

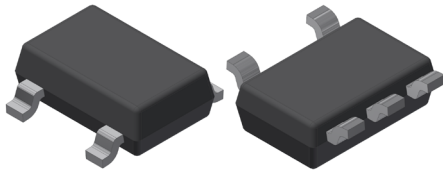
## AEC-Q100 Qualified Hall-Effect Current Sensor in 5-Pin SOT23-W for Cost-Optimized and Shunt Replacement Applications

### FEATURES AND BENEFITS

- Self-contained shuntless current sensing that does not require an external sense resistor; single-package solution
- Low ohmic loss with 1.6 mΩ conductor resistance on the LH package
- Differential sensing robust to external magnetic fields
- Small-footprint, five-pin small-outline transistor (SOT23-W) package (suffix LH)
- 125 kHz analog output for fast response time
- Inherent galvanic isolation
  - 100 V<sub>RMS</sub> functional isolation (ACS37041 only)
  - UL-certified 285 V<sub>RMS</sub> basic working voltage (ACS37042 only, pending)
- Total error less than ±5% over temperature
- 3.3 V and 5 V supply-voltage options
- Nonratiometric output
- Bidirectional current sensing up to 30 A
- Wide operating temperature range, -40°C to 125°C
- AEC-Q100 Grade 1, automotive qualified

### PACKAGE

5-pin SOT23-W  
(suffix LH)



### DESCRIPTION

The ACS37041/2 is a small, integrated current sensor for cost-optimized applications. It features a voltage output that is galvanically isolated from the measured current. The current conductor has a low 1.6 mΩ resistance, ideal for low power dissipation constraints.

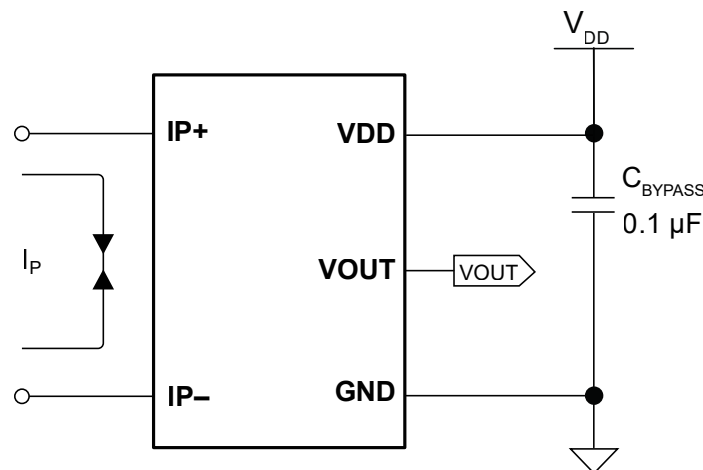
The ACS37041 features a 100 V<sub>RMS</sub> functional working voltage while the ACS37042 features a 285 V<sub>RMS</sub> basic working voltage.

The ACS37041/2 has 5 V and 3.3 V variants, which allows it to function in a variety of applications. The ACS37041/2 has a sensitivity error that is less than ±3.5% over temperature and can sense up to 30 A bidirectionally, all with the same footprint as a five-pin SOT23-W current-sense amplifier without the need for a shunt resistor.

The ACS37041/2 is a lead (Pb) free device plated with 100% matte tin, compatible with standard lead-free printed circuit board assembly processes.

### APPLICATIONS

- Industrial motor drivers (<100 V)
- Clean energy string inverter (optimizer)
- Clean energy microinverter
- Personal mobility (e-bikes and e-scooters)



The ACS37041 and ACS37042 output an analog signal at VOUT that varies linearly with the primary current,  $I_p$ , within the specified ranges.

Figure 1: Typical Application Circuit

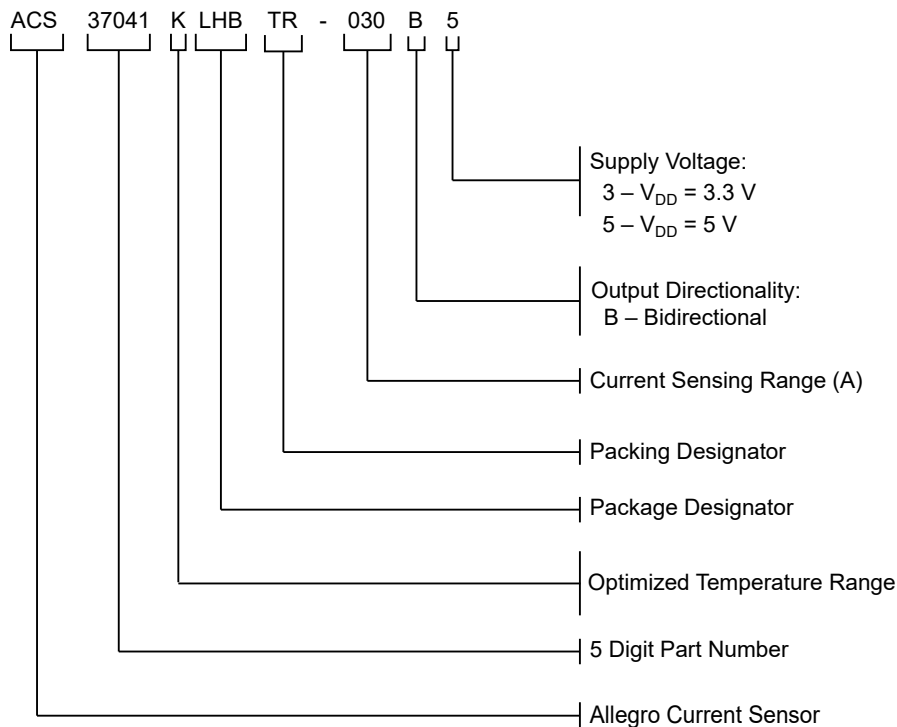
# ACS37041 and ACS37042

# AEC-Q100 Qualified Hall-Effect Current Sensor in 5-Pin SOT23-W for Cost-Optimized and Shunt Replacement Applications

## SELECTION GUIDE

Part Number	Current Sensing Range, $I_{PR}$ (A)	Sensitivity (mV/A)	$V_{DD}$ (V)	$V_{QVO}$ (V)	Isolation	Optimized Temperature Range $T_A$ (°C)	Packing
ACS37041KLHBLT-010B3	±10	132	3.3	1.65	Functional	-40 to 125	Tape and Reel, 3000 pieces per reel
ACS37041KLHBLT-030B3	±30	44					
ACS37041KLHBLT-010B5	±10	200	5	2.5			
ACS37041KLHBLT-030B5	±30	66.7					
ACS37042KLHBLT-010B3	±10	132	3.3	1.65	Basic	-40 to 125	Tape and Reel, 3000 pieces per reel
ACS37042KLHBLT-030B3	±30	44					
ACS37042KLHBLT-010B5	±10	200	5	2.5			
ACS37042KLHBLT-030B5	±30	66.7					

## NAMING SPECIFICATION



# ACS37041 and ACS37042

# AEC-Q100 Qualified Hall-Effect Current Sensor in 5-Pin SOT23-W for Cost-Optimized and Shunt Replacement Applications

## ABSOLUTE MAXIMUM RATINGS [1]

Characteristic	Symbol	Notes	Min	Max	Unit
Supply Voltage	$V_{DD}$	Applies to VDD	-0.5	6	V
Output Voltage	$V_O$	Applies to VOUT	-0.5	$V_{DD} + 0.5$	V
Operating Ambient Temperature	$T_A$		-40	125	°C
Storage Temperature	$T_{stg}$		-65	165	°C
Maximum Junction Temperature	$T_{J(max)}$		-	165	°C

[1] Stresses in excess of those listed in the absolute maximum ratings may cause permanent damage to the device. This is a stress rating only; functional operation of the device at these limits or at any other condition that exceeds those indicated in the operational sections of this specification is not implied. Exposure to an absolute maximum rating for an extended period may affect device reliability.

## ISOLATION CHARACTERISTICS

Characteristic	Symbol	Notes	Rating	Unit
<b>ACS37041 Only</b>				
Working Voltage for Functional Isolation	$V_{WVFI}$	Allegro approved working voltage for functional insulation	100	$V_{RMS}$
<b>ACS37042 Only</b>				
Withstand Voltage [1][2]	$V_{ISO}$	Agency rated for 60 seconds per UL 62368-1 (edition 3)	1767	$V_{RMS}$
Working Voltage for Basic Isolation [2]	$V_{WVBI}$	Maximum approved working voltage for basic insulation according to UL 62368-1 (edition 3)	403	$V_{PK}$ or $V_{DC}$
			285	$V_{RMS}$
Impulse Withstand Voltage	$V_{IMPULSE}$	Tested $\pm 5$ pulses at 2/minute in compliance with IEC 61000-4-5, 1.2 $\mu s$ (rise) and 50 $\mu s$ (width)	2500	$V_{PK}$
<b>ACS37041/ACS37042</b>				
Clearance	$D_{CL}$	Minimum distance through air from IP leads to signal leads	1.9	mm
Creepage	$D_{CR}$	Minimum distance along package body from IP leads to signal leads	2	mm
Distance Through Insulation	DTI	Minimum internal distance through insulation	25	$\mu m$
Comparative Tracking Index	CTI	Material Group II	400 to 599	V

[1] 100% production-tested in accordance with UL 62368-1 (edition 3).

[2] Certification pending.

