

3-V TO 4-V INPUT, 9-A OUTPUT SYNCHRONOUS BUCK PWM SWITCHER WITH INTEGRATED FETs (SWIFT™)

FEATURES

- 15-mΩ MOSFET Switches for High Efficiency at 9-A Continuous Output
- 0.9-V to 2.5-V Adjustable Output Voltage
- Externally Compensated With 1% Accuracy
- Fast Transient Response
- Wide PWM Frequency:
Fixed 350 kHz, 550 kHz or
Adjustable 280 kHz to 700 kHz
- Load Protected by Peak Current Limit and Thermal Shutdown
- Integrated Solution Reduces Board Area and Total Cost

APPLICATIONS

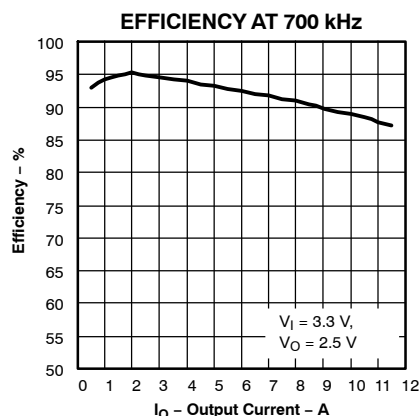
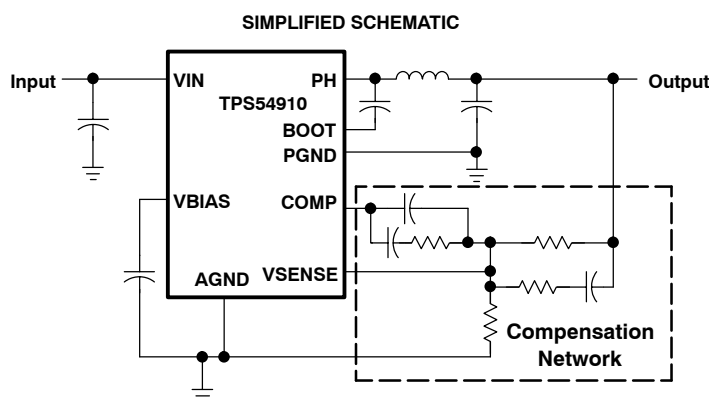
- Low-Voltage, High-Density Systems With Power Distributed at 3.3 V
- Point of Load Regulation for High Performance DSPs, FPGAs, ASICs and Microprocessors
- Broadband, Networking and Optical Communications Infrastructure
- Portable Computing/Notebook PCs

DESCRIPTION

As a member of the SWIFT™ family of dc/dc regulators, the TPS54910 low-input voltage high-output current synchronous buck PWM converter integrates all required active components. Included on the substrate with the listed features are a true, high performance, voltage error amplifier that enables maximum performance under transient conditions and flexibility in choosing the output filter L and C components; an under-voltage-lockout circuit to prevent start-up until the input voltage reaches 3 V; an internally and externally set slow-start circuit to limit in-rush currents; and a power good output useful for processor/logic reset, fault signaling, and supply sequencing.

The TPS54910 is available in a thermally enhanced 28-pin TSSOP (PWP) PowerPAD™ package, which eliminates bulky heatsinks. TI provides evaluation modules and the SWIFT™ designer software tool to aid in quickly achieving high-performance power supply designs to meet aggressive equipment development cycles.

SIMPLIFIED SCHEMATIC



Please be aware that an important notice concerning availability, standard warranty, and use in critical applications of Texas Instruments semiconductor products and disclaimers thereto appears at the end of this data sheet.

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These devices have limited built-in ESD protection. The leads should be shorted together or the device placed in conductive foam during storage or handling to prevent electrostatic damage to the MOS gates.

ORDERING INFORMATION

T _A	OUTPUT VOLTAGE	PACKAGE	PART NUMBER
–40°C to 85°C	0.9 V to 2.5 V	Plastic HTSSOP (PWP) ⁽¹⁾	TPS54910PWP

(1) The PWP package is also available taped and reeled. Add an R suffix to the device type (i.e., TPS54910PWPR). See the application section of the data sheet for PowerPAD drawing and layout information.

(2) For the most current package and ordering information, see the Package Option Addendum at the end of this document, or see the TI website at www.ti.com.

