



# BCM<sup>®</sup> Bus Converter

## MBCM270x338M235A00

(Previous Part – VMB0004MFJ)



## Isolated Fixed Ratio DC-DC Converter

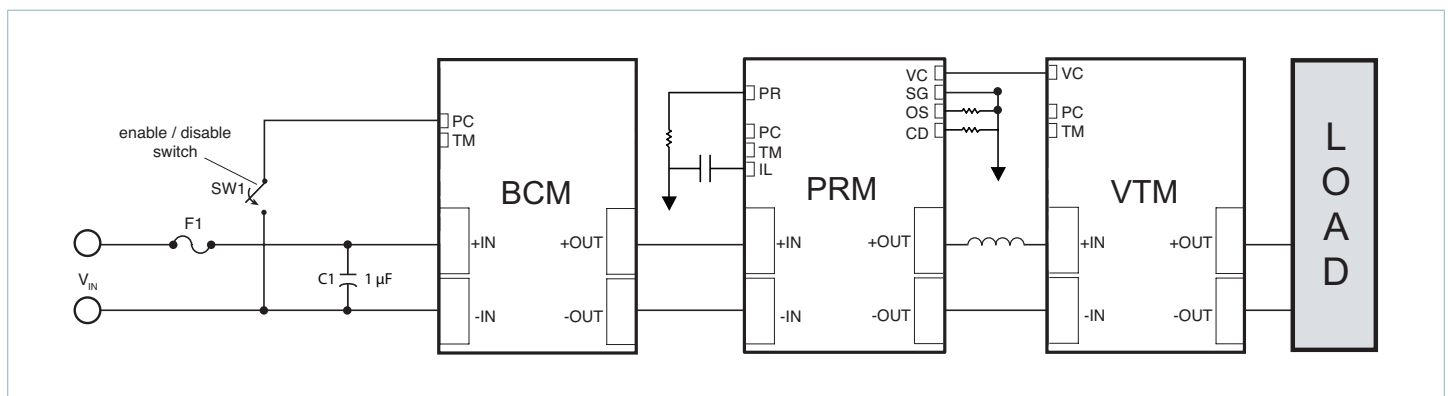
### Features & Benefits

- 270V<sub>DC</sub> – 33.75V<sub>DC</sub> 235W Bus Converter
- MIL-STD-704E/F Compliant
- High efficiency (>95.0%) reduces system power consumption
- High power density (>796W/in<sup>3</sup>) reduces power system footprint by >40%
- Contains built-in protection features against:
  - Undervoltage
  - Overvoltage lockout
  - Overcurrent protection
  - Short Circuit protection
  - Overtemperature protection
- Provides enable/disable control, internal temperature monitoring
- Can be paralleled to create multi-kW arrays

### Typical Applications

- High Voltage 270V Aircraft Distributed Power
- 28V<sub>DC</sub> MIL-COTS PRM<sup>™</sup> Interface (MP028F036M21AL)
- High Density Power Supplies
- Communications Systems

### Typical Application



### Product Ratings

$V_{IN} = 270V (240 - 330V)$	$P_{OUT} = \text{up to } 235W$
$V_{OUT} = 33.75V (30 - 41.25V)$ (NO LOAD)	$K = 1/8$

### Description

The MIL-COTS VI Chip<sup>®</sup> bus converter is a high efficiency (>95.0%) Sine Amplitude Converter<sup>™</sup> (SAC<sup>™</sup>) operating from a 240 to 330V primary bus to deliver an isolated 30 – 41.25V secondary voltage.

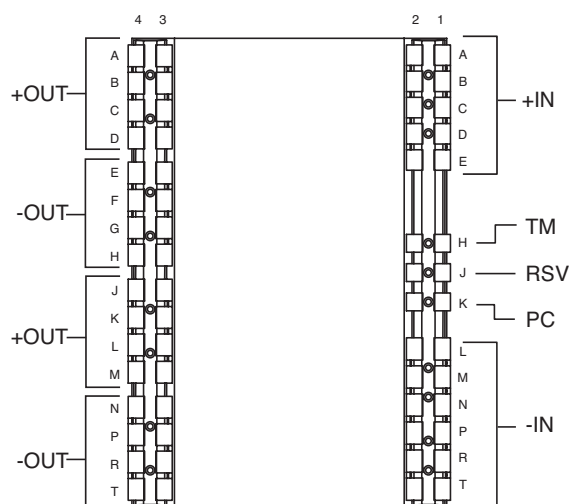
The MBCM270F338M235A00 is provided in a VI Chip package compatible with standard pick-and-place and surface mount assembly processes.

### Part Numbering

Product Number	Package Style (x)	Product Grade
MBCM270x450M270A00	<b>F</b> = J-Lead <b>T</b> = Through hole	<b>M</b> = -55° to 125°C

For Storage and Operating Temperatures see General Characteristics.

## Pin Configuration



Bottom View

## Pin Descriptions

Pin Number	Signal Name	Type	Function
A1-E1, A2-E2	+IN	INPUT POWER	Positive input power terminal
L1-T1, L2-T2	-IN	INPUT POWER RETURN	Negative input power terminal
H1, H2	TM	OUTPUT	Temperature monitor, input side referenced signal
J1, J2	RSV	NC	No connect
K1, K2	PC	OUTPUT/INPUT	Enable and disable control, input side referenced signal
A3-D3, A4-D4, J3-M3, J4-M4	+OUT	OUTPUT POWER	Positive output power terminal
E3-H3, E4-H4, N3-T3, N4-T4	-OUT	OUTPUT POWER RETURN	Negative output power terminal

## Control Pin Specifications

See *Using the Control Signals PC, TM* for more information.

### PC (BCM Primary Control)

The PC pin can enable and disable the BCM module. When held below  $V_{PC\_DIS}$  the BCM shall be disabled. When allowed to float with an impedance to -IN of greater than 50k $\Omega$  the module will start. When connected to another BCM PC pin the BCM modules will start simultaneously when enabled. The PC pin is capable of being driven high either by an external logic signal or internal pull up to 5V (operating).

### TM (BCM Temperature Monitor)

The TM pin monitors the internal temperature of the BCM module within an accuracy of  $\pm 5^{\circ}\text{C}$ . It has a room temperature setpoint of  $\sim 3.0\text{V}$  and an approximate gain of 10mV/ $^{\circ}\text{C}$ . It can source up to 100 $\mu\text{A}$  and may also be used as a "Power Good" flag to verify that the BCM module is operating.

## Absolute Maximum Voltage Ratings

The absolute maximum ratings below are stress ratings only. Operation at or beyond these maximum ratings can cause permanent damage to the device.

Parameter	Comments	Min	Max	Unit
+IN to -IN		-1.0	400	V <sub>DC</sub>
PC to -IN		-0.3	20	V <sub>DC</sub>
TM to -IN		-0.3	7	V <sub>DC</sub>
+IN/-IN to +OUT/-OUT	Isolation voltage (hipot)		4242	V
+IN/-IN to +OUT/-OUT	Working voltage (IN - OUT)		500	V
+OUT to -OUT		-1.0	60	V <sub>DC</sub>
Temperature during reflow	MSL 4 (Datecode 1528 and later)		245	°C

## Electrical Specifications

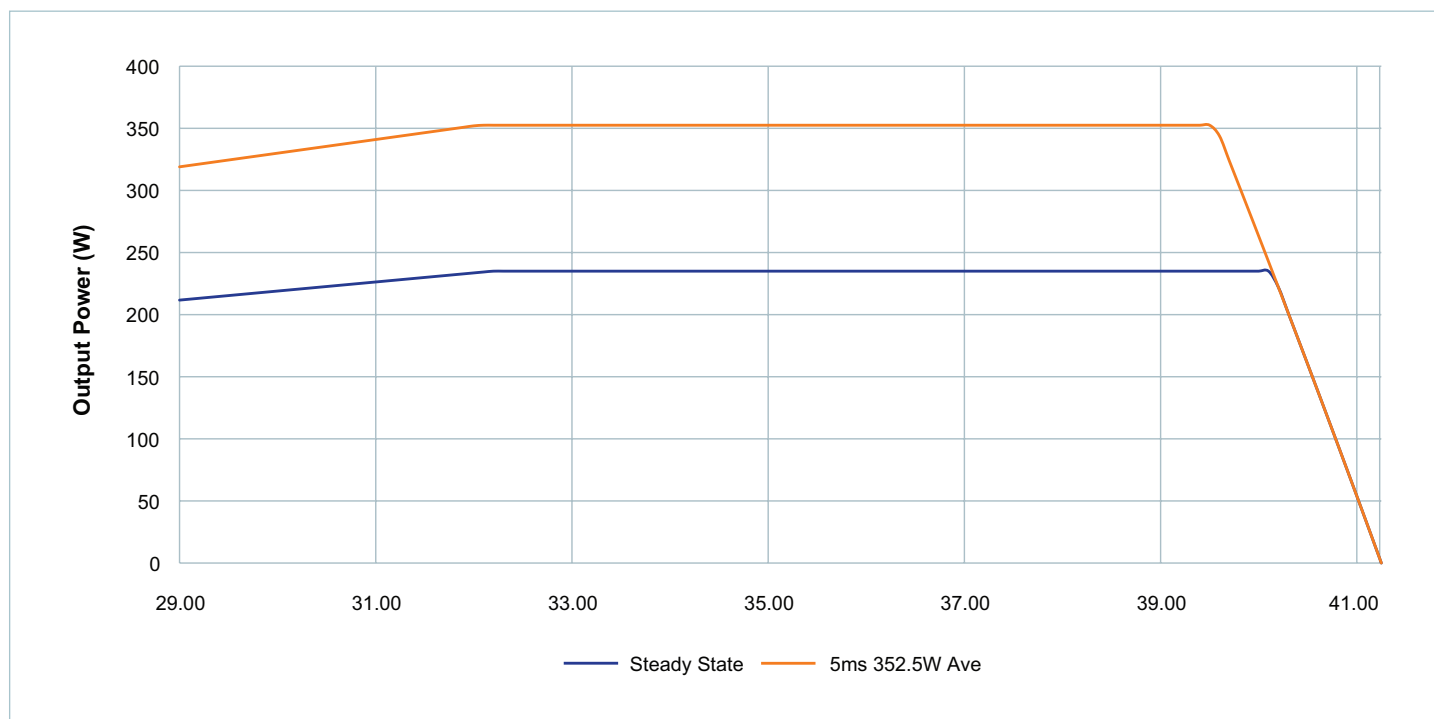
Specifications apply over all line and load conditions, unless otherwise noted; **boldface** specifications apply over the temperature range of  $-55^{\circ}\text{C} \leq T_J \leq 125^{\circ}\text{C}$  (M-Grade); all other specifications are at  $T_J = 25^{\circ}\text{C}$  unless otherwise noted.