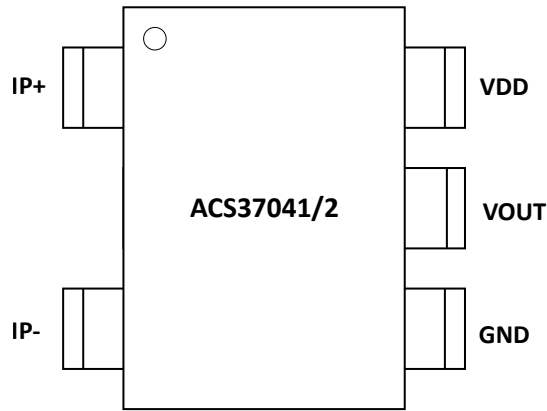
## PACKAGE CHARACTERISTICS

Characteristic	Symbol	Notes	Min.	Typ.	Max.	Unit
Internal Conductor Resistance	$R_{IC}$	$T_A = 25^\circ C$	-	1.6	-	m $\Omega$
Internal Conductor Inductance	$L_{IC}$	$T_A = 25^\circ C$	-	2	-	nH
Moisture Sensitivity Level	MSL	Per IPC/JEDEC J-STD-020	-	1	-	-

## THERMAL CHARACTERISTICS

Characteristic	Symbol	Notes	Value	Unit
Package Thermal Resistance (Junction to Ambient)	$R_{\theta JA}$	Mounted on the Allegro LH Current Sensor Evaluation Board (ACSEVB-LH5)	32	°C/W
Package Thermal Metric (Junction to Top)	$\Psi_{JT}$		3	°C/W

**PINOUT DIAGRAM AND TERMINAL LIST TABLE**

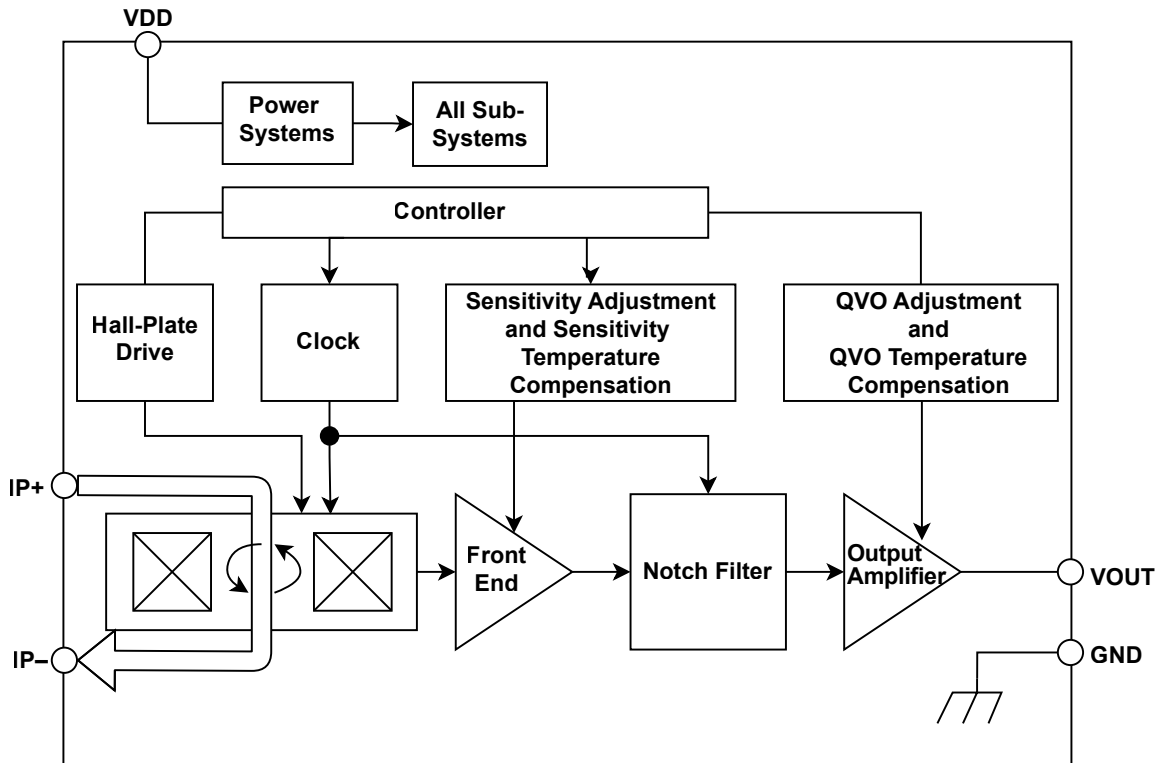


**Terminal List Table**

Number	Name	Function
1, 2	IP	Integrated current sensing path
3	GND	Device ground
4	VOUT	Voltage output
5	VDD	Device supply voltage

**Figure 2: LH Package Pinout Diagram**

**FUNCTIONAL BLOCK DIAGRAM**



**Figure 3: Functional Block Diagram**

**COMMON ELECTRICAL CHARACTERISTICS:** Valid through full operating temperature range,  $T_A = -40^{\circ}\text{C}$  to  $125^{\circ}\text{C}$ ,  $C_{\text{BYPASS}} = 0.1 \mu\text{F}$ , and typical  $V_{\text{DD}}$ , unless otherwise specified

Characteristic	Symbol	Test Conditions	Min.	Typ.	Max.	Units
Supply Voltage	$V_{\text{DD}}$	5 V variant	4.5	5	5.5	V
		3.3 V variant	3	3.3	3.6	V
Supply Current	$I_{\text{DD}}$	5 V variant, load not present on VOUT	–	9	12	mA
		3.3 V variant, load not present on VOUT	–	8	10	mA
VOUT Capacitive Load	$C_{\text{L\_VOUT}}$	VOUT to GND	–	–	1	nF
VOUT Resistive Load	$R_{\text{L\_VOUT}}$	VOUT to GND, VOUT to VDD	10	–	–	k $\Omega$
Power-On Reset Voltage	$V_{\text{POR}}$	VDD rising 1 V/ms	–	–	2.9	V
POR Hysteresis	$V_{\text{POR\_HYS}}$		100	–	–	mV
Power-On Time	$t_{\text{PO}}$	$T_A = 25^{\circ}\text{C}$ , $V_{\text{DD}}$ rising 1 V/ms	–	84	–	$\mu\text{s}$
Rise Time	$t_{\text{R}}$	$T_A = 25^{\circ}\text{C}$ , $C_{\text{L\_VOUT}} = 1 \text{ nF}$	–	2.8	4.8	$\mu\text{s}$
Response Time	$t_{\text{RESP}}$	$T_A = 25^{\circ}\text{C}$ , $C_{\text{L\_VOUT}} = 1 \text{ nF}$	–	3	5	$\mu\text{s}$
Propagation Delay	$t_{\text{PD}}$	$T_A = 25^{\circ}\text{C}$ , $C_{\text{L\_VOUT}} = 1 \text{ nF}$	–	1.8	3	$\mu\text{s}$
Bandwidth	BW	Small signal –3 dB, $C_{\text{L\_VOUT}} = 1 \text{ nF}$	–	125	–	kHz
Noise Density	$N_{\text{D}}$	5 V variant, $T_A = 25^{\circ}\text{C}$ , $C_{\text{L\_VOUT}} = 1 \text{ nF}$	–	139	–	$\mu\text{A}/\sqrt{\text{Hz}}$
		3.3 V variant, $T_A = 25^{\circ}\text{C}$ , $C_{\text{L\_VOUT}} = 1 \text{ nF}$	–	205	–	$\mu\text{A}/\sqrt{\text{Hz}}$
Output Saturation Voltage	$V_{\text{SAT\_H}}$	$R_{\text{L\_VOUT}} = 10 \text{ k}\Omega$ to GND	$V_{\text{DD}} - 0.25$	–	–	V
	$V_{\text{SAT\_L}}$	$R_{\text{L\_VOUT}} = 10 \text{ k}\Omega$ to VDD	–	–	0.25	V
Common-Mode Field Sensitivity	CMFS	Input-referred error due to a 40 G common-mode field	–	0.45	–	mA/G

# ACS37041 and ACS37042

# AEC-Q100 Qualified Hall-Effect Current Sensor in 5-Pin SOT23-W for Cost-Optimized and Shunt Replacement Applications

**xKLHB-010B3 PERFORMANCE CHARACTERISTICS:** Valid through full operating temperature range,  $T_A = -40^\circ\text{C}$  to  $125^\circ\text{C}$ ,  $C_{\text{BYPASS}} = 0.1 \mu\text{F}$ , and  $V_{\text{DD}} = 3.3 \text{ V}$  unless otherwise specified