ABSOLUTE MAXIMUM RATINGS

over operating free-air temperature range unless otherwise noted⁽¹⁾

		TPS54910	UNIT
Input voltage range, V _I	SS/ENA, SYNC	–0.3 to 7	V
	RT	–0.3 to 6	
	VSENSE	–0.3 to 4	
	VIN	–0.3 to 4.5	
	BOOT	–0.3 to 10	
Output voltage range, V _O	VBIAS, COMP, PWRGD	–0.3 to 7	V
	PH	–0.6 to 6	
Source current, I _O	PH	Internally Limited	
	COMP, VBIAS	6	mA
Sink current, I _S	PH	16	A
	COMP	6	mA
	SS/ENA, PWRGD	10	
Voltage differential	AGND to PGND	±0.3	V
Operating virtual junction temperature range, T _J		–40 to 125	°C
Storage temperature, T _{stg}		–65 to 150	°C
Lead temperature 1,6 mm (1/16 inch) from case for 10 seconds		300	°C

(1) Stresses beyond those listed under “absolute maximum ratings” may cause permanent damage to the device. These are stress ratings only, and functional operation of the device at these or any other conditions beyond those indicated under “recommended operating conditions” is not implied. Exposure to absolute-maximum-rated conditions for extended periods may affect device reliability.

RECOMMENDED OPERATING CONDITIONS

	MIN	NOM	MAX	UNIT
Input voltage, V _I	3		4	V
Operating junction temperature, T _J	–40		125	°C

DISSIPATION RATINGS⁽¹⁾⁽²⁾

PACKAGE	THERMAL IMPEDANCE JUNCTION-TO-AMBIENT	T _A = 25°C POWER RATING	T _A = 70°C POWER RATING	T _A = 85°C POWER RATING
28 Pin PWP with solder	14.4°C/W	6.94 W ⁽³⁾	3.81 W	2.77 W
28 Pin PWP without solder	27.9°C/W	3.58 W	1.97 W	1.43 W

(1) For more information on the PWP package, refer to TI technical brief, literature number SLMA002.

(2) Test board conditions:

1. 3" x 3", 4 layers, thickness: 0.062"
2. 1.5 oz. copper traces located on the top of the PCB
3. 1.5 oz. copper ground plane on the bottom of the PCB
4. 0.5 oz. copper ground planes on the 2 internal layers
5. 12 thermal vias (see “Recommended Land Pattern” in applications section of this data sheet)

(3) Maximum power dissipation may be limited by over current protection.

ELECTRICAL CHARACTERISTICS

 $T_J = -40^{\circ}\text{C}$ to 125°C , $V_I = 3\text{ V}$ to 4 V (unless otherwise noted)

PARAMETER		TEST CONDITIONS	MIN	TYP	MAX	UNIT
SUPPLY VOLTAGE, VIN						
Input voltage range, VIN			3.0		4.0	V
I(Q)	Quiescent current	f _s = 350 kHz, SYNC ≤ 0.8 V, RT open, PH pin open		9.8	17.0	mA
		f _s = 550 kHz, SYNC ≥ 2.5 V, RT open, PH pin open		14.0	23.0	
		Shutdown, SS/ENA = 0 V		1	1.4	
UNDER VOLTAGE LOCK OUT						
Start threshold voltage, UVLO			2.95		3.0	V
Stop threshold voltage, UVLO			2.70	2.80		V
Hysteresis voltage, UVLO			0.14	0.16		V
Rising and falling edge deglitch, UVLO ⁽¹⁾				2.5		μs
BIAS VOLTAGE						
Output voltage, VBIAS		I _(VBIAS) = 0	2.70	2.80	2.90	V
Output current, VBIAS ⁽²⁾					100	μA
CUMULATIVE REFERENCE						
V _{ref}	Accuracy		0.882	0.891	0.900	V
REGULATION						
Line regulation ⁽¹⁾⁽³⁾		I _L = 4.5 A, f _s = 350 kHz, T _J = 85°C			0.07	%V
		I _L = 4.5 A, f _s = 550 kHz, T _J = 85°C			0.07	
Load regulation ⁽¹⁾⁽³⁾		I _L = 0 A to 9 A, f _s = 350 kHz, T _J = 85°C			0.03	%A
		I _L = 0 A to 9 A, f _s = 550 kHz, T _J = 85°C			0.03	
OSCILLATOR						
Internally set—free running frequency		SYNC ≤ 0.8 V, RT open	280	350	420	kHz
		SYNC ≥ 2.5 V, RT open	440	550	660	
Externally set—free running frequency range		RT = 180 kΩ (1% resistor to AGND)	252	280	308	kHz
		RT = 100 kΩ (1% resistor to AGND)	460	500	540	
		RT = 68 kΩ (1% resistor to AGND)	663	700	762	
High level threshold, SYNC			2.5			V
Low level threshold, SYNC					0.8	V
Pulse duration, external synchronization, SYNC ⁽¹⁾			50			ns
Frequency range, SYNC ⁽¹⁾			330		700	kHz
Ramp valley ⁽¹⁾				0.75		V
Ramp amplitude (peak-to-peak) ⁽¹⁾				1		V
Minimum controllable on time ⁽¹⁾					200	ns
Maximum duty cycle ⁽¹⁾			90%			