Attribute	Symbol	Conditions / Notes	Min	Typ	Max	Unit
<b>Powertrain</b>						
Voltage range	$V_{IN}$		<b>240</b>	<b>270</b>	<b>330</b>	$V_{DC}$
dV/dt	$dV_{IN}/dt$				<b>1</b>	V/ $\mu\text{s}$
Quiescent power	$P_Q$	PC connected to -IN		395	<b>410</b>	mW
No load power dissipation	$P_{NL}$	$V_{IN} = 240$ to $330V$			<b>10</b>	W
Inrush Current Peak	$I_{INR\_P}$	$V_{IN} = 330V$ , $C_{OUT} = 100\mu\text{F}$ , $P_{OUT} = 235W$		2.5	<b>4</b>	A
DC Input Current	$I_{IN\_DC}$	$P_{OUT} = 235W$			<b>0.95</b>	A
K Factor $\left(\frac{V_{OUT}}{V_{IN}}\right)$	K			1/8		
Output Power (Average)	$P_{OUT}$	$V_{IN} = 270V_{DC}$			<b>235</b>	W
		$V_{IN} = 240 - 330V_{DC}$			<b>215</b>	
Output Power (Peak)	$P_{OUT\_P}$	$V_{IN} = 270 V_{DC}$ , Average $P_{OUT} \leq 235W$ , $T_{peak} < 5\text{ms}$			<b>352.5</b>	W
Output Voltage	$V_{OUT}$	No Load	<b>30</b>		<b>41.25</b>	V
Output Current (Average)	$I_{OUT}$	$P_{OUT} \leq 235W$			7.3	A
Efficiency (Ambient)	$\eta$	$V_{IN} = 270V$ , $P_{OUT} = 235W$	94.1	95.4		%
		$V_{IN} = 240V$ to $330V$ , $P_{OUT} = 235W$	94	95.2		
Efficiency (Hot)	$\eta$	$V_{IN} = 270V$ , $T_J = 100^{\circ}\text{C}$ , $P_{OUT} = 235W$	93.7	94.7		%
Minimum Efficiency (Over Load Range)	$\eta$	$60W < P_{OUT} < 235W$ Max	<b>90</b>			%
Output Resistance (Ambient)	$R_{OUT}$	$T_J = 25^{\circ}\text{C}$	100	130	170	$m\Omega$
Output Resistance (Hot)	$R_{OUT}$	$T_J = 125^{\circ}\text{C}$	130	180	210	$m\Omega$
Output Resistance (Cold)	$R_{OUT}$	$T_J = -55^{\circ}\text{C}$	40	105	160	$m\Omega$
Load Capacitance	$C_{OUT}$				<b>100</b>	$\mu\text{F}$
Switching Frequency	$F_{SW}$		<b>1.56</b>	1.64	<b>1.72</b>	MHz
Ripple Frequency	$F_{SW\_RP}$		<b>3.12</b>	3.28	<b>3.44</b>	MHz
Output Voltage Ripple	$V_{OUT\_PP}$	$C_{OUT} = 0\mu\text{F}$ , $P_{OUT} = 235W$ , $V_{IN} = 270V$		160	<b>400</b>	mV
$V_{IN}$ to $V_{OUT}$ (Application of $V_{IN}$ )	$T_{ON1}$	$V_{IN} = 270V$ , $C_{PC} = 0$	460	540	620	ms

## Electrical Specifications

Specifications apply over all line and load conditions, unless otherwise noted; **boldface** specifications apply over the temperature range of  $-55^{\circ}\text{C} \leq T_J \leq 125^{\circ}\text{C}$  (M-Grade); all other specifications are at  $T_J = 25^{\circ}\text{C}$  unless otherwise noted.

Attribute	Symbol	Conditions / Notes	Min	Typ	Max	Unit
<b>Protection</b>						
Input overvoltage recovery threshold	$V_{IN\_OVLO-}$		<b>350</b>	365	<b>380</b>	V
Input overvoltage lockout threshold	$V_{IN\_OVLO+}$		<b>355</b>	372	<b>385</b>	V
Input undervoltage lockout threshold	$V_{IN\_UVLO-}$		<b>90</b>	115	<b>125</b>	V
Input undervoltage recovery threshold	$V_{IN\_UVLO+}$		<b>100</b>	125	<b>135</b>	V
Output overcurrent trip	$I_{OCP}$	$V_{IN} = 270\text{V}, 25^{\circ}\text{C}$	<b>9</b>	12	<b>14</b>	A
Short circuit protection trip threshold	$I_{SCP}$		<b>14</b>			A
Short circuit protection response time constant	$T_{SCP}$		<b>0.8</b>	1	<b>1.2</b>	$\mu\text{s}$
Thermal shutdown threshold	$T_{J\_OTP}$		<b>125</b>	130	<b>135</b>	$^{\circ}\text{C}$



**Figure 1** — Safe operating area

## Signal Characteristics

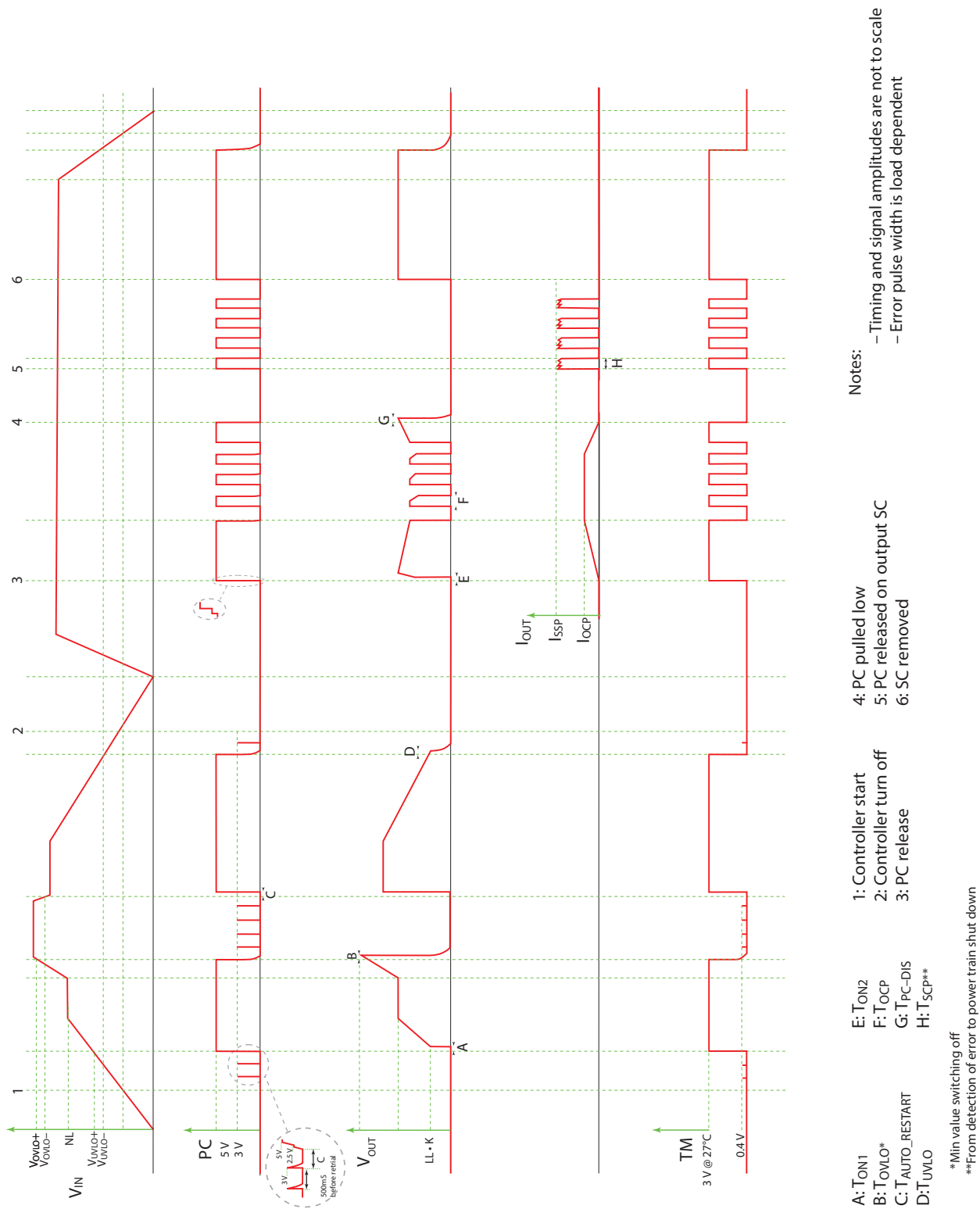
Specifications apply over all line and load conditions, unless otherwise noted; **boldface** specifications apply over the temperature range of  $-55^{\circ}\text{C} \leq T_J \leq 125^{\circ}\text{C}$  (M-Grade); all other specifications are at  $T_J = 25^{\circ}\text{C}$  unless otherwise noted.

Primary Control: PC						
<ul style="list-style-type: none"> <li>The PC pin enables and disables the BCM. When held low, the BCM module is disabled.</li> <li>In an array of BCM modules, PC pins should be interconnected to synchronize start up and permit start up into full load conditions.</li> <li>PC pin outputs 5V during normal operation. PC pin internal bias level drops to 2.5V during fault mode, provided <math>V_{IN}</math> remains in the valid range.</li> </ul>						
Attribute	Symbol	Conditions / Notes	Min	Typ	Max	Unit
PC Voltage (Operating)	$V_{PC}$		<b>4.7</b>	5	<b>5.3</b>	V
PC Voltage (Enable)	$V_{PC\_EN}$		<b>2</b>	2.5	<b>3</b>	V
PC Voltage (Disable)	$V_{PC\_DIS}$				<b>1.95</b>	V
PC Source Current (Startup)	$I_{PC\_EN}$		<b>50</b>	100	<b>300</b>	$\mu\text{A}$
PC Source Current (Operating)	$I_{PC\_OP}$		<b>2</b>	3.5	<b>5</b>	mA
PC Internal Resistance	$R_{PC\_SNK}$	Internal pull down resistor	<b>50</b>	150	<b>400</b>	k $\Omega$
PC Capacitance (Internal)	$C_{PC\_INT}$				1000	pF
PC Capacitance (External)	$C_{PC\_EXT}$	External capacitance delays PC enable time			1000	pF
External PC Resistance	$R_{PC}$	Connected to $-V_{IN}$	<b>50</b>			k $\Omega$
PC External Toggle Rate	$F_{PC\_TOG}$				<b>1</b>	Hz
PC to $V_{OUT}$ with PC Released	$T_{ON2}$	$V_{IN} = 270\text{V}$ , Pre-applied, $C_{PC} = 0$ , $C_{OUT} = 0$	50	100	150	$\mu\text{s}$
PC to $V_{OUT}$ , Disable PC	$T_{PC\_DIS}$	$V_{IN} = 270\text{V}$ , Pre-applied, $C_{PC} = 0$ , $C_{OUT} = 0$		4	10	$\mu\text{s}$