Characteristic	Symbol	Test Conditions	Min.	Typ.	Max.	Units
<b>NOMINAL PERFORMANCE</b>						
Current Sensing Range	$I_{\text{PR}}$		-10	-	10	A
Sensitivity	Sens	$I_{\text{PR}(\text{min})} < I_{\text{P}} < I_{\text{PR}(\text{max})}$	-	132	-	mV/A
Quiescent Voltage Output	$V_{\text{QVO}}$	$I_{\text{P}} = 0 \text{ A}$	-	1.65	-	V
<b>ERROR COMPONENTS [1]</b>						
Noise	N	$T_A = 25^\circ\text{C}$ , $C_{\text{L\_VOUT}} = 1 \text{ nF}$ , $\text{BW} = 125 \text{ kHz}$	-	$\pm 13$	-	mV <sub>RMS</sub>
Power Supply Sensitivity Error	$E_{\text{SENS\_PS}}$	$V_{\text{DD}(\text{MIN})}$ to $V_{\text{DD}(\text{MAX})}$ , $T_A = -40^\circ\text{C}$ to $125^\circ\text{C}$	-1.8	-	1.8	%
Power Supply Quiescent Voltage Output Error	$V_{\text{QVO\_PS}}$	$V_{\text{DD}(\text{MIN})}$ to $V_{\text{DD}(\text{MAX})}$ , $T_A = -40^\circ\text{C}$ to $125^\circ\text{C}$	-11	-	11	mV
<b>ERROR COMPONENTS INCLUDING LIFETIME DRIFT [2]</b>						
Sensitivity Error	$E_{\text{SENS}}$	$I_{\text{P}} = 3 \text{ A}$ , $T_A = 25^\circ\text{C}$	-2.3	$\pm 1.2$	2.3	%
		$I_{\text{P}} = 3 \text{ A}$ , $T_A = 25^\circ\text{C}$ to $125^\circ\text{C}$	-2.8	$\pm 1.2$	2.8	%
		$I_{\text{P}} = 3 \text{ A}$ , $T_A = -40^\circ\text{C}$ to $25^\circ\text{C}$	-3.1	$\pm 1.2$	3.1	%
Quiescent Voltage Output Error	$V_{\text{QVO\_E}}$	$I_{\text{P}} = 0 \text{ A}$ , $T_A = 25^\circ\text{C}$	-20	$\pm 7$	20	mV
		$I_{\text{P}} = 0 \text{ A}$ , $T_A = 25^\circ\text{C}$ to $125^\circ\text{C}$	-27	$\pm 11$	27	mV
		$I_{\text{P}} = 0 \text{ A}$ , $T_A = -40^\circ\text{C}$ to $25^\circ\text{C}$	-21	$\pm 10$	21	mV

[1] The minimum-to-maximum (min-to-max) interval of the performance characteristics is determined such that 99.99% of devices lie within the interval during initial characterization. The worst case of  $\mu \pm 6\sigma$  is calculated and applied symmetrically. The minimum and maximum limits include a calculation buffer for additional margin.

[2] The minimum-to-maximum interval is determined such that 99.7% of devices lie within the interval derived from two lots of characterization and the worst-case drift observed in AEC-Q100 qualification stresses with additional margin. The worst case of  $\mu \pm 3\sigma$  is calculated and applied symmetrically. The typical (typ) characteristic is determined such that 68% of devices lie within the interval during initial characterization. The worst case of  $\mu \pm 1\sigma$  is calculated and recorded.

# ACS37041 and ACS37042

# AEC-Q100 Qualified Hall-Effect Current Sensor in 5-Pin SOT23-W for Cost-Optimized and Shunt Replacement Applications

**xKLHB-030B3 PERFORMANCE CHARACTERISTICS:** Valid through full operating temperature range,  $T_A = -40^\circ\text{C}$  to  $125^\circ\text{C}$ ,  $C_{\text{BYPASS}} = 0.1 \mu\text{F}$ , and  $V_{\text{DD}} = 3.3 \text{ V}$  unless otherwise specified

Characteristic	Symbol	Test Conditions	Min.	Typ.	Max.	Units
<b>NOMINAL PERFORMANCE</b>						
Current Sensing Range [1]	$I_{\text{PR}}$		-30	-	30	A
Sensitivity	Sens	$I_{\text{PR}(\text{min})} < I_{\text{P}} < I_{\text{PR}(\text{max})}$	-	44	-	mV/A
Quiescent Voltage Output	$V_{\text{QVO}}$	$I_{\text{P}} = 0 \text{ A}$	-	1.65	-	V
<b>ERROR COMPONENTS [2]</b>						
Noise	N	$T_A = 25^\circ\text{C}$ , $C_{\text{L\_VOUT}} = 1 \text{ nF}$ , $\text{BW} = 125 \text{ kHz}$	-	$\pm 4$	-	$\text{mV}_{\text{RMS}}$
Power Supply Sensitivity Error	$E_{\text{SENS\_PS}}$	$V_{\text{DD}(\text{MIN})}$ to $V_{\text{DD}(\text{MAX})}$ , $T_A = -40^\circ\text{C}$ to $125^\circ\text{C}$	-1.8	-	1.8	%
Power Supply Quiescent Voltage Output Error	$V_{\text{QVO\_PS}}$	$V_{\text{DD}(\text{MIN})}$ to $V_{\text{DD}(\text{MAX})}$ , $T_A = -40^\circ\text{C}$ to $125^\circ\text{C}$	-5	-	5	mV
<b>ERROR COMPONENTS INCLUDING LIFETIME DRIFT [3]</b>						
Sensitivity Error	$E_{\text{SENS}}$	$I_{\text{P}} = 3 \text{ A}$ , $T_A = 25^\circ\text{C}$	-2.4	$\pm 1.4$	2.4	%
		$I_{\text{P}} = 3 \text{ A}$ , $T_A = 25^\circ\text{C}$ to $125^\circ\text{C}$	-2.6	$\pm 1.4$	2.6	%
		$I_{\text{P}} = 3 \text{ A}$ , $T_A = -40^\circ\text{C}$ to $25^\circ\text{C}$	-2.9	$\pm 1.4$	2.9	%
Quiescent Voltage Output Error	$V_{\text{QVO\_E}}$	$I_{\text{P}} = 0 \text{ A}$ , $T_A = 25^\circ\text{C}$	-11	$\pm 4$	11	mV
		$I_{\text{P}} = 0 \text{ A}$ , $T_A = 25^\circ\text{C}$ to $125^\circ\text{C}$	-12	$\pm 4$	12	mV
		$I_{\text{P}} = 0 \text{ A}$ , $T_A = -40^\circ\text{C}$ to $25^\circ\text{C}$	-16	$\pm 9$	16	mV

[1] For accuracy considerations with current greater than 15 A, refer to the IP Power Dissipation Output Drift section.

[2] The minimum-to-maximum (min-max) interval of the performance characteristics is determined such that 99.99% of devices lie within the interval during initial characterization. The worst case of  $\mu \pm 6\sigma$  is calculated and applied symmetrically. The minimum and maximum limits include a calculation buffer for additional margin.

[3] The minimum-to-maximum interval is determined such that 99.7% of devices lie within the interval derived from two lots of characterization and the worst-case drift observed in AEC-Q100 qualification stresses with additional margin. The worst case of  $\mu \pm 3\sigma$  is calculated and applied symmetrically. The typical (typ) characteristic is determined such that 68% of devices lie within the interval during initial characterization. The worst case of  $\mu \pm 1\sigma$  is calculated and recorded.

# ACS37041 and ACS37042

# AEC-Q100 Qualified Hall-Effect Current Sensor in 5-Pin SOT23-W for Cost-Optimized and Shunt Replacement Applications

**xKLHB-010B5 PERFORMANCE CHARACTERISTICS:** Valid through full operating temperature range,  $T_A = -40^\circ\text{C}$  to  $125^\circ\text{C}$ ,  $C_{\text{BYPASS}} = 0.1 \mu\text{F}$ , and  $V_{\text{DD}} = 5 \text{ V}$  unless otherwise specified

Characteristic	Symbol	Test Conditions	Min.	Typ.	Max.	Units
<b>NOMINAL PERFORMANCE</b>						
Current Sensing Range	$I_{\text{PR}}$		-10	-	10	A
Sensitivity	Sens	$I_{\text{PR}(\text{min})} < I_{\text{P}} < I_{\text{PR}(\text{max})}$	-	200	-	mV/A
Quiescent Voltage Output	$V_{\text{QVO}}$	$I_{\text{P}} = 0 \text{ A}$	-	2.5	-	V
<b>ERROR COMPONENTS [1]</b>						
Noise	N	$T_A = 25^\circ\text{C}$ , $C_{\text{L\_VOUT}} = 1 \text{ nF}$ , $\text{BW} = 125 \text{ kHz}$	-	$\pm 13$	-	mV <sub>RMS</sub>
Power Supply Sensitivity Error	$E_{\text{SENS\_PS}}$	$V_{\text{DD}(\text{MIN})}$ to $V_{\text{DD}(\text{MAX})}$ , $T_A = -40^\circ\text{C}$ to $125^\circ\text{C}$	-1.3	-	1.3	%
Power Supply Quiescent Voltage Output Error	$V_{\text{QVO\_PS}}$	$V_{\text{DD}(\text{MIN})}$ to $V_{\text{DD}(\text{MAX})}$ , $T_A = -40^\circ\text{C}$ to $125^\circ\text{C}$	-16	-	16	mV
<b>ERROR COMPONENTS INCLUDING LIFETIME DRIFT [2]</b>						
Sensitivity Error	$E_{\text{SENS}}$	$I_{\text{P}} = 3 \text{ A}$ , $T_A = 25^\circ\text{C}$	-2.1	$\pm 1.2$	2.1	%
		$I_{\text{P}} = 3 \text{ A}$ , $T_A = 25^\circ\text{C}$ to $125^\circ\text{C}$	-3.1	$\pm 1.6$	3.1	%
		$I_{\text{P}} = 3 \text{ A}$ , $T_A = -40^\circ\text{C}$ to $25^\circ\text{C}$	-2.9	$\pm 1.2$	2.9	%
Quiescent Voltage Output Error	$V_{\text{QVO\_E}}$	$I_{\text{P}} = 0 \text{ A}$ , $T_A = 25^\circ\text{C}$	-26	$\pm 6$	26	mV
		$I_{\text{P}} = 0 \text{ A}$ , $T_A = 25^\circ\text{C}$ to $125^\circ\text{C}$	-45	$\pm 11$	45	mV
		$I_{\text{P}} = 0 \text{ A}$ , $T_A = -40^\circ\text{C}$ to $25^\circ\text{C}$	-31	$\pm 8$	31	mV

[1] The minimum-to-maximum (min-to-max) interval of the performance characteristics is determined such that 99.99% of devices lie within the interval during initial characterization. The worst case of  $\mu \pm 6\sigma$  is calculated and applied symmetrically. The minimum and maximum limits include a calculation buffer for additional margin.

