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### FDS3692

# N-Channel PowerTrench® MOSFET 100V, 4.5A, 60m $\Omega$

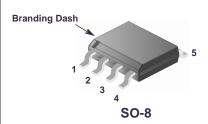
### **Features**

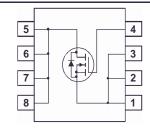
- $r_{DS(ON)} = 50 \text{m}\Omega$  (Typ.),  $V_{GS} = 10 \text{V}$ ,  $I_D = 4.5 \text{A}$
- $Q_q(tot) = 11nC (Typ.), V_{GS} = 10V$
- Low Miller Charge
- Low Q<sub>RR</sub> Body Diode
- Optimized efficiency at high frequencies
- UIS Capability (Single Pulse and Repetitive Pulse)

Formerly developmental type 82745

### **Applications**

- DC/DC converters and Off-Line UPS
- · Distributed Power Architectures and VRMs
- Primary Switch for 24V and 48V Systems
- High Voltage Synchronous Rectifier
- Direct Injection / Diesel Injection Systems
- 42V Automotive Load Control
- Electronic Valve Train Systems





### **MOSFET Maximum Ratings** $T_A = 25$ °C unless otherwise noted

Symbol	Parameter	Ratings	Units
V <sub>DSS</sub>	Drain to Source Voltage	100	V
V <sub>GS</sub>	Gate to Source Voltage	±20	V
	Drain Current		
	Continuous ( $T_A = 25^{\circ}C$ , $V_{GS} = 10V$ , $R_{\theta JA} = 50^{\circ}C/W$ )	4.5	Α
ıD	Continuous ( $T_A = 100$ °C, $V_{GS} = 10V$ , $R_{\theta JA} = 50$ °C/W)	2.8	А
	Pulsed	Figure 4	А
E <sub>AS</sub>	Single Pulse Avalanche Energy (Note 1)	171	mJ
	Power dissipation	2.5	W
$P_{D}$	Derate above 25°C	20	mW/°C
T <sub>J</sub> , T <sub>STG</sub>	Operating and Storage Temperature	-55 to 150	°C

### **Thermal Characteristics**

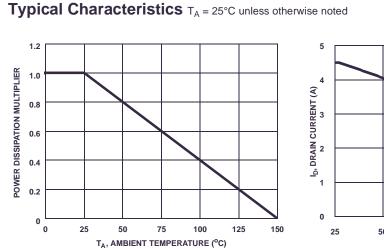
$R_{\theta JA}$	Thermal Resistance, Junction to Ambient at 10 seconds (Note 3)	50	°C/W
$R_{\theta JA}$	Thermal Resistance, Junction to Ambient at 1000 seconds (Note 3)	85	°C/W
$R_{\theta JC}$	Thermal Resistance, Junction to Case (Note 2)	25	°C/W

### **Package Marking and Ordering Information**

Device Marking Device		Package	Reel Size	Tape Width	Quantity
FDS3692	FDS3692	SO-8	13"	12mm	2500 units