Temperature Monitor: TM						
<ul style="list-style-type: none"> <li>The TM pin monitors the internal temperature of the controller IC within an accuracy of <math>\pm 5^{\circ}\text{C}</math>.</li> <li>Can be used as a "Power Good" flag to verify that the BCM module is operating.</li> <li>Is used to drive the internal comparator for Overtemperature Shutdown.</li> </ul>						
Attribute	Symbol	Conditions / Notes	Min	Typ	Max	Unit
TM accuracy	$A_{TM}$		<b>-5</b>		<b>+5</b>	$^{\circ}\text{C}$
TM Gain	$A_{TM}$			10		mV/ $^{\circ}\text{C}$
TM Source Current	$I_{TM}$				<b>100</b>	$\mu\text{A}$
TM Internal Resistance	$R_{TM\_SNK}$		<b>25</b>	40	<b>50</b>	k $\Omega$
External TM Capacitance	$C_{TM}$				<b>50</b>	pF
TM Voltage Ripple	$V_{TM\_PP}$	$C_{TM} = 0\mu\text{F}$ , $V_{IN} = 330\text{V}$ , $P_{OUT} = 235\text{W}$	<b>200</b>	400	<b>500</b>	mV

Reserved: RSV						
Reserved for factory use. No connection should be made to this pin.						

Timing Diagram



## Applications Characteristics

All specifications are at  $T_J = 25^\circ\text{C}$  unless otherwise noted. See associated figures for general trend data.

Attribute	Symbol	Conditions / Notes	Min	Typ	Max	Unit
No Load Power	$P_{NL}$	$V_{IN} = 270\text{V}$ , PC enabled		5.5		W
Inrush Current Peak	$I_{NR\_P}$	$C_{OUT} = 100\mu\text{F}$ , $P_{OUT} = 235\text{W}$		2.5		A
Efficiency (Ambient)	$\eta$	$V_{IN} = 270\text{V}$ , $P_{OUT} = 235\text{W}$		95.4		%
Efficiency (Hot – $100^\circ\text{C}$ )	$\eta$	$V_{IN} = 270\text{V}$ , $P_{OUT} = 235\text{W}$		94.7		%
Output Resistance ( $-55^\circ\text{C}$ )	$R_{OUT}$	$V_{IN} = 270\text{V}$		105		$\text{m}\Omega$
Output Resistance ( $25^\circ\text{C}$ )	$R_{OUT}$	$V_{IN} = 270\text{V}$		130		$\text{m}\Omega$
Output Resistance ( $120^\circ\text{C}$ )	$R_{OUT}$	$V_{IN} = 270\text{V}$		180		$\text{m}\Omega$
Output Voltage Ripple	$V_{OUT\_PP}$	$C_{OUT} = 0\mu\text{F}$ , $P_{OUT} = 235\text{W}$ @ $V_{IN} = 270$ , $V_{IN} = 270\text{V}$		160		mV
$V_{OUT}$ Transient (Positive)	$V_{OUT\_TRAN+}$	$I_{OUT\_STEP} = 0$ TO $7.3\text{A}$ , $I_{SLEW} > 10\text{A}/\mu\text{s}$		1.4		V
$V_{OUT}$ Transient (Negative)	$V_{OUT\_TRAN-}$	$I_{OUT\_STEP} = 7.3\text{A}$ to $0\text{A}$ , $I_{SLEW} > 10\text{A}/\mu\text{s}$		1.3		V
Undervoltage Lockout Response Time	$T_{UVLO}$			150		$\mu\text{s}$
Output Overcurrent Response Time	$T_{OCP}$	$9 < I_{OCP} < 14\text{A}$		5		ms
Overvoltage Lockout Response Time	$T_{OVLO}$			120		$\mu\text{s}$
TM Voltage (Ambient)	$V_{TM\_AMB}$	$T_J \approx 27^\circ\text{C}$		3		V



## Application Characteristics

The following values, typical of an application environment, are collected at  $T_{CASE} = 25^{\circ}\text{C}$  unless otherwise noted. See associated figures for general trend data.