[2] The minimum-to-maximum interval is determined such that 99.7% of devices lie within the interval derived from two lots of characterization and the worst-case drift observed in AEC-Q100 qualification stresses with additional margin. The worst case of  $\mu \pm 3\sigma$  is calculated and applied symmetrically. The typical (typ) characteristic is determined such that 68% of devices lie within the interval during initial characterization. The worst case of  $\mu \pm 1\sigma$  is calculated and recorded.

**xKLHB-030B5 PERFORMANCE CHARACTERISTICS:** Valid through full operating temperature range,  $T_A = -40^\circ\text{C}$  to  $125^\circ\text{C}$ ,  $C_{\text{BYPASS}} = 0.1 \mu\text{F}$ , and  $V_{\text{DD}} = 5 \text{ V}$  unless otherwise specified

Characteristic	Symbol	Test Conditions	Min.	Typ.	Max.	Units
<b>NOMINAL PERFORMANCE</b>						
Current Sensing Range [1]	$I_{\text{PR}}$		-30	-	30	A
Sensitivity	Sens	$I_{\text{PR}(\text{min})} < I_{\text{P}} < I_{\text{PR}(\text{max})}$	-	66.7	-	mV/A
Quiescent Voltage Output	$V_{\text{QVO}}$	$I_{\text{P}} = 0 \text{ A}$	-	2.5	-	V
<b>ERROR COMPONENTS [2]</b>						
Noise	N	$T_A = 25^\circ\text{C}$ , $C_{\text{L\_VOUT}} = 1 \text{ nF}$ , $\text{BW} = 125 \text{ kHz}$	-	$\pm 4$	-	$\text{mV}_{\text{RMS}}$
Power Supply Sensitivity Error	$E_{\text{SENS\_PS}}$	$V_{\text{DD}(\text{MIN})}$ to $V_{\text{DD}(\text{MAX})}$ , $T_A = -40^\circ\text{C}$ to $125^\circ\text{C}$	-1.3	-	1.3	%
Power Supply Quiescent Voltage Output Error	$V_{\text{QVO\_PS}}$	$V_{\text{DD}(\text{MIN})}$ to $V_{\text{DD}(\text{MAX})}$ , $T_A = -40^\circ\text{C}$ to $125^\circ\text{C}$	-8	-	8	mV
<b>ERROR COMPONENTS INCLUDING LIFETIME DRIFT [3]</b>						
Sensitivity Error	$E_{\text{SENS}}$	$I_{\text{P}} = 3 \text{ A}$ , $T_A = 25^\circ\text{C}$	-2.7	$\pm 1.1$	2.7	%
		$I_{\text{P}} = 3 \text{ A}$ , $T_A = 25^\circ\text{C}$ to $125^\circ\text{C}$	-3.3	$\pm 1.6$	3.3	%
		$I_{\text{P}} = 3 \text{ A}$ , $T_A = -40^\circ\text{C}$ to $25^\circ\text{C}$	-2.8	$\pm 1.1$	2.8	%
Quiescent Voltage Output Error	$V_{\text{QVO\_E}}$	$I_{\text{P}} = 0 \text{ A}$ , $T_A = 25^\circ\text{C}$	-13	$\pm 4$	13	mV
		$I_{\text{P}} = 0 \text{ A}$ , $T_A = 25^\circ\text{C}$ to $125^\circ\text{C}$	-19	$\pm 6$	19	mV
		$I_{\text{P}} = 0 \text{ A}$ , $T_A = -40^\circ\text{C}$ to $25^\circ\text{C}$	-19	$\pm 8$	19	mV

[1] For accuracy considerations with current greater than 15 A, refer to the IP Power Dissipation Output Drift section.

[2] The minimum-to-maximum (min-to-max) interval of the performance characteristics is determined such that 99.99% of devices lie within the interval during initial characterization. The worst case of  $\mu \pm 6\sigma$  is calculated and applied symmetrically. The minimum and maximum limits include a calculation buffer for additional margin.

[3] The minimum-to-maximum interval is determined such that 99.7% of devices lie within the interval derived from two lots of characterization and the worst-case drift observed in AEC-Q100 qualification stresses with additional margin. The worst case of  $\mu \pm 3\sigma$  is calculated and applied symmetrically. The typical (typ) characteristic is determined such that 68% of devices lie within the interval during initial characterization. The worst case of  $\mu \pm 1\sigma$  is calculated and recorded.

### RESPONSE CHARACTERISTICS DEFINITIONS AND PERFORMANCE DATA

#### Response Time ( $t_{RESP}$ )

The time interval between a) when the sensed input current reaches 90% of its full-scale value, and b) when the sensor output,  $V_{OUT}$ , reaches 90% of its full-scale output value.

#### Rise Time ( $t_R$ )

The time interval between a) when the sensor output,  $V_{OUT}$ , reaches 10% of its full-scale value, and b) when the sensor output,  $V_{OUT}$ , reaches 90% of its full-scale value.

#### Propagation Delay ( $t_{PD}$ )

The time interval between a) when the sensed input current reaches 20% of its full-scale value, and b) when the sensor output,  $V_{OUT}$ , reaches 20% of its full-scale output value.

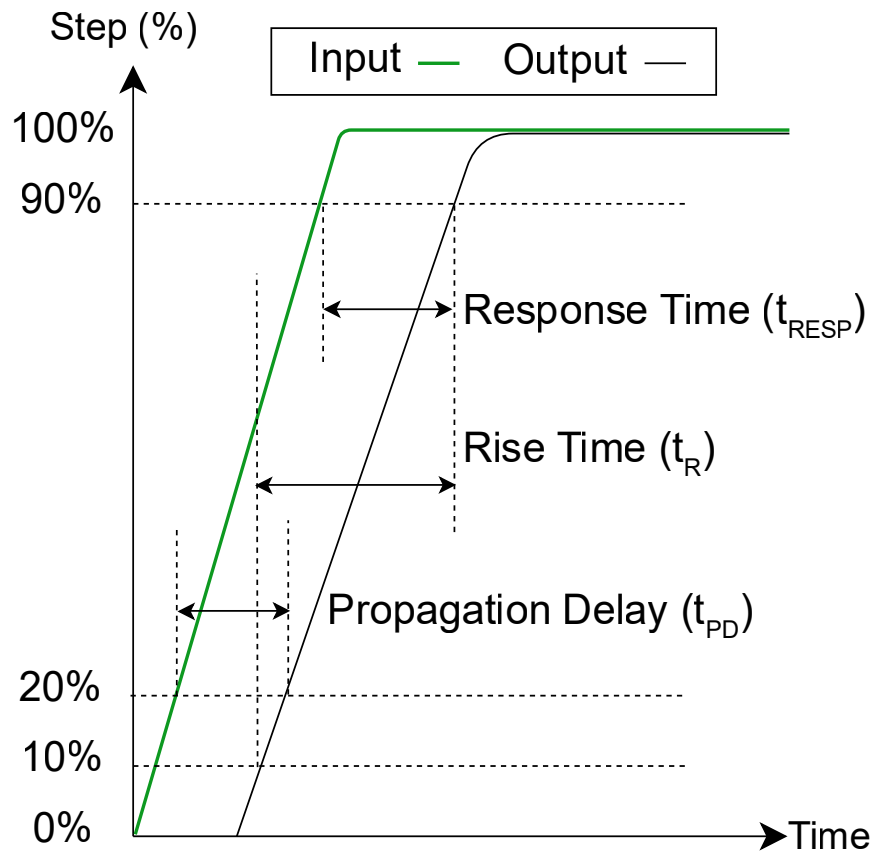


Figure 4: Step Response Characteristics

## FUNCTIONAL DESCRIPTION OF POWER-ON AND POWER-OFF OPERATION

### Introduction

The graphs in this section show the behavior of  $V_{OUT}$  as  $V_{DD}$  reaches or reduces to less than the required power-on voltage. The same labeling convention for different voltage thresholds is used in Figure 5 and Figure 6. References in brackets “[ ]” are valid for each of these graphs.

### POWER-ON OPERATION

As  $V_{DD}$  ramps up, the  $V_{OUT}$  pin is in a high-impedance (high-Z) state until  $V_{DD}$  increases to greater than  $V_{POR}$  [1]. Once  $V_{DD}$  is greater than  $V_{POR}$  [1],  $V_{OUT}$  enters typical operation and starts to respond to applied current,  $I_P$ .

### POWER-OFF OPERATION

As  $V_{DD}$  reduces to less than  $V_{POR} - V_{POR\_HYS}$ , the outputs enter a high-Z state. The hysteresis on the power-on voltage prevents noise on the supply line from causing  $V_{OUT}$  to repeatedly enter and exit the high-Z state at approximately the  $V_{POR}$  level.

NOTE: Because the device is entering a high-Z state and is not driving the output, the time it takes the output to reach a steady state depends on the external circuitry.

### Voltage Thresholds

#### POWER-ON RESET RELEASE VOLTAGE ( $V_{POR}$ )

If  $V_{DD}$  reduces to less than  $V_{POR} - V_{POR\_HYS}$  [2] while the sensor is in operation, the digital circuitry turns off and the output re-enters a high-Z state. After  $V_{DD}$  recovers and exceeds  $V_{POR}$  [1], the output enters typical operation after a delay of  $t_{PO}$ .