Symbol	Parameter	Test Conditions		Min	Тур	Max	Units
Off Chara	cteristics						
B <sub>VDSS</sub>	Drain to Source Breakdown Voltage	I <sub>D</sub> = 250μA, V <sub>GS</sub>	= 0V	100	-	-	V
	7 0	V <sub>DS</sub> = 80V		-	-	1	
I <sub>DSS</sub>	Zero Gate Voltage Drain Current	$V_{GS} = 0V$	$T_{\rm C} = 150^{\rm o}{\rm C}$	-	-	250	μΑ
I <sub>GSS</sub>	Gate to Source Leakage Current	$V_{GS} = \pm 20V$		-	-	±100	nA
On Chara	cteristics						
V <sub>GS(TH)</sub>	Gate to Source Threshold Voltage	$V_{GS} = V_{DS}, I_D =$	250μΑ	2	-	4	V
00(111)		I <sub>D</sub> = 4.5A, V <sub>GS</sub> =		-	0.050	0.060	
		$I_D = 2A, V_{GS} = 6$		-	0.064	0.096	
r <sub>DS(ON)</sub>	Drain to Source On Resistance		$I_D = 4.5A, V_{GS} = 10V,$		0.101	0.122	Ω
Dvnamic	Characteristics	_					
C <sub>ISS</sub>	Input Capacitance	V <sub>DS</sub> = 25V, V <sub>GS</sub> = 0V, f = 1MHz		-	746	-	pF
C <sub>OSS</sub>	Output Capacitance			-	115	-	pF
C <sub>RSS</sub>	Reverse Transfer Capacitance			-	27	-	pF
Q <sub>g(TOT)</sub>	Total Gate Charge at 10V	V <sub>GS</sub> = 0V to 10V	'	-	11	15	nC
$Q_{g(TH)}$	Threshold Gate Charge	$V_{GS} = 0V \text{ to } 2V$	V <sub>DD</sub> = 50V	-	1.4	1.9	nC
Q <sub>gs</sub>	Gate to Source Gate Charge		$I_{D} = 4.5A$	-	3.5	-	nC
Q <sub>gs2</sub>	Gate Charge Threshold to Plateau		$I_g = 1.0 \text{mA}$		2.1	-	nC
Q <sub>gd</sub>	Gate to Drain "Miller" Charge	7		-	2.8	-	nC
	Characteristics (V <sub>GS</sub> = 10V)						
t <sub>ON</sub>	Turn-On Time			-	-	54	ns
t <sub>d(ON)</sub>	Turn-On Delay Time			-	9.8	-	ns
t <sub>r</sub>	Rise Time	$V_{DD} = 50V, I_{D} = 4.5A$ $V_{GS} = 10V, R_{GS} = 26\Omega$		-	26	-	ns
t <sub>d(OFF)</sub>	Turn-Off Delay Time			-	34	-	ns
t <sub>f</sub>	Fall Time			-	26	-	ns
t <sub>OFF</sub>	Turn-Off Time			-	-	90	ns
 Drain-Soເ	urce Diode Characteristics						
$V_{SD}$	Source to Drain Diode Voltage	I <sub>SD</sub> = 4.5A		-	-	1.25	V
* SD	Source to Brain Blode Voltage	I <sub>SD</sub> = 2A		-	-	1.0	V
t <sub>rr</sub>	Reverse Recovery Time	I <sub>SD</sub> = 4.5A, dI <sub>SD</sub> /dt= 100A/μs		-	-	47	ns
Q <sub>RR</sub>	Reverse Recovered Charge	I <sub>SD</sub> = 4.5A, dI <sub>SD</sub> /dt= 100A/μs		-	-	64	nC

- Notes:
  1: E<sub>AS</sub> of 171mJ is based on starting T<sub>J</sub> = 25°C, L = 38mH, I<sub>AS</sub> = 3A. 100% test at L = 1mH, I<sub>AS</sub> = 10.3A.
  2: R<sub>θ,JA</sub> is the sum of the junction-to-case and case-to-ambient thermal resistance where the case thermal reference is defined as the solder mounting surface of the drain pins. R<sub>θ,JC</sub> is guaranteed by design while R<sub>θCA</sub> is determined by the user's board design.
  3: R<sub>θ,JA</sub> is measured with 1.0 in<sup>2</sup> copper on FR-4 board



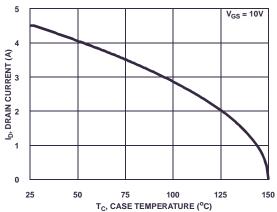


Figure 1. Normalized Power Dissipation vs Ambient Temperature

Figure 2. Maximum Continuous Drain Current vs Case Temperature

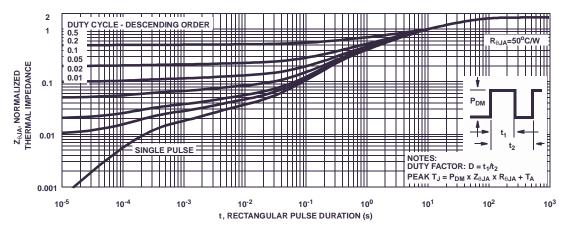


Figure 3. Normalized Maximum Transient Thermal Impedance

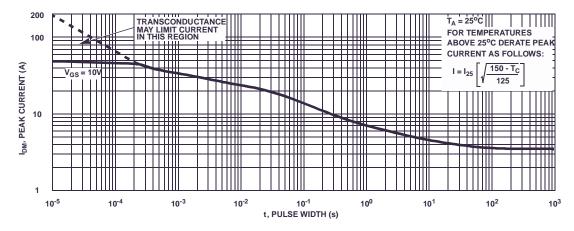
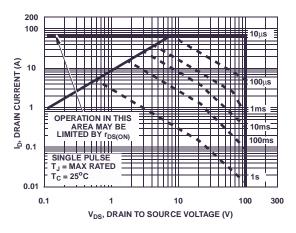