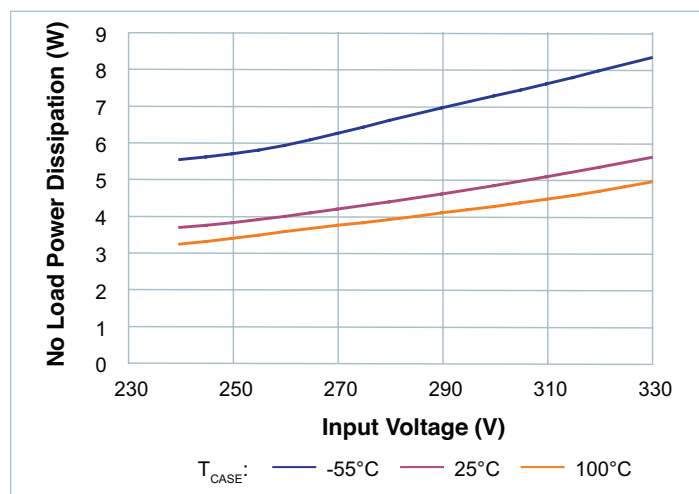


Figure 2 — No load power dissipation vs.  $V_{IN}$ ;  $T_{CASE}$

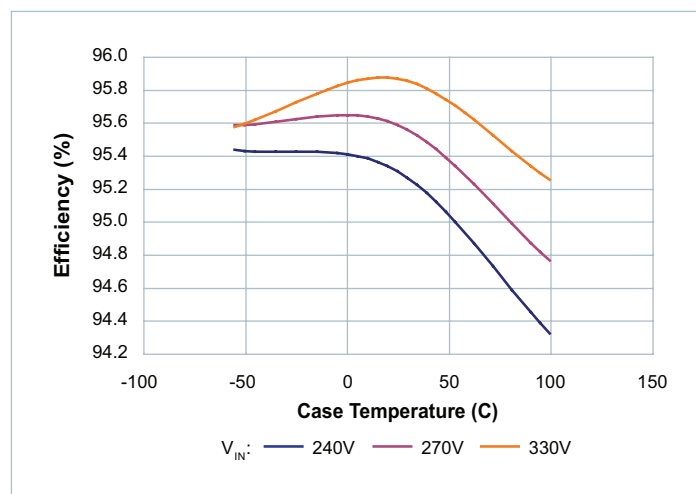


Figure 3 — Full load efficiency vs. temperature;  $V_{IN}$

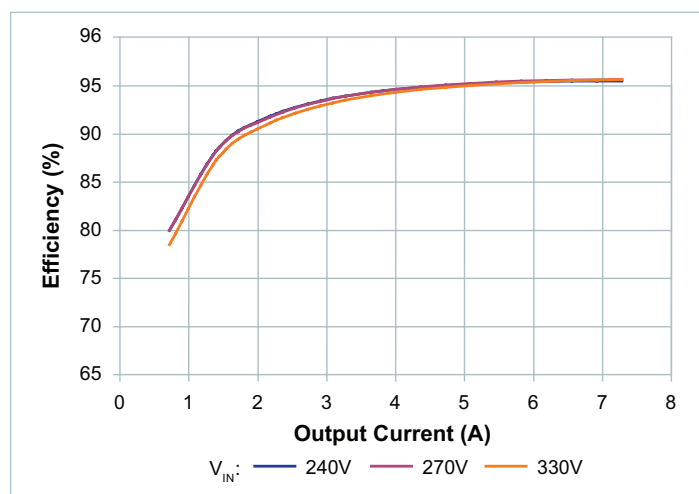


Figure 4 — Efficiency at  $T_{CASE} = -55^{\circ}\text{C}$

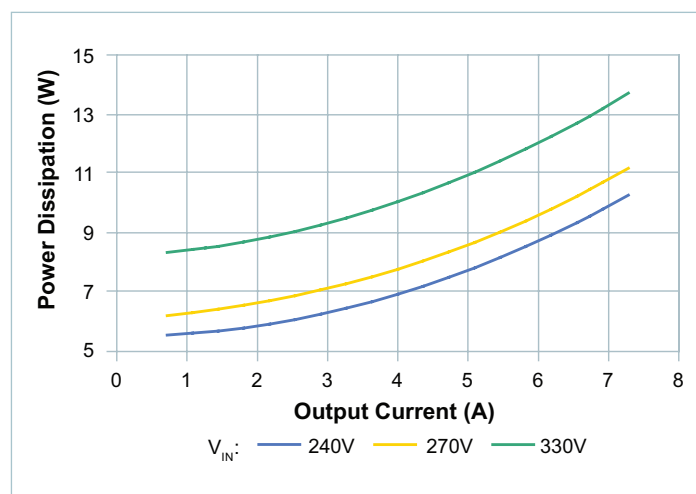


Figure 5 — Power dissipation at  $T_{CASE} = -55^{\circ}\text{C}$

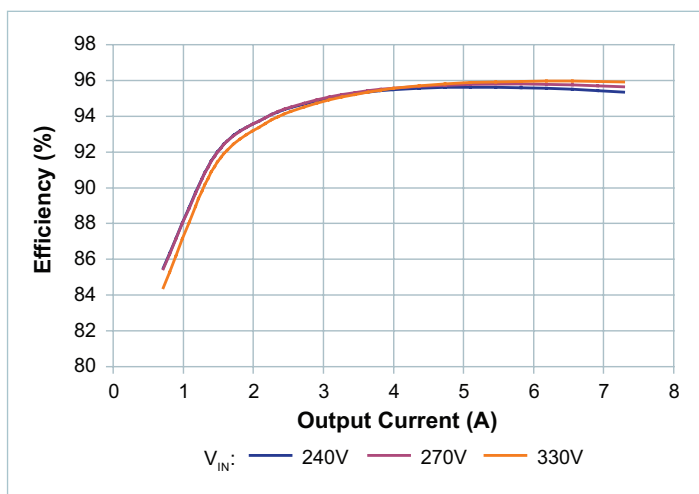


Figure 6 — Efficiency at  $T_{CASE} = 25^{\circ}\text{C}$

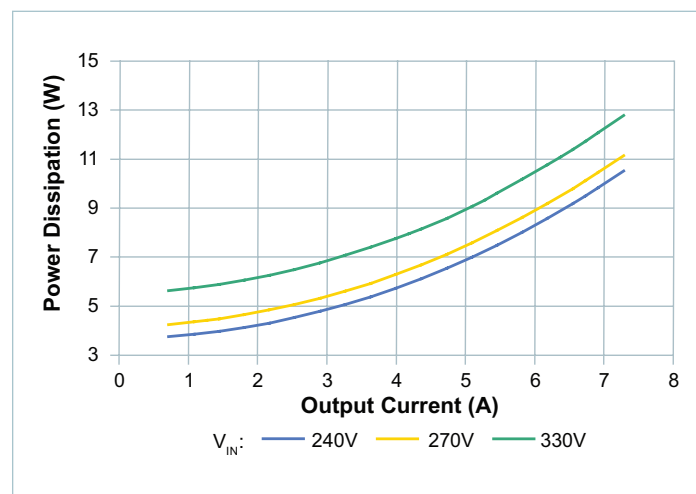
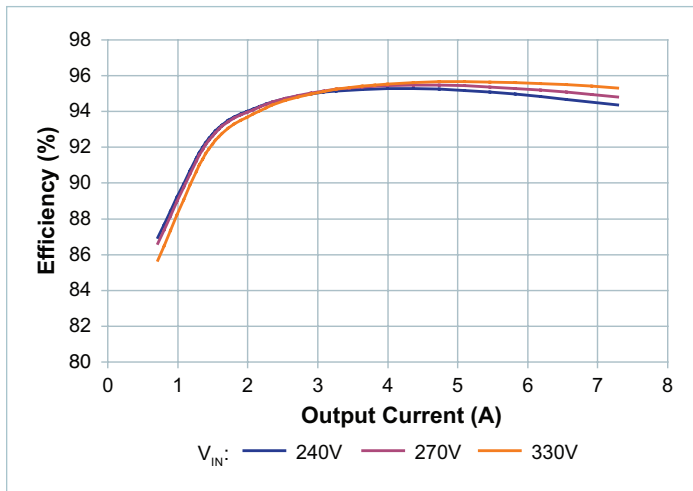
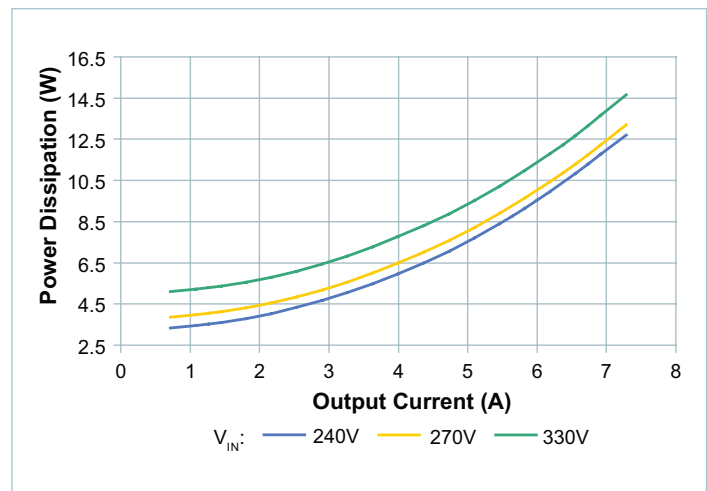
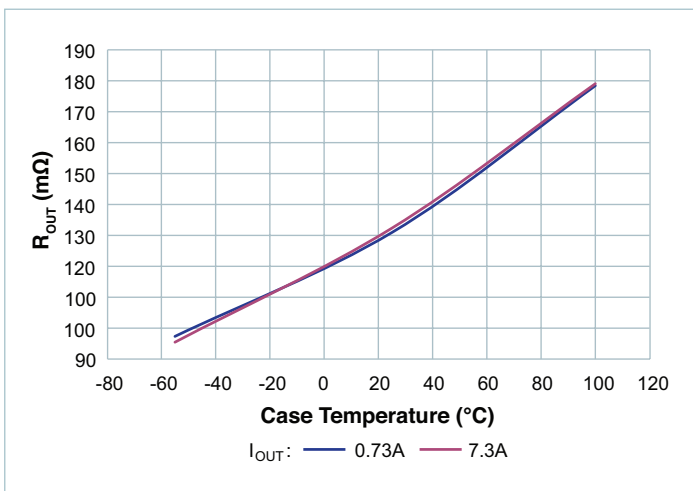
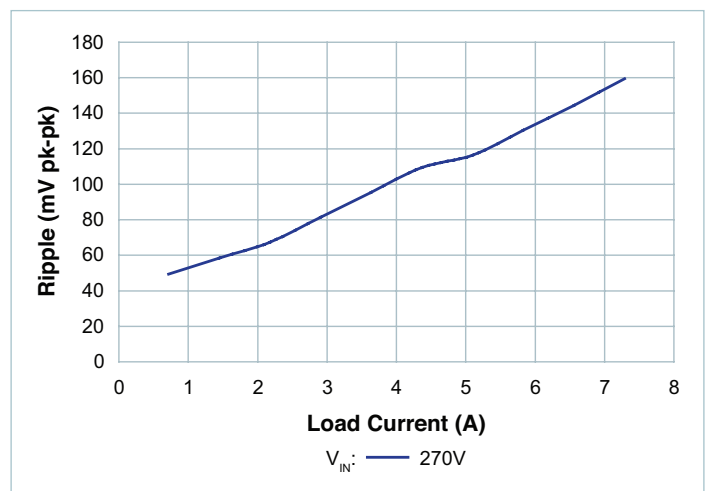
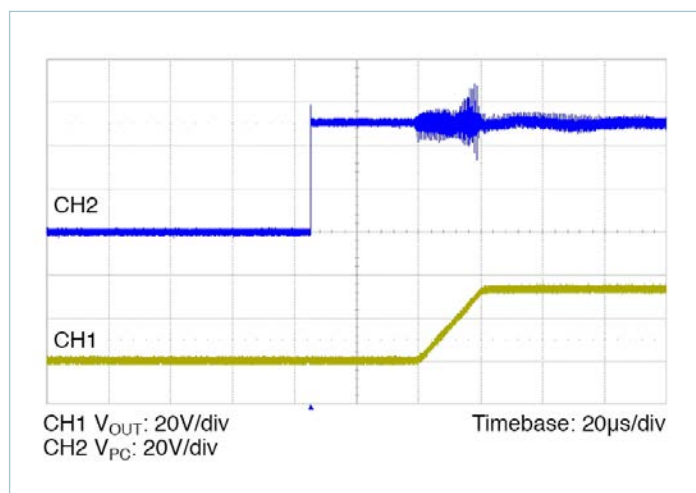
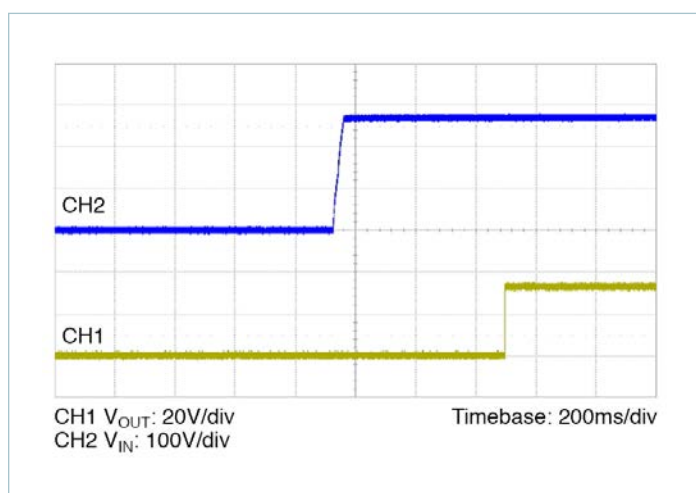
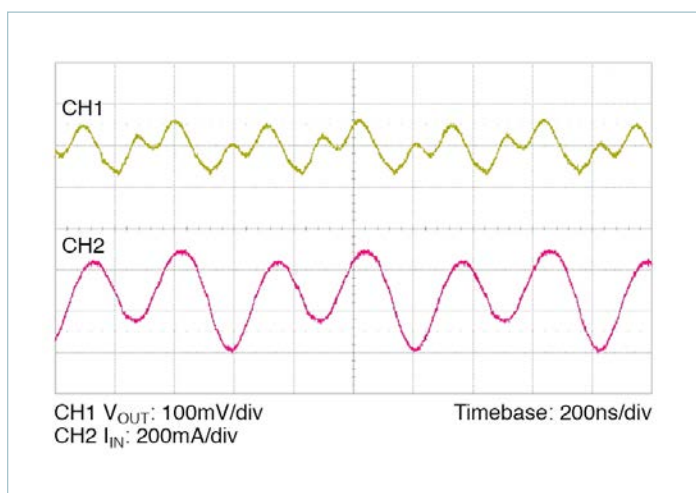
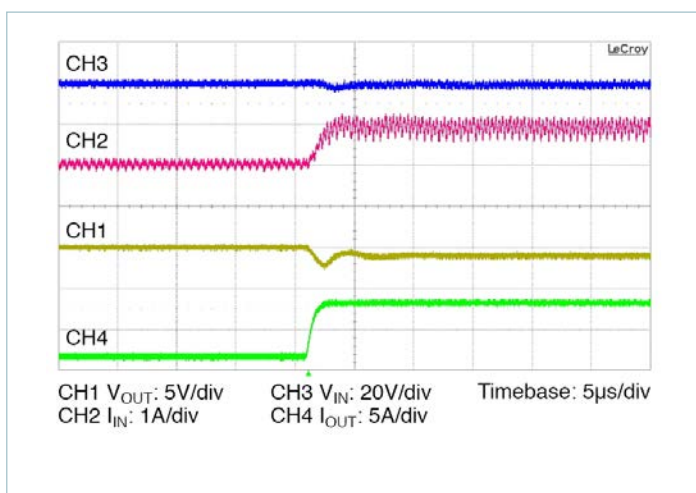
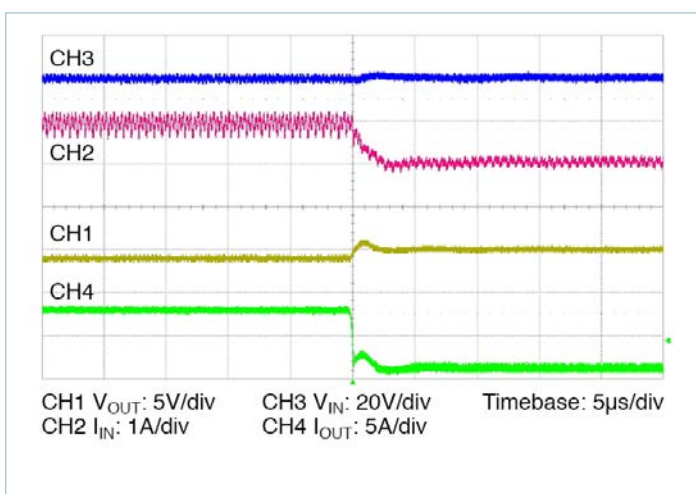
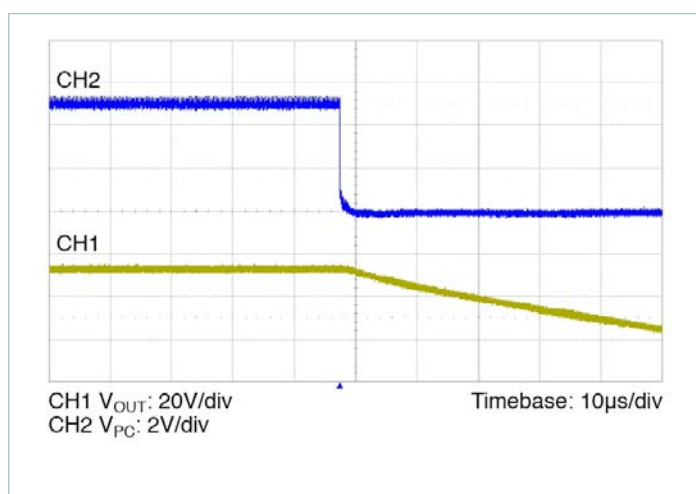