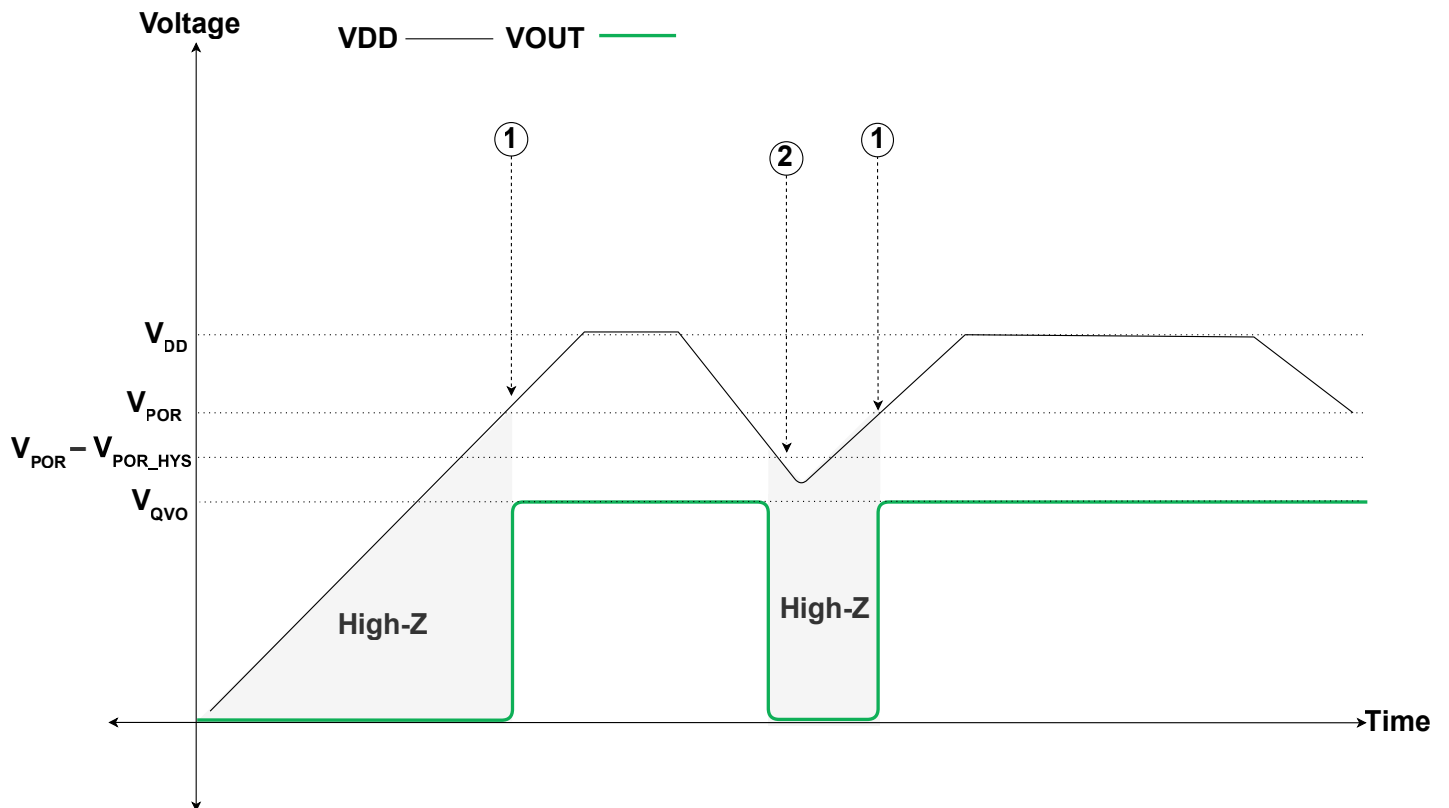


Figure 5: Power-On and Power-Off Operation

### Timing Thresholds

#### POWER-ON DELAY ( $t_{PO}$ )

When the supply voltage reaches  $V_{POR}$  [1], the device requires a finite time to power its internal components before the outputs are released from the high-impedance state and start to respond to the measured current,  $I_P$ . Power-on time,  $t_{PO}$ , is defined as the time it takes for the output voltage to settle within  $\pm 10\%$  of its steady-state value under an applied current,  $I_P$ , which can be observed in Figure 6 as the time from [1] to [A].

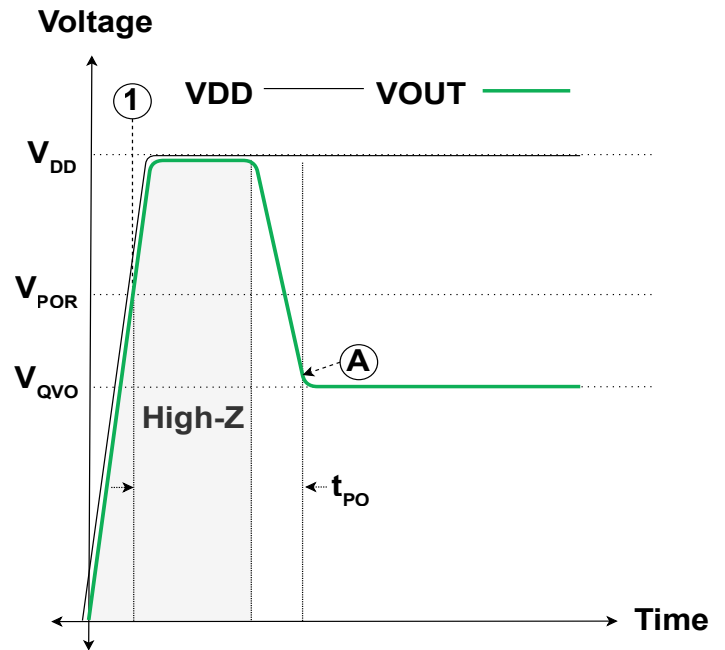


Figure 6: Power-On Delay,  $t_{PO}$

## DEFINITIONS OF OPERATING AND PERFORMANCE CHARACTERISTICS

### Quiescent Voltage Output ( $V_{QVO}$ )

Quiescent voltage output,  $V_{QVO}$ , is defined as the voltage on the output,  $V_{OUT}$ , when current is not applied,  $I_p = 0$ .

### Quiescent Voltage Output Error ( $V_{QVO\_E}$ )

Quiescent voltage output error,  $V_{QVO\_E}$ , is defined as the deviation of  $V_{QVO}$  from the nominal target value in production testing.

### Quiescent Voltage Output Temperature Drift ( $V_{QVO\_T}$ )

Quiescent voltage output temperature drift,  $V_{QVO\_T}$ , is defined as the expected deviation of  $V_{QVO}$  from its value at  $T_A = 25^\circ\text{C}$  throughout the temperature ranges  $T_A = -40^\circ\text{C}$  to  $25^\circ\text{C}$ , and  $T_A = 25^\circ\text{C}$  to  $125^\circ\text{C}$ , based on the observed three-sigma temperature drifts.

### Output Saturation Voltage ( $V_{SAT\_H}$ and $V_{SAT\_L}$ )

Output saturation voltage,  $V_{SAT}$ , is defined as the low or high voltage that  $V_{OUT}$  does not exceed.  $V_{SAT\_H}$  is the highest voltage the output can reach;  $V_{SAT\_L}$  is the lowest.

NOTE: A change in sensitivity does not change the  $V_{SAT}$  points.

### Sensitivity (Sens)

Sensitivity (Sens) is defined as the ratio of the  $V_{OUT}$  swing and the current through the primary conductor,  $I_p$ . The current causes a voltage change on  $V_{OUT}$  away from  $V_{QVO}$  until the  $V_{SAT}$  point is reached. The magnitude and direction of the output voltage is proportional to the magnitude and direction of the current,  $I_p$ . The proportional relationship between output voltage and current is sensitivity, defined as:

$$Sens = \frac{V_{OUT}(I_{P1}) - V_{OUT}(I_{P2})}{I_{P1} - I_{P2}}$$

where  $I_{P1}$  and  $I_{P2}$  are two different currents, and  $V_{OUT}(I_{P1})$  and  $V_{OUT}(I_{P2})$  are the respective output voltages, at  $V_{OUT}$ , at those currents.

### Sensitivity Error ( $E_{SENS}$ )

Sensitivity error,  $E_{SENS}$ , is the deviation of Sensitivity from the nominal sensitivity target value in production testing.

### Sensitivity Temperature Drift ( $E_{SENS\_T}$ )

Sensitivity temperature drift,  $E_{SENS\_T}$ , is defined as the expected deviation of sensitivity from its value at  $T_A = 25^\circ\text{C}$  throughout the temperature ranges  $T_A = -40^\circ\text{C}$  to  $25^\circ\text{C}$ , and  $T_A = 25^\circ\text{C}$  to  $125^\circ\text{C}$ , based on the observed three-sigma temperature drifts.

### Power Supply Sensitivity Error ( $E_{SENS\_PS}$ )

Power supply sensitivity error,  $E_{SENS\_PS}$ , is defined as the percent change in sensitivity when  $V_{DD}$  varies within the specified test voltages.

### Power Supply Offset Error ( $V_{OE\_PS}$ )

Power supply offset error,  $V_{OE\_PS}$ , is defined as the change in  $V_{QVO}$  when  $V_{DD}$  varies within the specified test voltages.

### Noise Density ( $N_D$ )

Noise density,  $N_D$ , is the spectral density of noise, or the square root of noise power per square root hertz.

