in the most efficient manner to minimize loss of harvested energy. How optimal the power transfer between harvester and power converter is, can be expressed by matching efficiency.

The matching efficiency is defined as:

$$\text{Eff}_{\text{match}} = \frac{P_{\text{IN}}}{P_{\text{available}}} \cdot 100 \%$$

Where P_{IN} is the actual power at the input of the power converter and $P_{\text{available}}$ is the maximum power that can be achieved at the input (which is at 100% matching).

From the graphs in Section 6.6, (Fig. 6 to Fig. 12), it can be seen that the matching efficiency as part of the overall efficiency has a dependency on the ratio of V_{MPP} and V_{BAT} . The V_{BAT} relation can be understood from the perspective that the capacitive power converter has a given boost factor between input and output:

$$V_{\text{IN}} = \frac{V_{\text{BAT}}}{\text{boosting factor}}$$

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Where the boosting factor of the NEH7110 can be 2, 4, 8 or 16. The maximum power-point voltage (V_{MPP}) is the voltage on the power converter's input where most power is delivered by the harvester.

Thus, for optimal matching efficiency a harvester should be chosen with a V_{MPP} close to V_{BAT} / boosting factor. Since the efficiency of the PMIC is highest at the lowest boosting factor, this is the preferred boosting factor. In case the optimum PV cell is not available, the impact on the overall efficiency is limited, i.e. up to about 10 %, see [Fig. 12](#). This limited efficiency impact is as a result of the MPPT algorithm that can change more configuration parameters of the power converter than only the boosting factor.

10. Revision history

Table 12. Revision history

Document ID	Release date	Data sheet status	Change notice	Supersedes
NEH7110 v.1	20241217	Product data sheet	-	-

11. Legal information

Data sheet status

Document status [1][2]	Product status [3]	Definition
Objective [short] data sheet	Development	This document contains data from the objective specification for product development.
Preliminary [short] data sheet	Qualification	This document contains data from the preliminary specification.
Product [short] data sheet	Production	This document contains the product specification.

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- [2] The term 'short data sheet' is explained in section "Definitions".
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