⁽¹⁾ Specified by design

⁽²⁾ Static resistive loads only

⁽³⁾ Specified by the circuit used in Figure 10

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ELECTRICAL CHARACTERISTICS (continued)

 $T_J = -40^{\circ}\text{C}$ to 125°C , $V_I = 3\text{ V}$ to 4 V (unless otherwise noted)

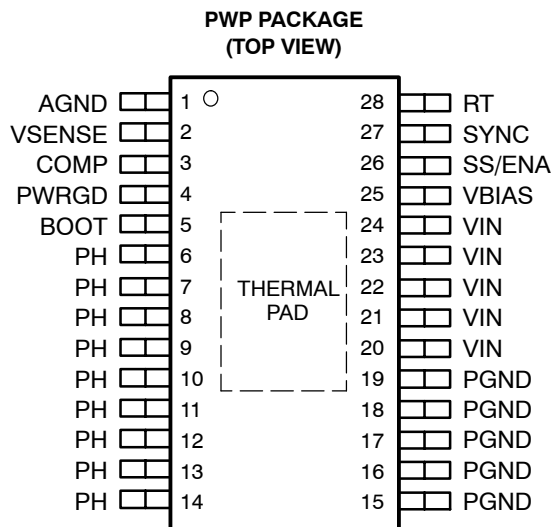
PARAMETER	TEST CONDITIONS	MIN	TYP	MAX	UNIT
ERROR AMPLIFIER					
Error amplifier open loop voltage gain	1 k Ω COMP to AGND ⁽¹⁾	90	110		dB
Error amplifier unity gain bandwidth	Parallel 10 k Ω , 160 pF COMP to AGND ⁽¹⁾	3	5		MHz
Error amplifier common mode input voltage range	Powered by internal LDO ⁽¹⁾	0		V _{BIAS}	V
Input bias current, VSENSE	VSENSE = V _{ref}		60	250	nA
Output voltage slew rate (symmetric), COMP		1.0	1.4		V/ μ s
PWM COMPARATOR					
PWM comparator propagation delay time, PWM comparator input to PH pin (excluding deadtime)	10-mV overdrive ⁽¹⁾		70	85	ns
SLOW-START/ENABLE					
Enable threshold voltage, SS/ENA		0.82	1.2	1.4	V
Enable hysteresis voltage, SS/ENA ⁽¹⁾			0.03		V
Falling edge deglitch, SS/ENA ⁽¹⁾			2.5		μ s
Internal slow-start time		2.6	3.35	4.1	ms
Charge current, SS/ENA	SS/ENA = 0 V	3	5	8	μ A
Discharge current, SS/ENA	SS/ENA = 1.3 V, V _I = 1.5 V	1.5	2.3	4.0	mA
POWER GOOD					
Power good threshold voltage	VSENSE falling		90		%V _{ref}
Power good hysteresis voltage ⁽¹⁾			3		%V _{ref}
Power good falling edge deglitch ⁽¹⁾			35		μ s
Output saturation voltage, PWRGD	I _(sink) = 2.5 mA		0.18	0.3	V
Leakage current, PWRGD	V _I = 5.5 V			1	μ A
CURRENT LIMIT					
Current limit	V _I = 3.3 V ⁽¹⁾ , Output shorted	11	15		A
Current limit leading edge blanking time			100		ns
Current limit total response time			200		ns
THERMAL SHUTDOWN					
Thermal shutdown trip point ⁽¹⁾		135	150	165	$^{\circ}\text{C}$
Thermal shutdown hysteresis ⁽¹⁾			10		$^{\circ}\text{C}$
OUTPUT POWER MOSFETS					
r _{DS(on)} Power MOSFET switches	V _I = 3 V ⁽⁴⁾		15	30	m Ω
	V _I = 3.6 V ⁽⁴⁾		14	28	

⁽¹⁾ Specified by design

⁽²⁾ Static resistive loads only

⁽³⁾ Specified by the circuit used in Figure 10

⁽⁴⁾ Matched MOSFETs low-side r_{DS(on)} production tested, high-side r_{DS(on)} production tested.