To calculate the  $A_{RMS}$  for a brick-wall filter approximation, take the provided input noise density,  $N_D$ , and multiply it by the square root of the device or system bandwidth. Input-referred noise density helps to evaluate the sensor performance independent of its sensitivity. For the average noise density of the ACS37041/2 device variants, refer to Figure 7.

$$A_{RMS} = N_D \times \sqrt{BW}$$

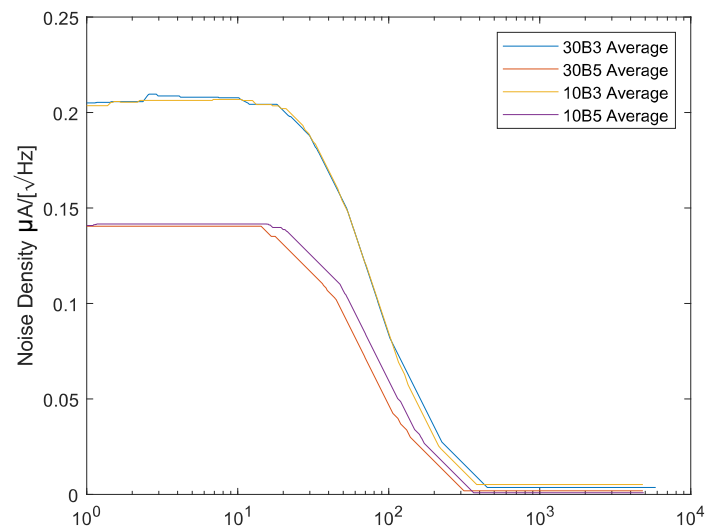


Figure 7: Average Noise Density

### Noise (N)

Noise,  $N$ , is the output-referred noise of the ACS37041/2. This is the total noise at the output of the sensor, and it includes noise sources within the sensor itself.

## THERMAL PERFORMANCE

### Thermal Rise vs. Primary Current

Resistive heating due to the flow of electrical current in the package should be considered during the thermal design of the application. The sensor, printed circuit board (PCB), and contacts to the PCB generate heat and act as a heat sink.

The thermal response is highly dependent on PCB layout, copper thickness, cooling methods, and the profile of the injected current, including peak current, current on-time, and duty cycle.

In-pad vias help improve thermal performance. Placing vias under the copper pads of the current sensor reduces electrical resistance and improves heat conduction to the PCB, while vias outside of the pads limit the current path to the top of the PCB trace and have worse heat-sink capability under the part (see Figure 8 and Figure 9).

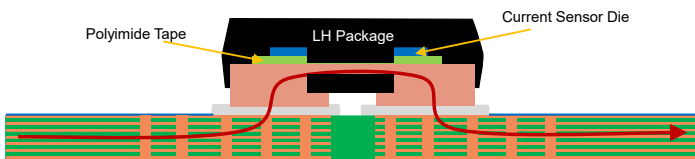


Figure 8: With In-Pad Vias

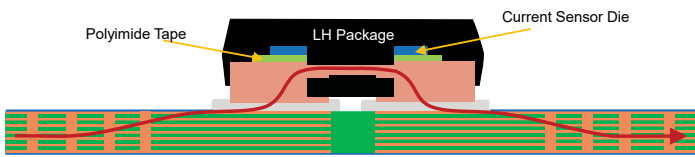


Figure 9: Without In-Pad Vias

The measured increase in steady-state die temperature of the ACS37041/2 versus DC continuous current at an ambient temperature,  $T_A$ , of 25°C, is shown in Figure 10 for two board designs: one with filled vias under copper pads and the other without vias under copper pads.

The measured increase in steady-state die temperature of the ACS37041/2 versus DC continuous current at an ambient temperature of 25°C and 125°C is shown in Figure 11.

The thermal capacity of the ACS37041/2 should be verified by the end user in the application-specific conditions. The maximum junction temperature,  $T_{J(max)}$  (165°C), should not be exceeded. A measurement of the temperature at the top of the package is a close approximation of the die temperature.

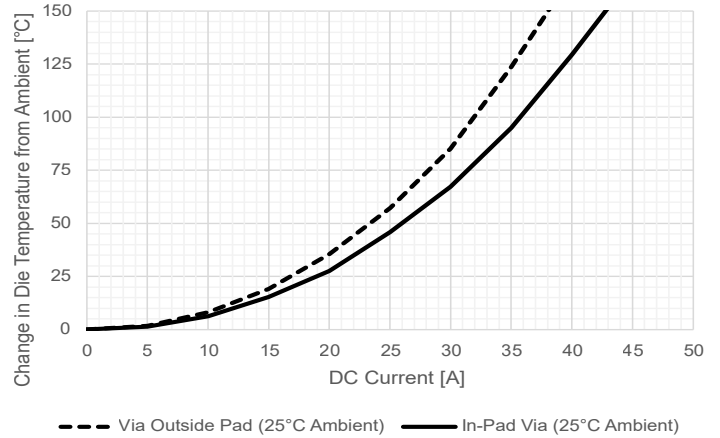


Figure 10: Comparison of Die-Temperature Increase With and Without In-Pad Vias at  $T_A = 25^\circ\text{C}$

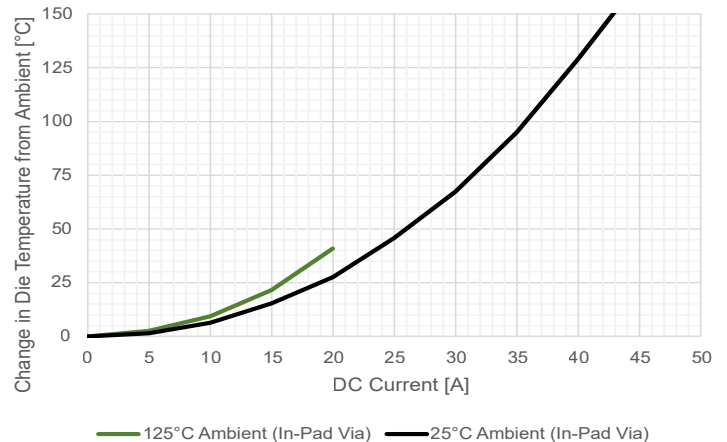
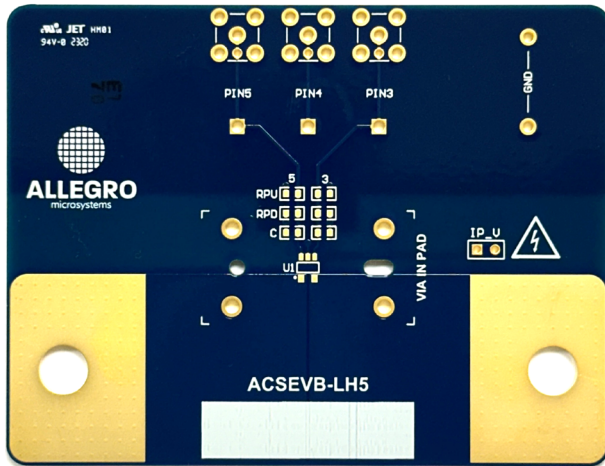


Figure 11: Comparison of Die-Temperature Increase at  $T_A = 25^\circ\text{C}$  and  $T_A = 125^\circ\text{C}$  With In-Pad Vias

### Evaluation Board Layout

Thermal data was collected using the LH current sensor evaluation board (ACSEVB-LH5, TED-0004112) in Figure 12.

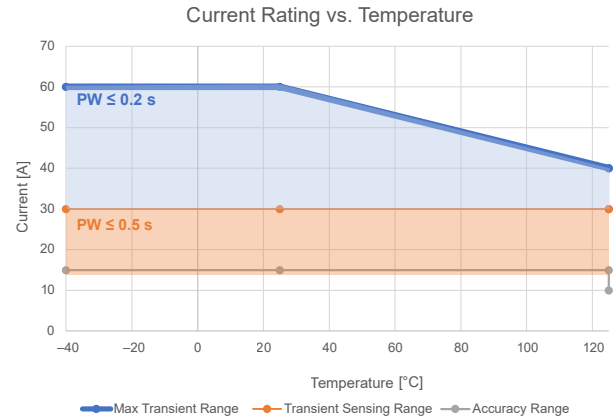


**Figure 12: LH Package Allegro Evaluation Board**

Design support files for the ACSEVB-LH5 evaluation board are available for download from the Allegro website. For more information, see the technical documents section of the ACS37041/2 website.

### CURRENT RANGE VS. TEMPERATURE

From  $-40^{\circ}\text{C}$  to  $25^{\circ}\text{C}$ , there is a rating of up to 60 A for up to 200 ms, and from  $25^{\circ}\text{C}$  to  $125^{\circ}\text{C}$ , there is a rating of up to 60 A to 40 A for up to 200 ms with a derating slope of  $-0.2\text{ A}/^{\circ}\text{C}$ . This range is a statement of allowable current excursions and on-times during transient events, such as overcurrent events.



**Figure 13: Current Ratings vs. Temperature**

## I<sub>P</sub> POWER DISSIPATION OUTPUT DRIFT

### Introduction

Power dissipation in very small packages creates challenges for integrated-conductor current-sensing devices. The ACS37041/2 is in a small, custom SOT23 package designed to minimize the effect of heating due to applied current on the accuracy of the measurement. However, higher applied currents can cause small thermal gradients across the die, which can create a small offset shift. It is important for the system integrator to understand this effect when designing a system using the ACS37041/2.

I<sub>P</sub> power-dissipation is the heat generated by the ohmic loss in the integrated primary conductor (I<sub>P</sub>) when current is applied. The heat generated by the internal conductor spreads through the package unevenly and induces a thermal gradient across the die. A gradient of temperature across the circuitry creates mismatch that results in a change in the signal-path performance. Generation of the thermal gradient is not instantaneous. The offset error of the device due to I<sub>P</sub> power dissipation depends on both the time the current is applied and the square of the current applied. The effect is independent of the direction of the applied current.