Figure 4. Peak Current Capability





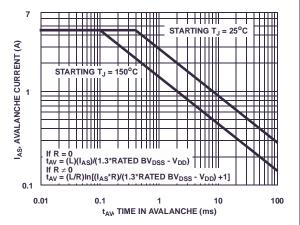
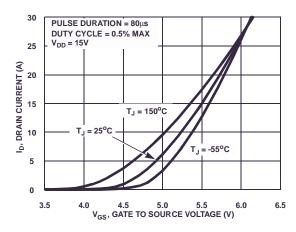


Figure 5. Forward Bias Safe Operating Area

NOTE: Refer to Fairchild Application Notes AN7514 and AN7515

Figure 6. Unclamped Inductive Switching

Capability



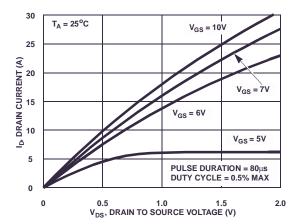
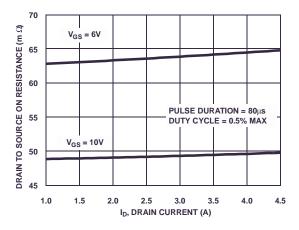


Figure 7. Transfer Characteristics

Figure 8. Saturation Characteristics



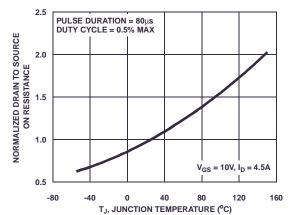


Figure 9. Drain to Source On Resistance vs Drain Current

Figure 10. Normalized Drain to Source On Resistance vs Junction Temperature

## Typical Characteristics $T_A = 25$ °C unless otherwise noted

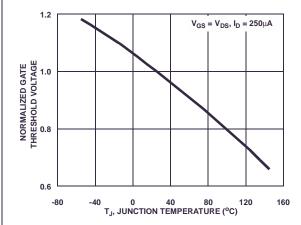


Figure 11. Normalized Gate Threshold Voltage vs Junction Temperature

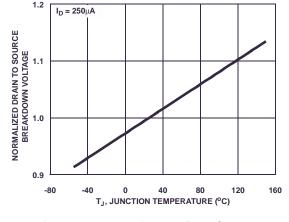


Figure 12. Normalized Drain to Source Breakdown Voltage vs Junction Temperature

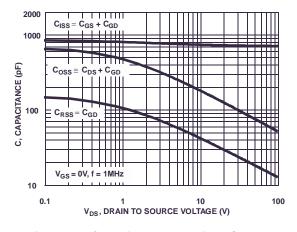


Figure 13. Capacitance vs Drain to Source Voltage

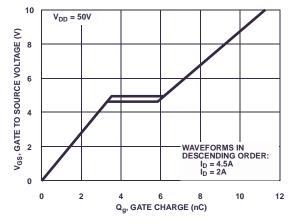
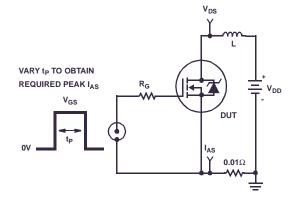


Figure 14. Gate Charge Waveforms for Constant Gate Currents

### **Test Circuits and Waveforms**



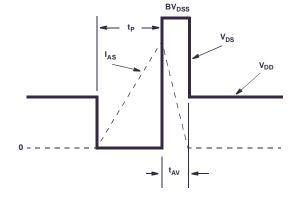


Figure 15. Unclamped Energy Test Circuit

Figure 16. Unclamped Energy Waveforms

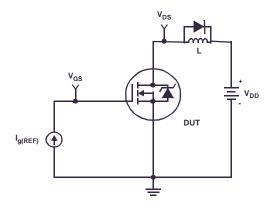


Figure 17. Gate Charge Test Circuit

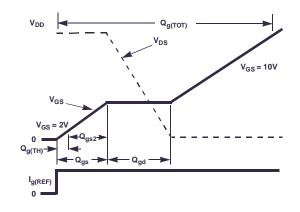


Figure 18. Gate Charge Waveforms

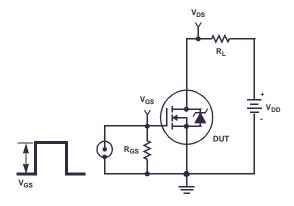


Figure 19. Switching Time Test Circuit

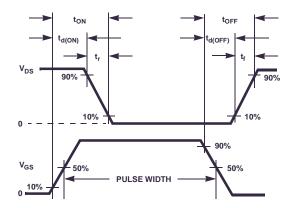


Figure 20. Switching Time Waveforms

FDS3692 Rev. C

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### Thermal Resistance vs. Mounting Pad Area