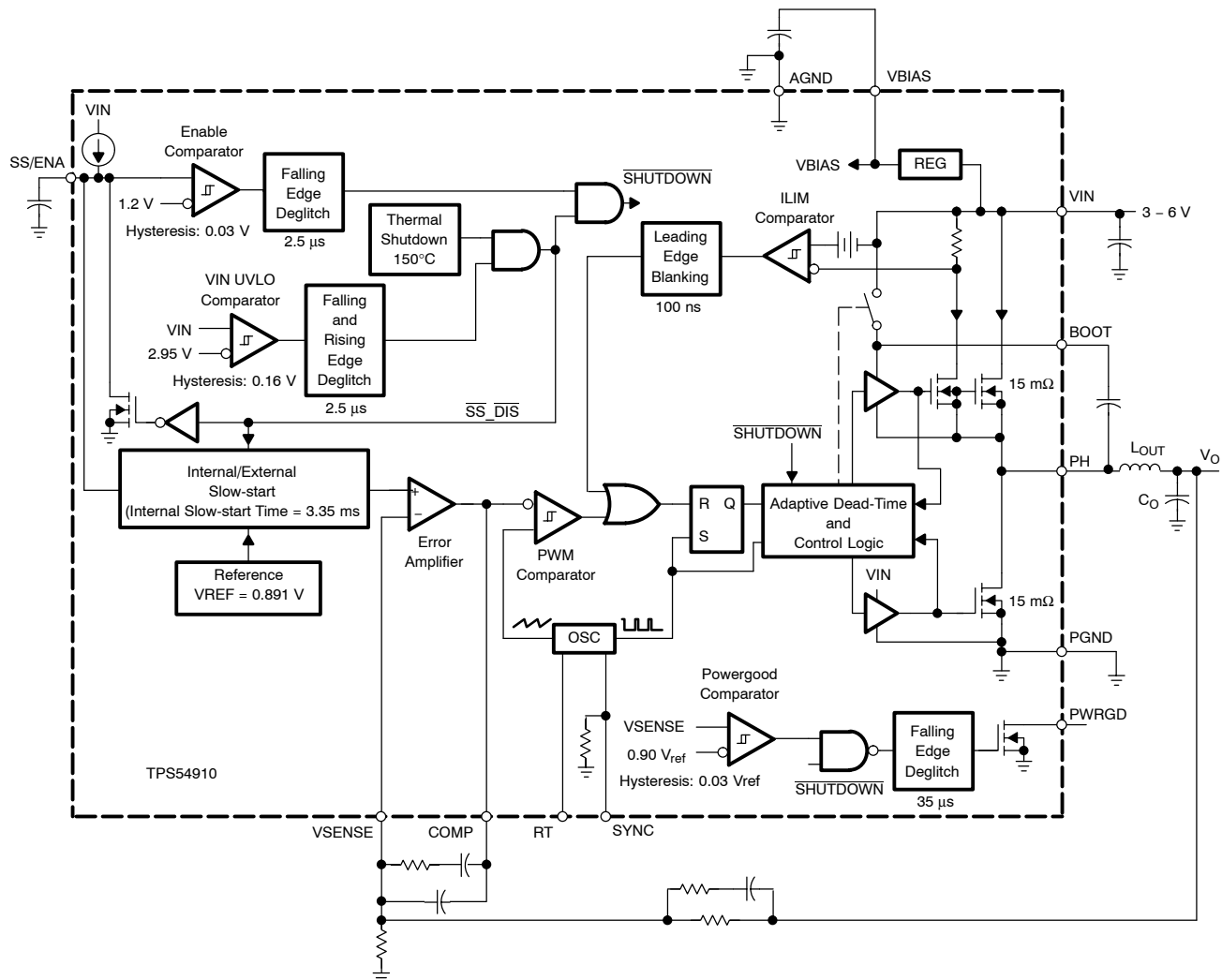
TERMINAL FUNCTIONS

TERMINAL NAME	NO.	DESCRIPTION
AGND	1	Analog ground. Return for compensation network/output divider, slow-start capacitor, VBIAS capacitor, RT resistor and SYNC pin. Connect PowerPAD to AGND.
BOOT	5	Bootstrap output. 0.022-μF to 0.1-μF low-ESR capacitor connected from BOOT to PH generates floating drive for the high-side FET driver.
COMP	3	Error amplifier output. Connect frequency compensation network from COMP to VSENSE
PGND	15–19	Power ground. High current return for the low-side driver and power MOSFET. Connect PGND with large copper areas to the input and output supply returns, and negative terminals of the input and output capacitors. A single point connection to AGND is recommended.
PH	6–14	Phase output. Junction of the internal high-side and low-side power MOSFETs, and output inductor.
PWRGD	4	Power good open drain output. High when VSENSE ≥ 90% V _{ref} , otherwise PWRGD is low. Note that output is low when SS/ENA is low or the internal shutdown signal is active.
RT	28	Frequency setting resistor input. Connect a resistor from RT to AGND to set the switching frequency, f _s .
SS/ENA	26	Slow-start/enable input/output. Dual function pin which provides logic input to enable/disable device operation and capacitor input to externally set the start-up time.
SYNC	27	Synchronization input. Dual function pin which provides logic input to synchronize to an external oscillator or pin select between two internally set switching frequencies. When used to synchronize to an external signal, a resistor must be connected to the RT pin.
VBIAS	25	Internal bias regulator output. Supplies regulated voltage to internal circuitry. Bypass VBIAS pin to AGND pin with a high-quality, low-ESR 0.1-μF to 1.0-μF ceramic capacitor.
VIN	20–24	Input supply for the power MOSFET switches and internal bias regulator. Bypass VIN pins to PGND pins close to device package with a high-quality, low-ESR 10-μF ceramic capacitor.
VSENSE	2	Error amplifier inverting input. Connect to output voltage compensation network/output divider.

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INTERNAL BLOCK DIAGRAM



RELATED DC/DC PRODUCTS

- TPS40000—dc/dc controller
- TPS56300—dc/dc controller
- PT6600 series—9 A plugin modules