### Characteristics of the I<sub>P</sub> Power Dissipation Output Drift

#### POSITIVE APPLIED CURRENT

The ACS37041/2 I<sub>P</sub> power dissipation output drift is shown in Figure 14 through Figure 16 during and after a positive current step is applied to the device.

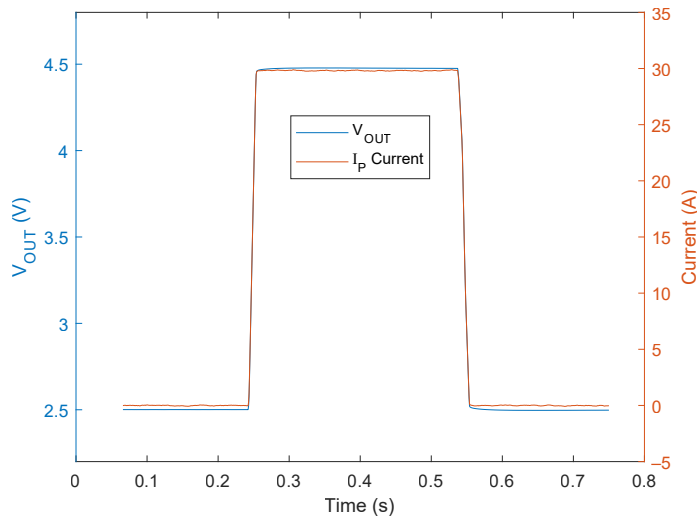


Figure 14: Positive I<sub>P</sub> Pulse, I<sub>P</sub> Power Dissipation Output Drift

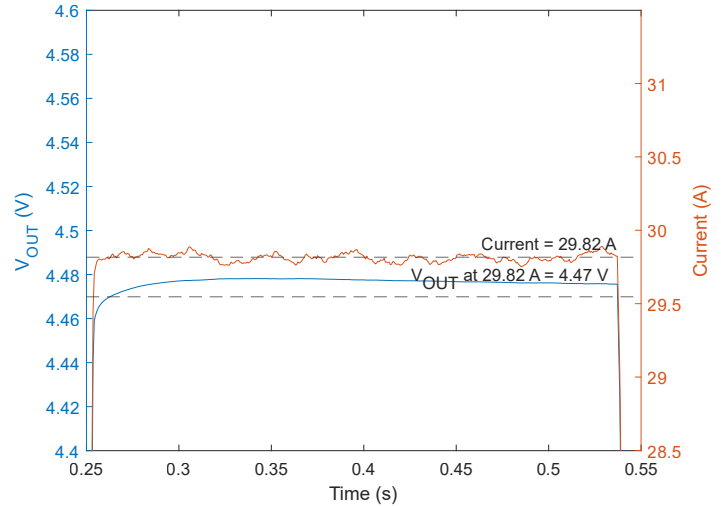


Figure 15: Positive I<sub>P</sub> Pulse, I<sub>P</sub> Power Dissipation Output Drift During Applied Step

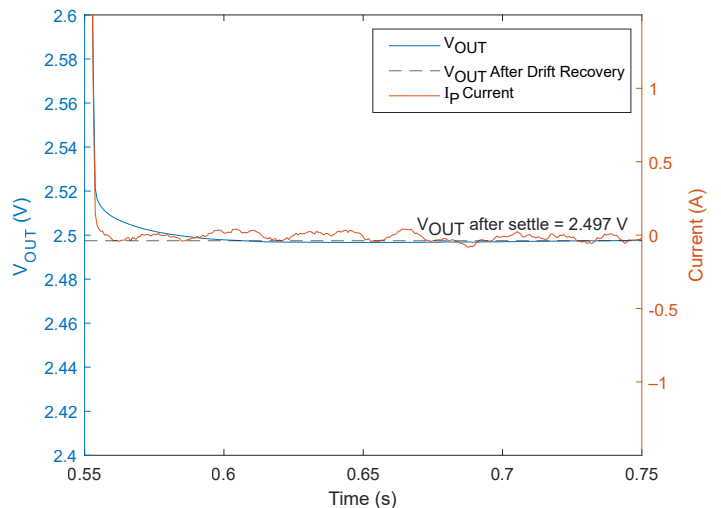


Figure 16: Positive I<sub>P</sub> Pulse, I<sub>P</sub> Power Dissipation Output Drift After Applied Step

### $I_p$ POWER DISSIPATION OUTPUT DRIFT

#### NEGATIVE APPLIED CURRENT

The ACS37041/2  $I_p$  power dissipation output drift is shown in Figure 17 through Figure 19 during and after a negative current step is applied to the device.

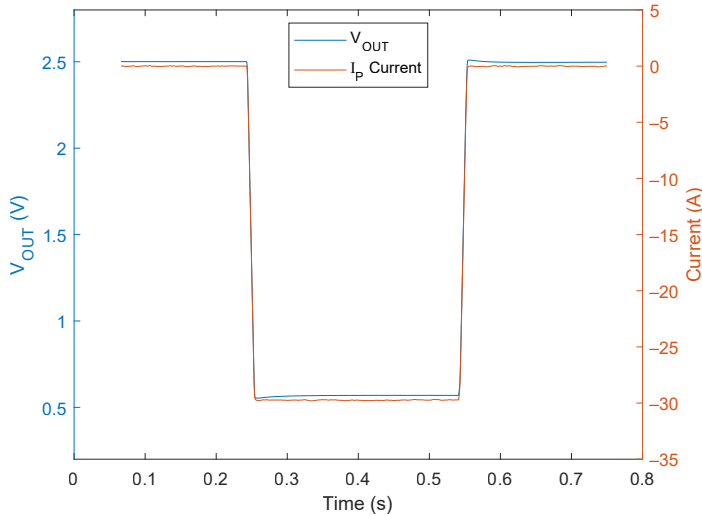


Figure 17: Negative  $I_p$  Pulse,  $I_p$  Power Dissipation Output Drift

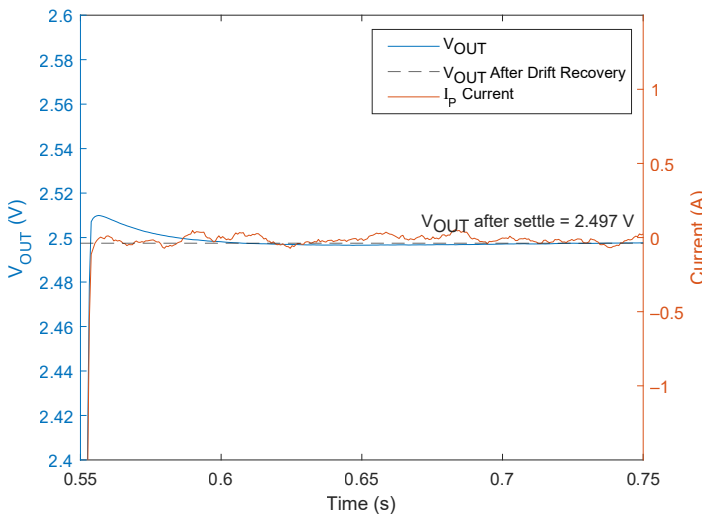


Figure 18: Negative  $I_p$  Pulse,  $I_p$  Power Dissipation Output Drift During Applied Step

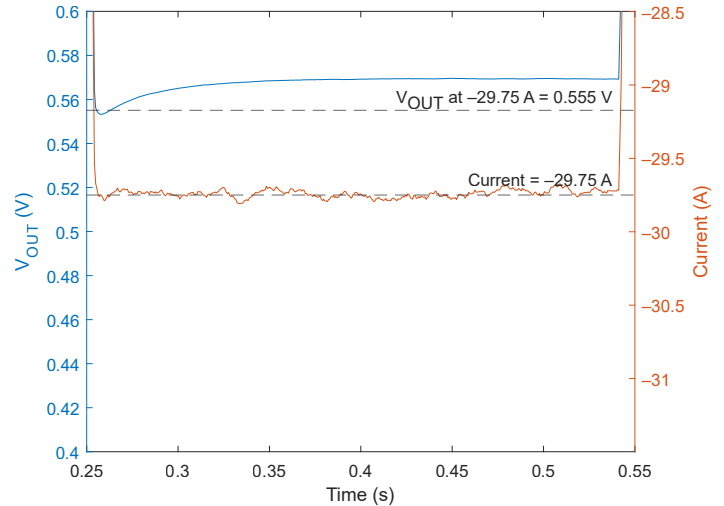


Figure 19: Negative  $I_p$  Pulse,  $I_p$  Power Dissipation Output Drift After Applied Step

#### $I_p$ Power Dissipation Output Drift Description

The impact of the thermal gradient on the circuit is to create an offset in the front-end amplifier. Because the drift occurs before any amplification, the signal-path gain affects the amount of mV of error observed at the output due to this heating effect; however, it is consistent in mA error when input referred. Values in this document are input referred. To determine the effect on a specific ACS37041/2 variant, adjust the error reported by the gain of the sensor.

As the ambient temperature increases, the  $I_p$  power dissipation drift also increases. This is due to changes in resistance over temperature that are inherent to the copper internal conductor. Additionally, the thermal transmissivity of the integrated conductor, solder, and PCB pads decrease over temperature such that the system takes more time to reach a steady state at higher temperature.

#### Recommended Use Cases

To achieve the accuracy specifications in the performance characteristics table, use of the ACS37041/2 for systems with steady-state current operation is recommended at less than 15 A. Although the ACS37041/2 can measure currents up to 30 A, currents in excess of 15 A are recommended to be limited to short transients of < 1 second.