Figure 7 — Power dissipation at  $T_{CASE} = 25^{\circ}\text{C}$

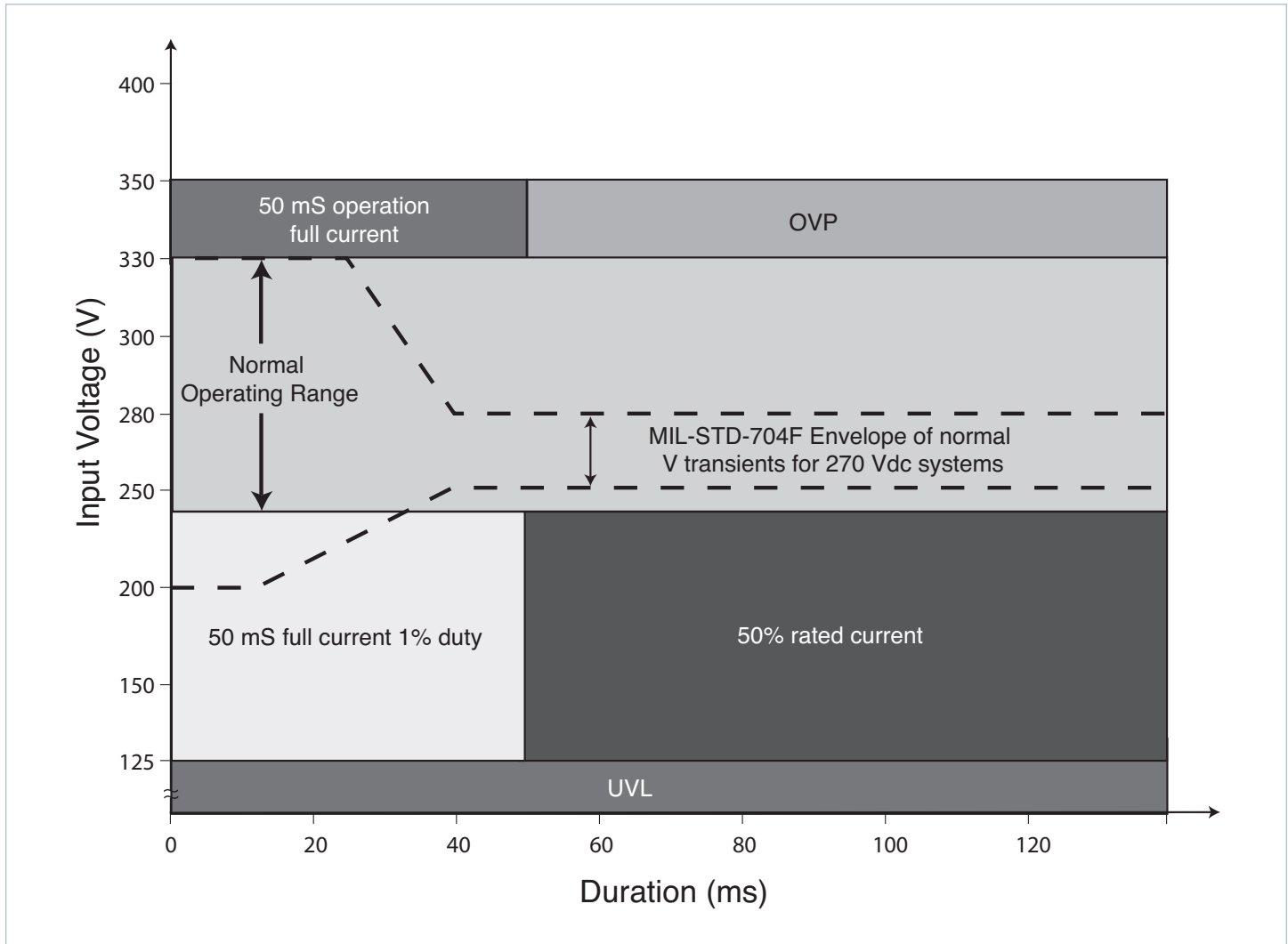
## Application Characteristics (Cont.)

Figure 8 — Efficiency at  $T_{CASE} = 100^{\circ}C$ Figure 9 — Power dissipation at  $T_{CASE} = 100^{\circ}C$ Figure 10 —  $R_{OUT}$  vs. temperature; nominal inputFigure 11 —  $V_{RIPPLE}$  vs.  $I_{OUT}$ ; no external  $C_{OUT}$ . Board mounted module, scope setting: 20MHz analog BW

## Application Characteristics (Cont.)

Figure 12 — Start up from applicaiton of PC;  $V_{IN}$  preapplid  $C_{OUT}$ Figure 13 — Start up from applicaiton of  $V_{IN}$ Figure 14 — Full load ripple, 100µF  $C_{IN}$ ; no external  $C_{OUT}$ . Board mounted module, scope setting: 20MHz analog BWFigure 15 — 0A - 7.3A transient response.  $C_{IN} = 100\mu F$ , no external  $C_{OUT}$ Figure 16 — 7.3A - 0A transient response.  $C_{IN} = 100\mu F$ , no external  $C_{OUT}$ Figure 17 — PC disable waveform, 270V<sub>IN</sub>, 100µF  $C_{OUT}$  full load

## Application Characteristics (Cont.)



**Figure 18** — Envelope of normal voltage transient for 270V<sub>DC</sub> system.

## General Characteristics

Specifications apply over all line and load conditions, unless otherwise noted; **boldface** specifications apply over the temperature range of  $-55^{\circ}\text{C} \leq T_J \leq 125^{\circ}\text{C}$  (M-Grade); all other specifications are at  $T_J = 25^{\circ}\text{C}$  unless otherwise noted.

Attribute	Symbol	Conditions / Notes	Min	Typ	Max	Unit
Mechanical						
Length	L		32.4 / [1.27]	32.5 / [1.28]	32.6 / [1.29]	mm / [in]
Width	W		21.7 / [0.85]	22.0 / [0.87]	22.3 / [0.89]	mm / [in]
Height	H		6.48 / [0.255]	6.73 / [0.265]	6.98 / [0.275]	mm / [in]
Volume	Vol	No heat sink		4.81 / [0.295]		cm <sup>3</sup> / [in <sup>3</sup> ]
Footprint	F	No heat sink		7.3 / [1.1]		cm <sup>2</sup> / [in <sup>2</sup> ]
Power Density	P <sub>D</sub>	No heat sink		796		W/in <sup>3</sup>
				49		W/cm <sup>3</sup>
Weight	W			14 / [0.5]		g / [oz]
Lead Finish		Nickel (0.51-2.03μm)				μm
		Palladium (0.02-0.15μm)				
		Gold (0.003-0.05μm)				
Thermal						
Operating temperature	T <sub>J</sub>		-55		125	°C
Storage Temperature	T <sub>ST</sub>		-65		125	°C
Thermal Impedance	Ø <sub>JC</sub>	Min Board Heat sinking		1.1	1.5	°C/W
Thermal Capacity				9		Ws/°C
Assembly						
Peak Compressive Force Applied to Case (Z-axis)		No J-lead support		5	6	lbs
ESD Rating	ESD <sub>HBM</sub>	Human Body Model, JEDEC JESD 22-A114c.01	1500			V <sub>DC</sub>
	ESD <sub>MM</sub>	Machine Model, JEDEC JESD 22-A115-A	400			
Soldering						
Peak Temperature During Reflow		MSL 4 (Datecode 1528 and later)			245	°C
Peak Time Above 183°C					150	s
Peak Heating Rate During Reflow				1.5	3	°C/s
Peak Cooling Rate Post Reflow				1.5	6	°C/s
Safety						
Working voltage (IN – OUT)	V <sub>WORKING</sub>				500	V
Isolation voltage (hipot)	V <sub>HIPOT</sub>		4242			V
Isolation capacitance	C <sub>IN_OUT</sub>	Unpowered unit	500	660	800	pF
Isolation resistance	R <sub>IN_OUT</sub>		10			MΩ
MTBF		MIL HDBK 217F, 25°C, GB		4.2		MHrs
Agency approvals / standards		cTUVus				
		cURus				
		CE Marked for Low Voltage Directive and ROHS recast directive, as applicable.				

## Using the Control Signals PC, TM

**Primary Control (PC)** pin can be used to accomplish the following functions:

- **Logic enable and disable for module:** Once  $T_{ON1}$  time has been satisfied, a PC voltage greater than  $V_{PC\_EN}$  will cause the module to start. Bringing PC lower than  $V_{PC\_DIS}$  will cause the module to enter standby.
- **Auxiliary voltage source:** Once enabled in regular operational conditions (no fault), each BCM module PC provides a regulated 5V, 3.5mA voltage source.
- **Synchronized start up:** In an array of parallel modules, PC pins should be connected to synchronize start up across units. This permits the maximum load and capacitance to scale by the number of paralleled modules.
- **Output disable:** PC pin can be actively pulled down in order to disable the module. Pull down impedance shall be lower than  $60\Omega$ .
- **Fault detection flag:** The PC 5V voltage source is internally turned off as soon as a fault is detected.
- Note that PC can not sink significant current during a fault condition. The PC pin of a faulted module will not cause interconnected PC pins of other modules to be disabled.