TYPICAL CHARACTERISTICS

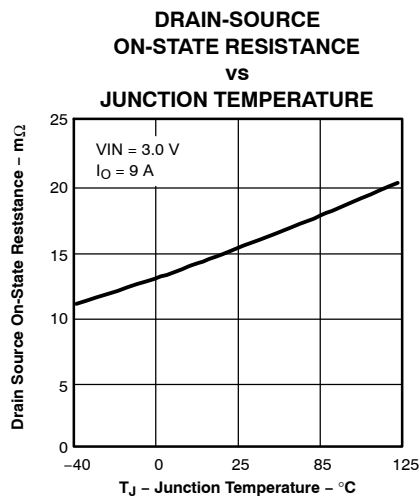


Figure 1

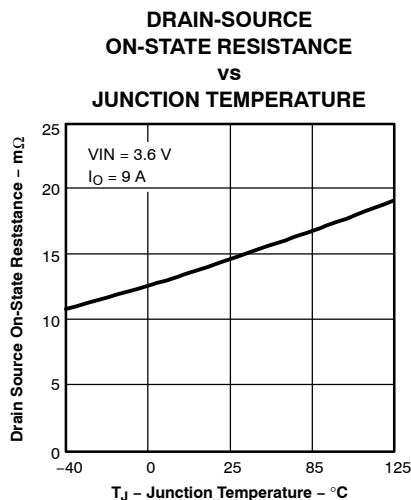


Figure 2

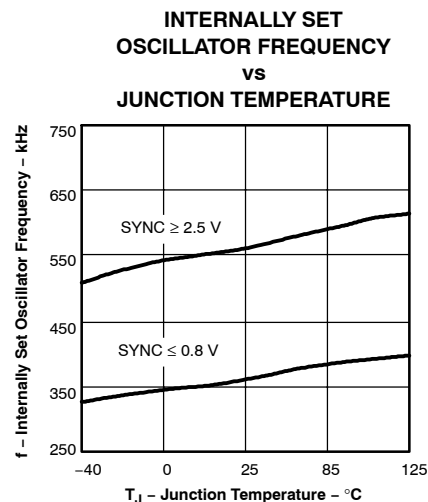


Figure 3

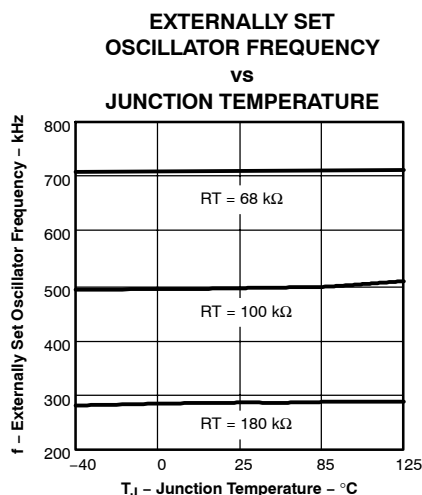


Figure 4