$I_P$  Power Dissipation Output Drift

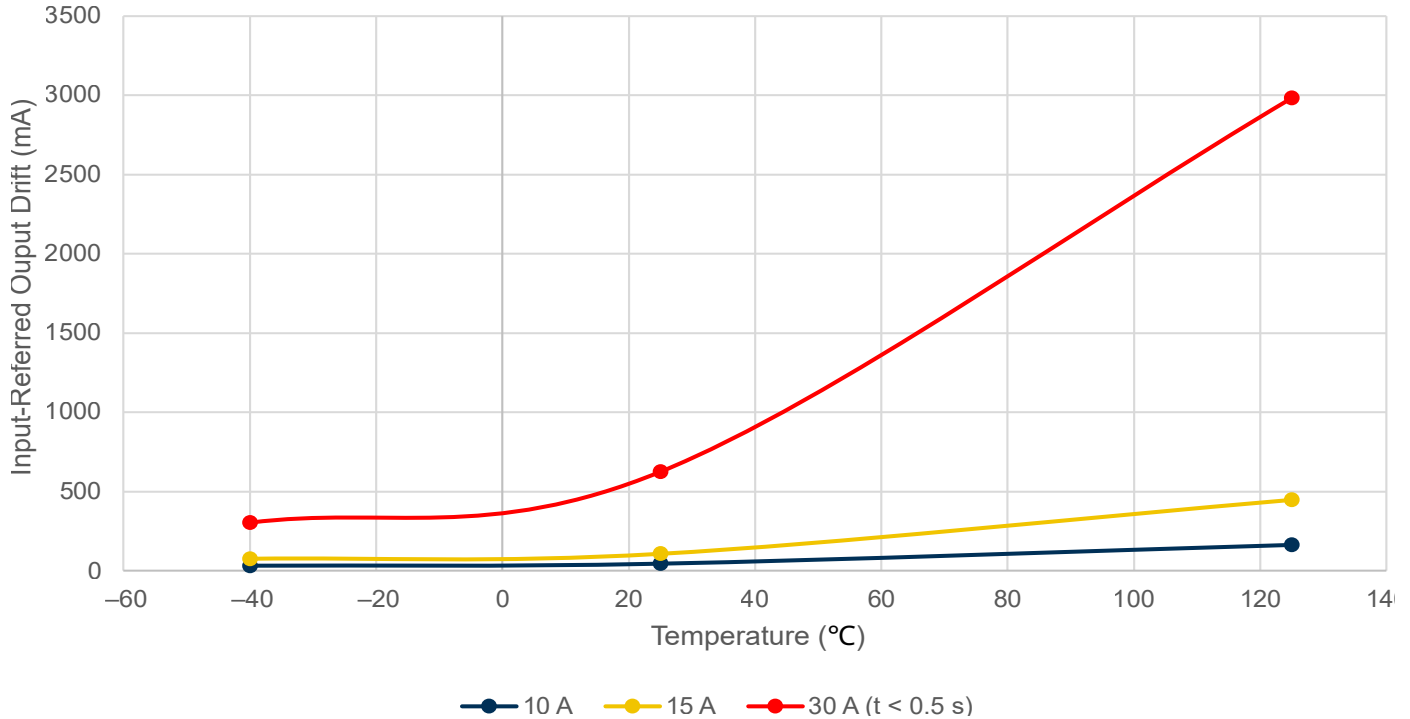


Figure 20: Power Dissipation Output Drift Over Temperature

**$I_P$  Power Dissipation Output Drift Specifications**

Power loss,  $P = I^2R$ , generates heat in alignment with the exponential relationship exhibited by the output-drift dependence of applied current at a specific temperature. Worst-case measurements of 10 devices in bench characterization, where drift behavior is isolated from other sources of error, is shown in Table 1. The ambient temperature affects the integrated current loop resistance in a relationship that aligns with the data shown in Table 1. This indicates the presence of a scaling effect over temperature (refer to Figure 20). For accurate results, it is critical that the system, including the device and the PCB design, is able to manage this heat. For 10 A or 15 A of applied current, the system reaches a thermal equilibrium across all temperatures, which maintains output drift within 3% of the input signal. For 30 A of applied current, the system exhibits output drift of nearly 10% of the input signal, especially at higher temperatures; this remains true with short-duration on-times.

The layout of the PCB affects the overall system performance in terms of the magnitude and time scales of the  $I_P$  power dissipation output drift. For more information, refer to the Thermal Performance section.

NOTE: Any thermal gradient across the device can create behavior similar to  $I_P$  power dissipation output drift, where the direction is dependent on the direction of the temperature gradient across the die.

Table 1:  $I_P$  Power Dissipation Output Drift Summary

Current [A]	Step Duration [s]	Temperature			Offset (Input Referred)
		-40°C	25°C	125°C	
10	1.5	35	45	165	mA
15	1.5	80	115	450	mA
30	0.5	310	650	2990	mA

PACKAGE OUTLINE DRAWING

For Reference Only – Not for Tooling Use

(PRELIMINARY – Reference Drawing DWG-0000628, Rev. 01)

Dimensions in millimeters – NOT TO SCALE

Dimensions exclusive of mold flash, gate burrs, and dambar protrusions  
Exact case and lead configuration at supplier discretion within limits shown

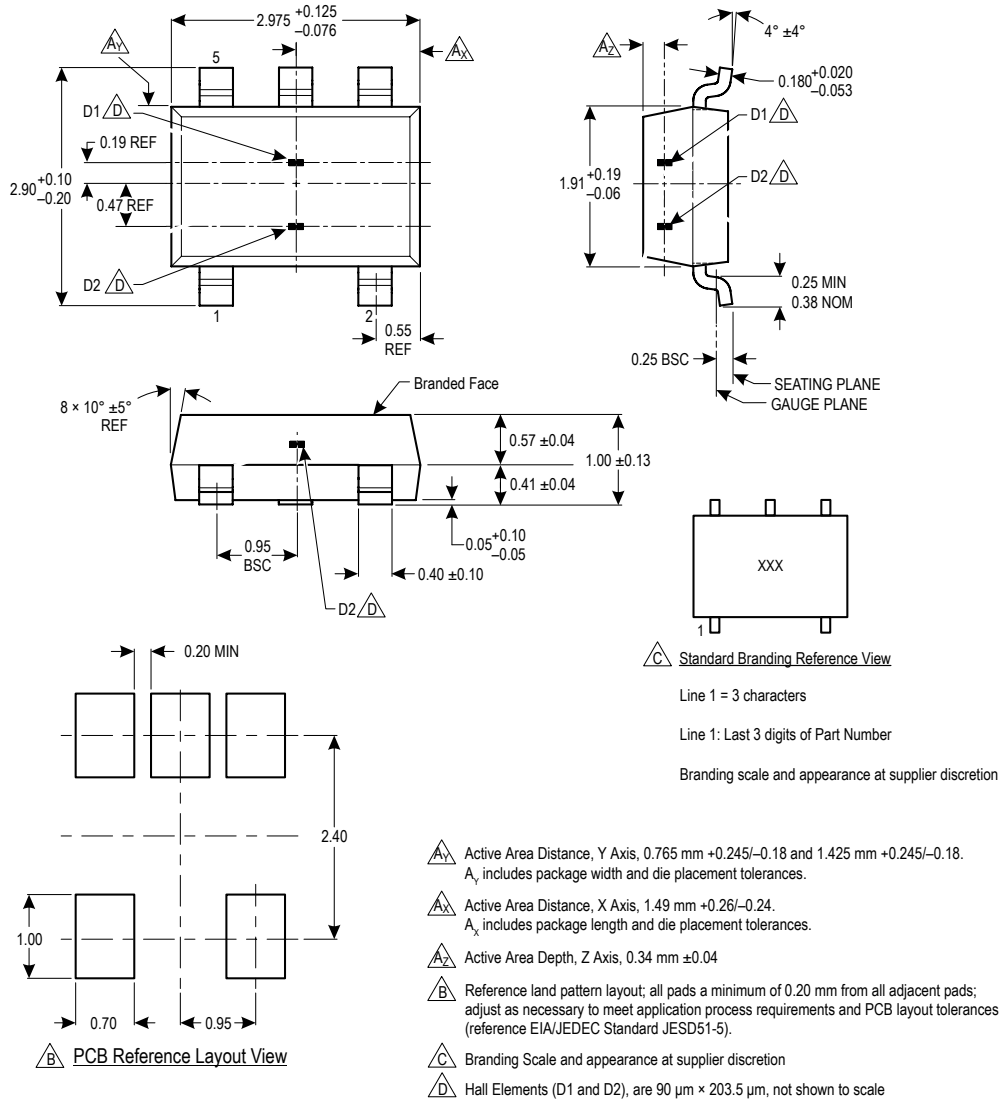


Figure 21: ACS37041 LH 5-Pin SOT23-W Package Drawing

**Revision History**

<b>Number</b>	<b>Date</b>	<b>Description</b>
–	November 1, 2024	Initial release
1	December 13, 2024	Updated the status of the ACS37042 device (pages 1 and 2) and made minor editorial changes throughout
2	February 19, 2025	Updated Features and Benefits (page 1) and Power Dissipation Output Drift Over Temperature figure (page 18)
3	April 30, 2025	Updated Features and Benefits (page 1), corrected MSL rating (page 3), corrected figure numbering (pages 16 through 19), updated Power Dissipation Output Drift Over Temperature figure (page 18), modified product description in headings (all pages), and updated format to support interactive PDF capability (all pages).
4	March 30, 2026	Updated Features and Benefits and Typical Application Circuit (page 1), Selection Guide table (page 2), and minor editorial updates

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