**Temperature Monitor (TM)** pin provides a voltage proportional to the absolute temperature of the converter control IC.

It can be used to accomplish the following functions:

- **Monitor the control IC temperature:** The temperature in Kelvin is equal to the voltage on the TM pin scaled by 100. (i.e.  $3.0V = 300K = 27^{\circ}C$ ). If a heat sink is applied, TM can be used to protect the system thermally.
- **Fault detection flag:** The TM voltage source is internally turned off as soon as a fault is detected. For system monitoring purposes microcontroller interface faults are detected on falling edges of TM signal.

## Sine Amplitude Converter™ Point of Load Conversion

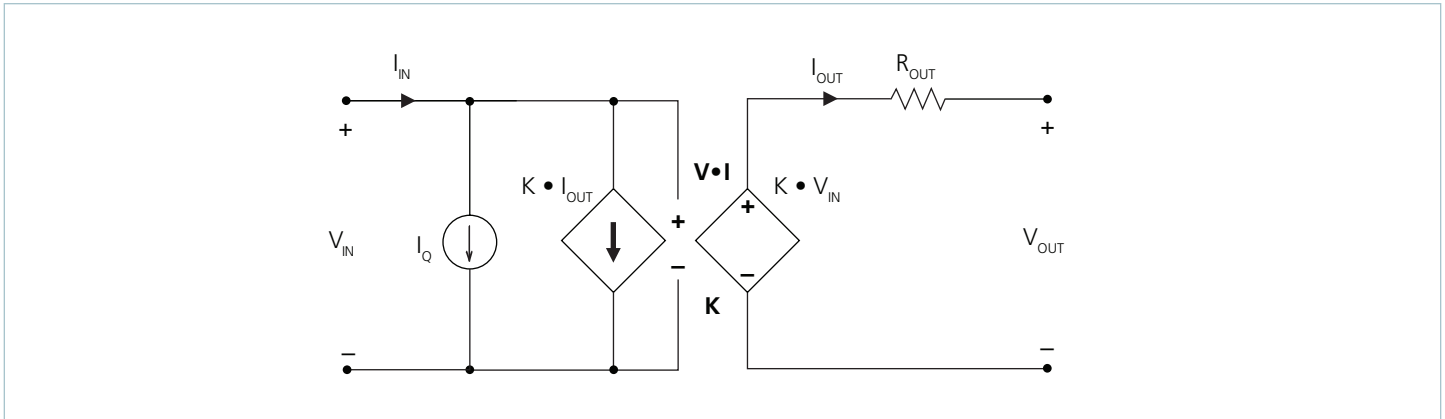


Figure 19 — BCM® DC model

The Sine Amplitude Converter (SAC™) uses a high frequency resonant tank to move energy from input to output. The resonant LC tank, operated at high frequency, is amplitude modulated as a function of input voltage and output current. A small amount of capacitance embedded in the input and output stages of the module is sufficient for full functionality and is key to achieving power density.

The MBCM270x338M235A00 SAC can be simplified into the preceding model.

At no load:

$$V_{OUT} = V_{IN} \cdot K \quad (1)$$

K represents the “turns ratio” of the SAC.  
Rearranging Eq (1):

$$K = \frac{V_{OUT}}{V_{IN}} \quad (2)$$

In the presence of load,  $V_{OUT}$  is represented by:

$$V_{OUT} = V_{IN} \cdot K - I_{OUT} \cdot R_{OUT} \quad (3)$$

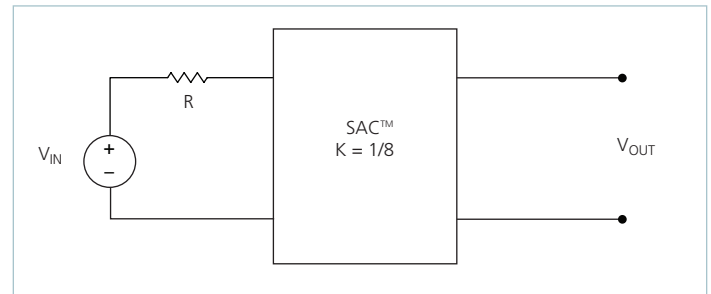
and  $I_{OUT}$  is represented by:

$$I_{OUT} = \frac{I_{IN} - I_Q}{K} \quad (4)$$

$R_{OUT}$  represents the impedance of the SAC, and is a function of the  $R_{DS(on)}$  of the input and output MOSFETs and the winding resistance of the power transformer.  $I_Q$  represents the quiescent current of

the SAC control, gate drive circuitry, and core losses.

The use of DC voltage transformation provides additional interesting attributes. Assuming that  $R_{OUT} = 0\Omega$  and  $I_Q = 0A$ , Eq. (3) now becomes Eq. (1) and is essentially load independent, resistor R is now placed in series with  $V_{IN}$ .

Figure 20 —  $K = 1/8$  Sine Amplitude Converter™ with series input resistor

The relationship between  $V_{IN}$  and  $V_{OUT}$  becomes:

$$V_{OUT} = (V_{IN} - I_{IN} \cdot R) \cdot K \quad (5)$$

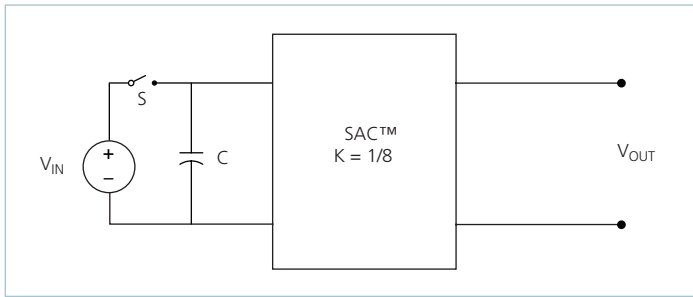
Substituting the simplified version of Eq. (4) ( $I_Q$  is assumed = 0A) into Eq. (5) yields:

$$V_{OUT} = V_{IN} \cdot K - I_{OUT} \cdot R \cdot K^2 \quad (6)$$

This is similar in form to Eq. (3), where  $R_{OUT}$  is used to represent the characteristic impedance of the SACTm. However, in this case a real  $R$  on the input side of the SAC is effectively scaled by  $K^2$  with respect to the output.

Assuming that  $R = 1\Omega$ , the effective  $R$  as seen from the output side is  $15.6m\Omega$ , with  $K = 1/8$  as shown in Figure 20.

A similar exercise should be performed with the addition of a capacitor or shunt impedance at the input to the SAC. A switch in series with  $V_{IN}$  is added to the circuit. This is depicted in Figure 21.



**Figure 21** — Sine Amplitude Converter™ with input capacitor

A change in  $V_{IN}$  with the switch closed would result in a change in capacitor current according to the following equation:

$$I_C(t) = C \frac{dV_{IN}}{dt} \quad (7)$$

Assume that with the capacitor charged to  $V_{IN}$ , the switch is opened and the capacitor is discharged through the idealized SAC. In this case,

$$I_C = I_{OUT} \cdot K \quad (8)$$

substituting Eq. (1) and (8) into Eq. (7) reveals:

$$I_{OUT} = \frac{C}{K^2} \cdot \frac{dV_{OUT}}{dt} \quad (9)$$

The equation in terms of the output has yielded a  $K^2$  scaling factor for  $C$ , specified in the denominator of the equation.

A  $K$  factor less than unity results in an effectively larger capacitance on the output when expressed in terms of the input. With a  $K = 1/8$  as shown in Figure 21,  $C = 1\mu F$  would appear as  $C = 64\mu F$  when viewed from the output.

Low impedance is a key requirement for powering a high-current, low-voltage load efficiently. A switching regulation stage should have minimal impedance while simultaneously providing appropriate filtering for any switched current. The use of a SAC between the regulation stage and the point of load provides a dual benefit of scaling down series impedance leading back to the source and scaling up shunt capacitance or energy storage as a function of its  $K$  factor squared. However, the benefits are not useful if the series impedance of the SAC is too high. The impedance of the SAC must be low, i.e. well beyond the crossover frequency of the system.

A solution for keeping the impedance of the SAC low involves switching at a high frequency. This enables small magnetic components because magnetizing currents remain low. Small magnetics mean small path lengths for turns. Use of low loss core material at high frequencies also reduces core losses.

The two main terms of power loss in the BCM module are:

- No load power dissipation ( $P_{NL}$ ): defined as the power used to power up the module with an enabled powertrain at no load.
- Resistive loss ( $P_{ROUT}$ ): refers to the power loss across the BCM module modeled as pure resistive impedance.

$$P_{DISSIPATED} = P_{NL} + P_{ROUT} \quad (10)$$

Therefore,

$$P_{OUT} = P_{IN} - P_{DISSIPATED} = P_{IN} - P_{NL} - P_{ROUT} \quad (11)$$

The above relations can be combined to calculate the overall module efficiency:

$$\begin{aligned} \eta &= \frac{P_{OUT}}{P_{IN}} = \frac{P_{IN} - P_{NL} - P_{ROUT}}{P_{IN}} \quad (12) \\ &= \frac{V_{IN} \cdot I_{IN} - P_{NL} - (I_{OUT})^2 \cdot R_{OUT}}{V_{IN} \cdot I_{IN}} \\ &= 1 - \frac{(P_{NL} + (I_{OUT})^2 \cdot R_{OUT})}{V_{IN} \cdot I_{IN}} \end{aligned}$$



## Input and Output Filter Design

A major advantage of SAC™ systems versus conventional PWM converters is that the transformers do not require large functional filters. The resonant LC tank, operated at extreme high frequency, is amplitude modulated as a function of input voltage and output current and efficiently transfers charge through the isolation transformer. A small amount of capacitance embedded in the input and output stages of the module is sufficient for full functionality and is key to achieve power density.

This paradigm shift requires system design to carefully evaluate external filters in order to:

### 1. *Guarantee low source impedance:*

To take full advantage of the BCM module's dynamic response, the impedance presented to its input terminals must be low from DC to approximately 5MHz. The connection of the bus converter module to its power source should be implemented with minimal distribution inductance. If the interconnect inductance exceeds 100nH, the input should be bypassed with a RC damper to retain low source impedance and stable operation. With an interconnect inductance of 200nH, the RC damper may be as high as 1μF in series with 0.3Ω. A single electrolytic or equivalent low-Q capacitor may be used in place of the series RC bypass.

### 2. *Further reduce input and/or output voltage ripple without sacrificing dynamic response:*

Given the wide bandwidth of the module, the source response is generally the limiting factor in the overall system response. Anomalies in the response of the source will appear at the output of the module multiplied by its K factor.