The maximum rated junction temperature,  $T_{JM}$ , and the thermal resistance of the heat dissipating path determines the maximum allowable device power dissipation,  $P_{DM}$ , in an application. Therefore the application's ambient temperature,  $T_A$  (°C), and thermal resistance  $R_{\theta JA}$  (°C/W) must be reviewed to ensure that  $T_{JM}$  is never exceeded. Equation 1 mathematically represents the relationship and serves as the basis for establishing the rating of the part.

$$P_{DM} = \frac{(T_{JM} - T_A)}{R_{\theta JA}} \tag{EQ. 1}$$

In using surface mount devices such as the SO8 package, the environment in which it is applied will have a significant influence on the part's current and maximum power dissipation ratings. Precise determination of  $P_{DM}$  is complex and influenced by many factors:

- Mounting pad area onto which the device is attached and whether there is copper on one side or both sides of the board.
- The number of copper layers and the thickness of the board.
- 3. The use of external heat sinks.
- 4. The use of thermal vias.
- 5. Air flow and board orientation.
- For non steady state applications, the pulse width, the duty cycle and the transient thermal response of the part, the board and the environment they are in.

Fairchild provides thermal information to assist the designer's preliminary application evaluation. Figure 21 defines the  $R_{\theta JA}$  for the device as a function of the top copper (component side) area. This is for a horizontally positioned FR-4 board with 1oz copper after 1000 seconds of steady state power with no air flow. This graph provides the necessary information for calculation of the steady state junction temperature or power dissipation. Pulse applications can be evaluated using the Fairchild device Spice thermal model or manually utilizing the normalized

maximum transient thermal impedance curve.

Thermal resistances corresponding to other copper areas can be obtained from Figure 21 or by calculation using Equation 2. The area, in square inches is the top copper area including the gate and source pads.

$$R_{\theta JA} = 64 + \frac{26}{0.23 + Area}$$
 (EQ. 2)

The transient thermal impedance  $(Z_{\theta JA})$  is also effected by varied top copper board area. Figure 22 shows the effect of copper pad area on single pulse transient thermal impedance. Each trace represents a copper pad area in square inches corresponding to the descending list in the graph. Spice and SABER thermal models are provided for each of the listed pad areas.

Copper pad area has no perceivable effect on transient thermal impedance for pulse widths less than 100ms. For pulse widths less than 100ms the transient thermal impedance is determined by the die and package. Therefore, CTHERM1 through CTHERM5 and RTHERM1 through RTHERM5 remain constant for each of the thermal models. A listing of the model component values is available in Table 1.