### 3. *Protect the module from overvoltage transients imposed by the system that would exceed maximum ratings and cause failures:*

The module input/output voltage ranges shall not be exceeded. An internal overvoltage lockout function prevents operation outside of the normal operating input range. Even during this condition, the powertrain is exposed to the applied voltage and power MOSFETs must withstand it. A criterion for protection is the maximum amount of energy that the input or output switches can tolerate if avalanched.

Total load capacitance at the output of the BCM module shall not exceed the specified maximum. Owing to the wide bandwidth and low output impedance of the module, low-frequency bypass capacitance and significant energy storage may be more densely and efficiently provided by adding capacitance at the input of the module. At frequencies <500kHz the module appears as an impedance of  $R_{OUT}$  between the source and load.

Within this frequency range, capacitance at the input appears as effective capacitance on the output per the relationship defined in Eq. 13.

$$C_{OUT} = \frac{C_{IN}}{K^2} \quad (13)$$

This enables a reduction in the size and number of capacitors used in a typical system.

## Thermal Considerations

VI Chip® products are multi-chip modules whose temperature distribution varies greatly for each part number as well as with the input / output conditions, thermal management and environmental conditions. Maintaining the top of the MBCM270x338M235A00 case to less than 100°C will keep all junctions within the VI Chip module below 125°C for most applications.

The percent of total heat dissipated through the top surface versus through the J-lead is entirely dependent on the particular mechanical and thermal environment. The heat dissipated through the top surface is typically 60%. The heat dissipated through the J-lead onto the PCB surface is typically 40%. Use 100% top surface dissipation when designing for a conservative cooling solution.

It is not recommended to use a VI Chip module for an extended period of time at full load without proper heat sinking.

## Current Sharing

The SAC™ topology bases its performance on efficient transfer of energy through a transformer without the need of closed loop control. For this reason, the transfer characteristic can be approximated by an ideal transformer with a positive temperature coefficient series resistance.

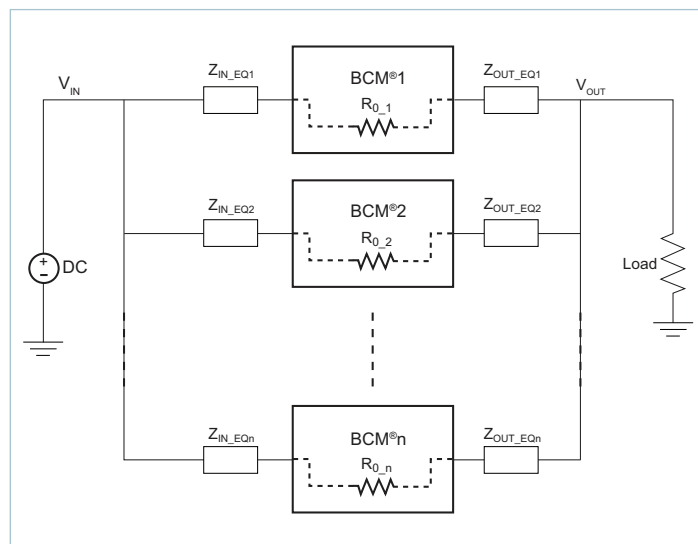
This type of characteristic is close to the impedance characteristic of a DC power distribution system, both in dynamic (AC) behavior and for steady state (DC) operation.

When multiple BCM modules of a given part number are connected in an array they will inherently share the load current according to the equivalent impedance divider that the system implements from the power source to the point of load.

Some general recommendations to achieve matched array impedances include:

- Dedicate common copper planes within the PCB to deliver and return the current to the modules.
- Provide as symmetric a PCB layout as possible among modules
- Apply same input / output filters (if present) to each unit.

For further details see [AN:016 Using BCM Bus Converters in High Power Arrays](#).



**Figure 22** — BCM module array

## Fuse Selection

In order to provide flexibility in configuring power systems VI Chip® products are not internally fused. Input line fusing of VI Chip products is recommended at system level to provide thermal protection in case of catastrophic failure.

The fuse shall be selected by closely matching system requirements with the following characteristics:

- Current rating (usually greater than maximum current of BCM module)
- Maximum voltage rating (usually greater than the maximum possible input voltage)
- Ambient temperature
- Nominal melting  $I^2t$
- Recommended fuse:  $\leq 2.5A$  Bussmann PC-Tron or  $\leq 3.15A$  SOC type 36CFA.

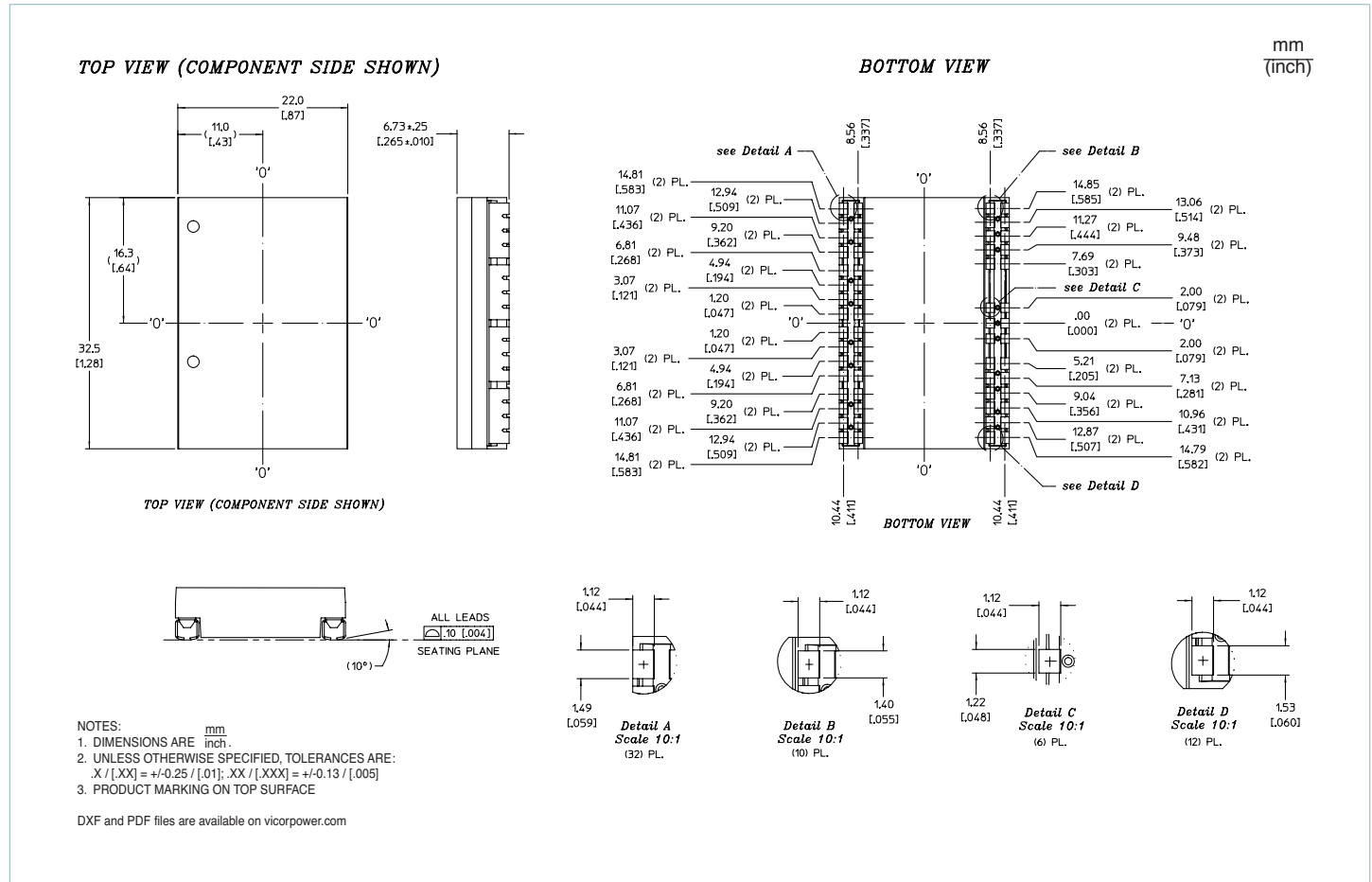
## Reverse Operation

BCM modules are capable of reverse power operation. Once the unit is started, energy will be transferred from secondary back to the primary whenever the secondary voltage exceeds  $V_{IN} \cdot K$ . The module will continue operation in this fashion for as long as no faults occur.

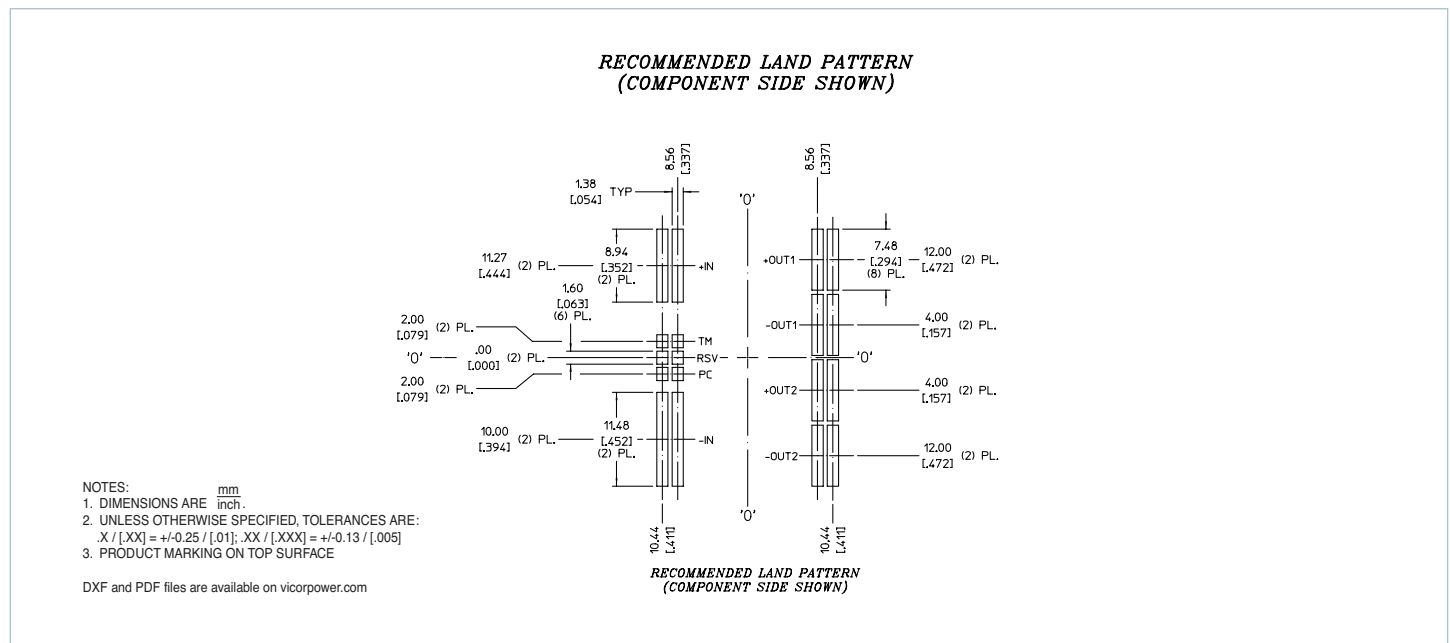
The MBCM270x338M235A00 has not been qualified for continuous operation in a reverse power condition. Furthermore fault protections which help protect the module in forward operation will not fully protect the module in reverse operation.

Transient operation in reverse is expected in cases where there is significant energy storage on the output and transient voltages appear on the input. Transient reverse power operation of less than 10ms, 10% duty cycle is permitted and has been qualified to cover these cases.

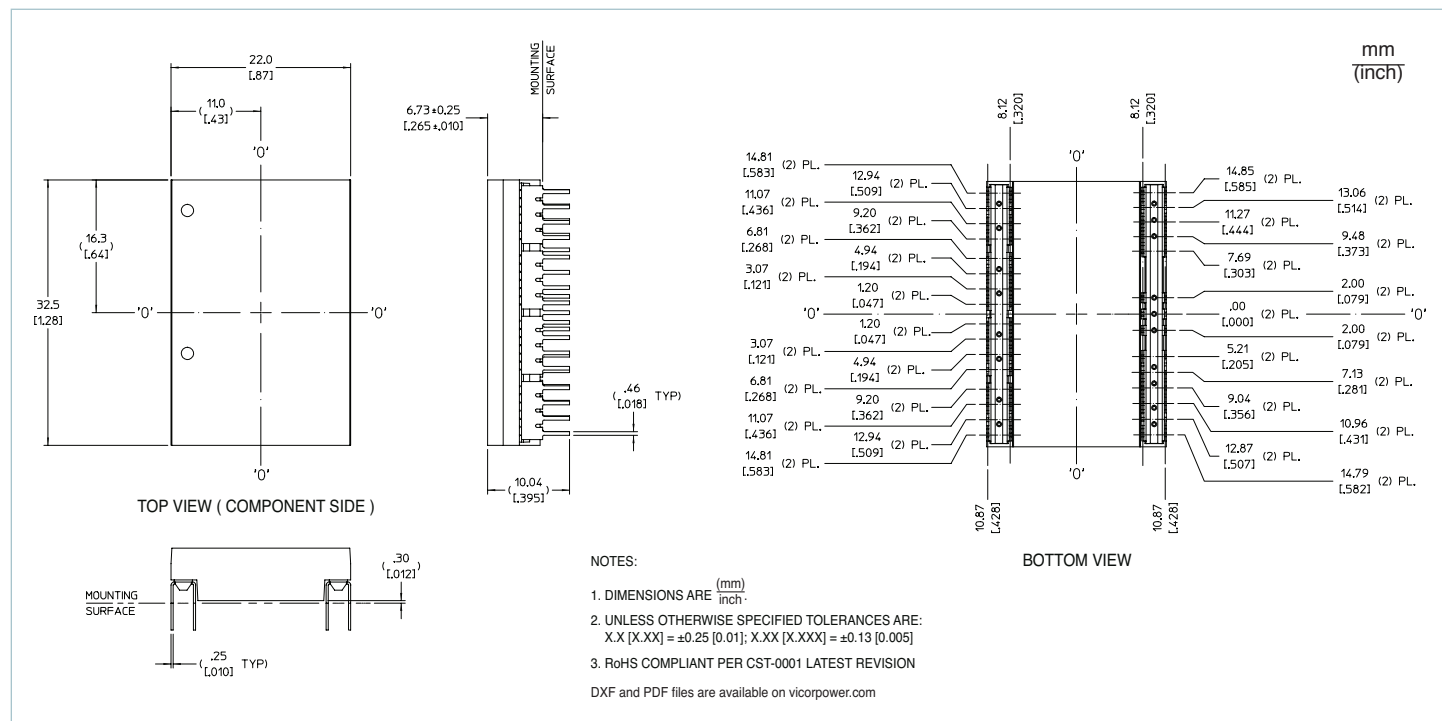
## J-LEAD Package Mechanical drawing



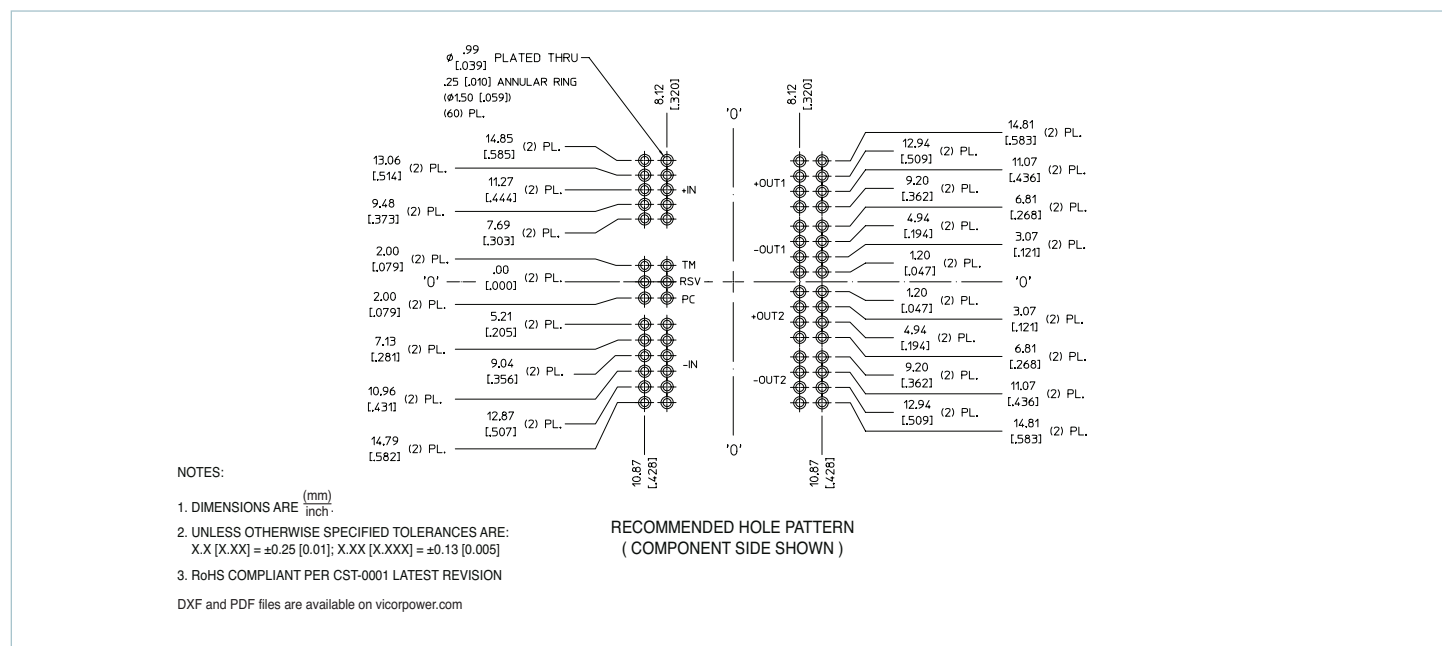
## J-LEAD Package Recommended Land Pattern



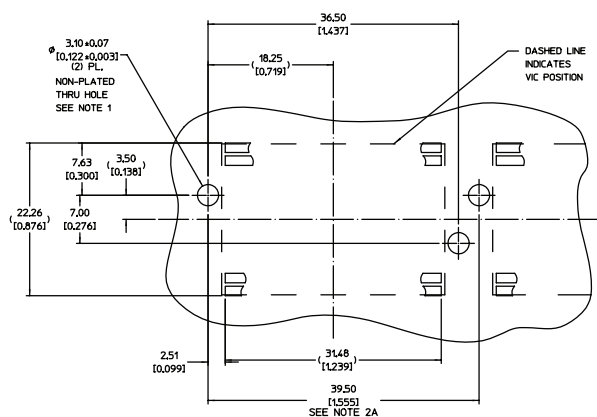
## Through Hole Package Mechanical drawing



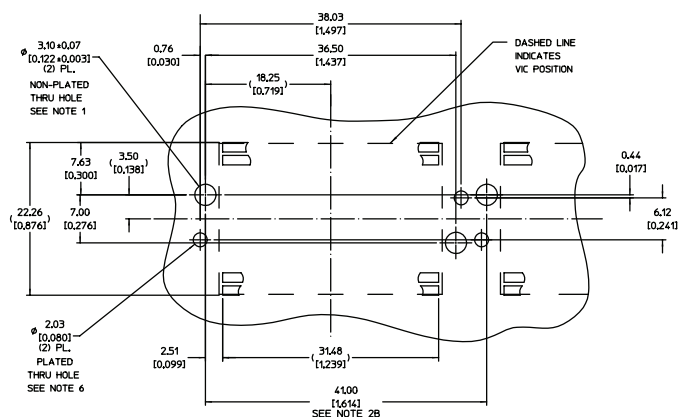
## Through Hole Package Recommended Land Pattern



## Recommended Heat Sink Push Pin Location



(NO GROUNDING CLIPS)



(WITH GROUNDING CLIPS)

## Notes:

- Maintain 3.50 (0.138) Dia. keep-out zone free of copper, all PCB layers.
- (A) Minimum recommended pitch is 39.50 (1.555). This provides 7.00 (0.275) component edge-to-edge spacing, and 0.50 (0.020) clearance between Vicor heat sinks.  
(B) Minimum recommended pitch is 41.00 (1.614). This provides 8.50 (0.334) component edge-to-edge spacing, and 2.00 (0.079) clearance between Vicor heat sinks.
- VI Chip® module land pattern shown for reference only; actual land pattern may differ. Dimensions from edges of land pattern to push-pin holes will be the same for all full-size VI Chip® products.
- RoHS compliant per CST-0001 latest revision.
- Unless otherwise specified: Dimensions are mm (inches) tolerances are:  
x.x (x.xx) =  $\pm 0.3$  (0.01)  
x.xx (x.xxx) =  $\pm 0.13$  (0.005)
- Plated through holes for grounding clips (33855) shown for reference, heat sink orientation and device pitch will dictate final grounding solution.

## Revision History

Revision	Date	Description	Page Number(s)
1.8	08/01/16	Formatting Update	All

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