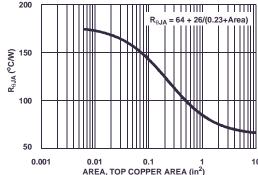


Figure 21. Thermal Resistance vs Mounting
Pad Area

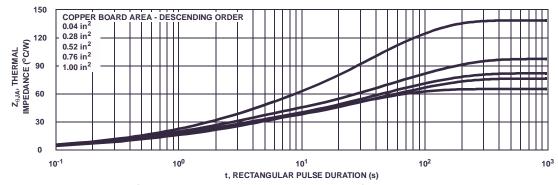
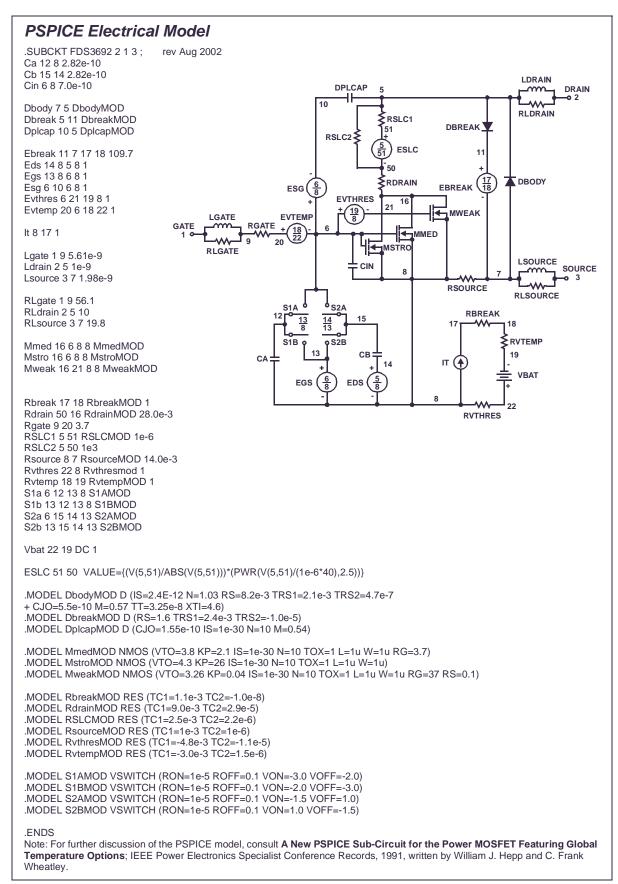
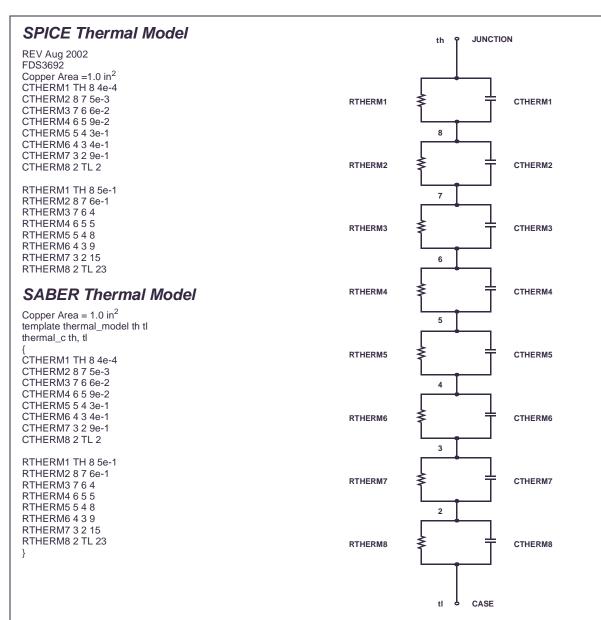


Figure 22. Thermal Impedance vs Mounting Pad Area



#### SABER Electrical Model REV Aug 2002 template FDS3692 n2,n1,n3 electrical n2,n1,n3 var i iscl dp..model dbodymod = (isl=2.4e-12,nl=1.03,rs=8.2e-3,trs1=2.1e-3,trs2=4.7e-7,cjo=5.5e-10,m=0.57,tt=3.25e-8,xti=4.6) dp..model dbreakmod = (rs=1.6.trs1=2.4e-3.trs2=-1.0e-5)dp..model dplcapmod = (cjo=1.55e-10,isl=10e-30,nl=10,m=0.54) $m..model mmedmod = (type=\_n, vto=3.8, kp=2.1, is=1e-30, tox=1)$ m..model mstrongmod = (type=\_n,vto=4.3,kp=26,is=1e-30, tox=1) m..model mweakmod = $(type=_n, vto=3.26, kp=0.04, is=1e-30, tox=1, rs=0.1)$ sw\_vcsp..model s1amod = (ron=1e-5,roff=0.1,von=-3.0,voff=-2.0) LDRAIN sw\_vcsp..model s1bmod = (ron=1e-5,roff=0.1,von=-2.0,voff=-3.0) DPLCAP DRAIN sw\_vcsp..model s2amod = (ron=1e-5,roff=0.1,von=-1.5,voff=1.0) 10 sw\_vcsp..model s2bmod = (ron=1e-5,roff=0.1,von=1.0,voff=-1.5) RI DRAIN c.ca n12 n8 = 2.82e-10ERSLC1 c.cb n15 n14 = 2.82e-1051 RSI C2 ₹ c.cin n6 n8 = 7.0e-10ISCL dp.dbody n7 n5 = model=dbodymod DBREAK 50 dp.dbreak n5 n11 = model=dbreakmod **≨**RDRAIN dp.dplcap n10 n5 = model=dplcapmod 8 ESG ( ▲ DBODY **EVTHRES** 16 spe.ebreak n11 n7 n17 n18 = 109.7 19 8 MWEAK **LGATE** EVTEMP spe.eds n14 n8 n5 n8 = 1 spe.egs n13 n8 n6 n8 = 1 (18 22 EBREAK MMED 20 spe.esg n6 n10 n6 n8 = 1 MSTRO RLGATE spe.evthres n6 n21 n19 n8 = 1 LSOURCE spe.evtemp n20 n6 n18 n22 = 1 CIN SOURCE RSOURCE i.it n8 n17 = 1RLSOURCE I.lgate n1 n9 = 5.61e-9RBRFAK <u>13</u> 8 <u>14</u> 13 I.ldrain n2 n5 = 1e-917 18 1.1source n3 n7 = 1.98e-9 **₹**RVTEMP S1B o S2B CB 19 res.rlgate n1 n9 = 56.1 CA IT res.rldrain n2 n5 = 10 VBAT res.rlsource n3 n7 = 19.8 EGS **EDS** m.mmed n16 n6 n8 n8 = model=mmedmod, l=1u, w=1u m.mstrong n16 n6 n8 n8 = model=mstrongmod, l=1u, w=1u **RVTHRES** m.mweak n16 n21 n8 n8 = model=mweakmod, l=1u, w=1u res.rbreak n17 n18 = 1, tc1=1.1e-3,tc2=-1.0e-8 res.rdrain n50 n16 = 28.0e-3, tc1=9.0e-3,tc2=2.9e-5 res.rgate n9 n20 = 3.7res.rslc1 n5 n51 = 1e-6, tc1=2.5e-3,tc2=2.2e-6 res.rslc2 n5 n50 = 1e3res.rsource n8 n7 = 14.0e-3, tc1=1e-3,tc2=1e-6 res.rvthres n22 n8 = 1, tc1=-4.8e-3,tc2=-1.1e-5res.rvtemp n18 n19 = 1. tc1=-3.0e-3.tc2=1.5e-6sw\_vcsp.s1a n6 n12 n13 n8 = model=s1amod sw\_vcsp.s1b n13 n12 n13 n8 = model=s1bmod sw\_vcsp.s2a n6 n15 n14 n13 = model=s2amod sw\_vcsp.s2b n13 n15 n14 n13 = model=s2bmod v.vbat n22 n19 = dc=1 equations { i (n51->n50) +=iscl iscl: v(n51,n50) = ((v(n5,n51)/(1e-9+abs(v(n5,n51))))\*((abs(v(n5,n51)\*1e6/40))\*\* 2.5))



### TABLE 1. THERMAL MODELS

COMPONANT	0.04 in <sup>2</sup>	0.28 in <sup>2</sup>	0.52 in <sup>2</sup>	0.76 in <sup>2</sup>	1.0 in <sup>2</sup>
CTHERM6	3.2e-1	3.5e-1	4.0e-1	4.0e-1	4.0e-1
CTHERM7	8.5e-1	9.0e-1	9.0e-1	9.0e-1	9.0e-1
CTHERM8	0.3	1.8	2.0	2.0	2.0
RTHERM6	24	18	12	10	9
RTHERM7	36	21	18	16	15
RTHERM8	53	37	30	28	23

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GENERAL TinyBoost<sup>1</sup> TinyBuck™ TinyCalc™ TinyLogic<sup>®</sup> TINYOPTO™ TinyPower™ TinyPWM™ TinyWire™ TranSiC® TriFault Detect™ TRUECURRENT®\*  $\mu SerDes^{\intercal_{M}}$ 

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Counterfeiting of semiconductor parts is a growing problem in the industry. All manufactures of semiconductor products are experiencing counterfeiting of their parts. Customers who inadvertently purchase counterfeit parts experience many problems such as loss of brand reputation, substandard performance, failed application, and increased cost of production and manufacturing delays. Fairchild is taking strong measures to protect ourselves and our customers from the proliferation of counterfeit parts. Fairchild strongly encourages customers to purchase Fairchild parts either directly from Fairchild or from Authorized Fairchild Distributors who are listed by country on our web page cited above. Products customers buy either from Fairchild directly or from Authorized Fairchild Distributors are genuine parts, have full traceability, meet Fairchild's quality standards for handing and storage and provide access to Fairchild's full range of up-to-date technical and product information. Fairchild and our Authorized Distributors will stand behind all warranties and will appropriately address and warranty issues that may arise. Fairchild will not provide any warranty coverage or other assistance for parts bought from Unauthorized Sources. Fairchild is committed to combat this global problem and encourage our customers to do their part in stopping this practice by buying direct or from authorized distributors.

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Datasheet Identification Product Status		Definition		
Advance Information Formative / In Design		Datasheet contains the design specifications for product development. Specifications may change in any manner without notice.		
Preliminary	First Production	Datasheet contains preliminary data; supplementary data will be published at a later date. Fairchild Semiconductor reserves the right to make changes at any time without notice to improve design.		
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