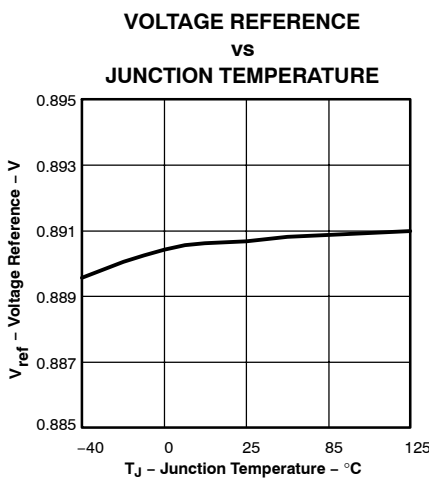


Figure 5

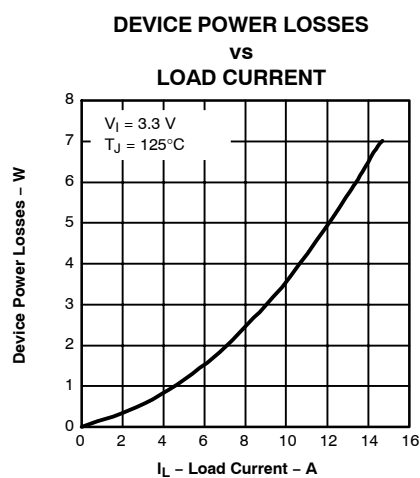


Figure 6

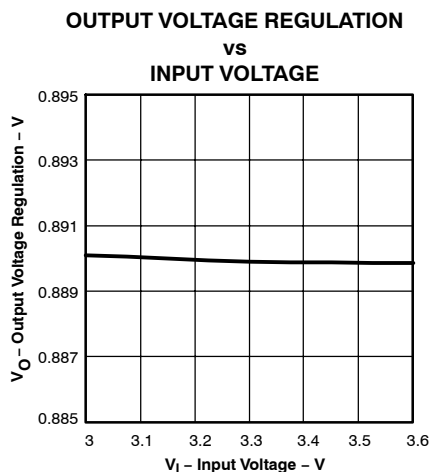


Figure 7

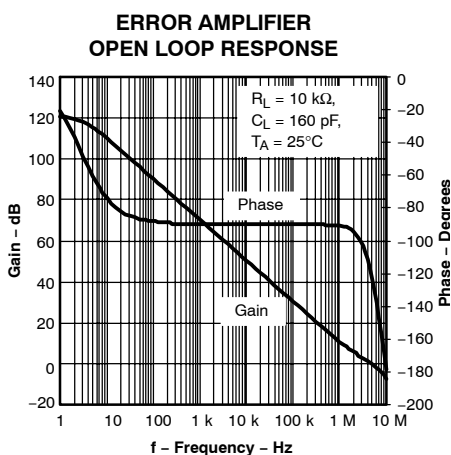


Figure 8

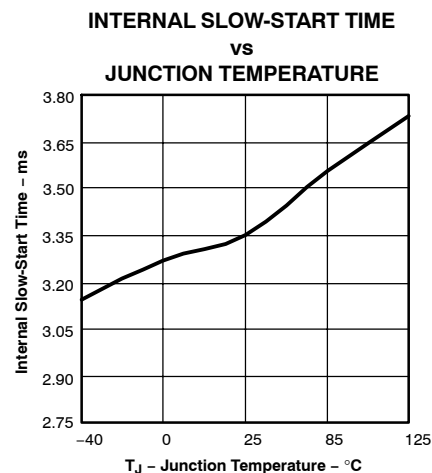


Figure 9

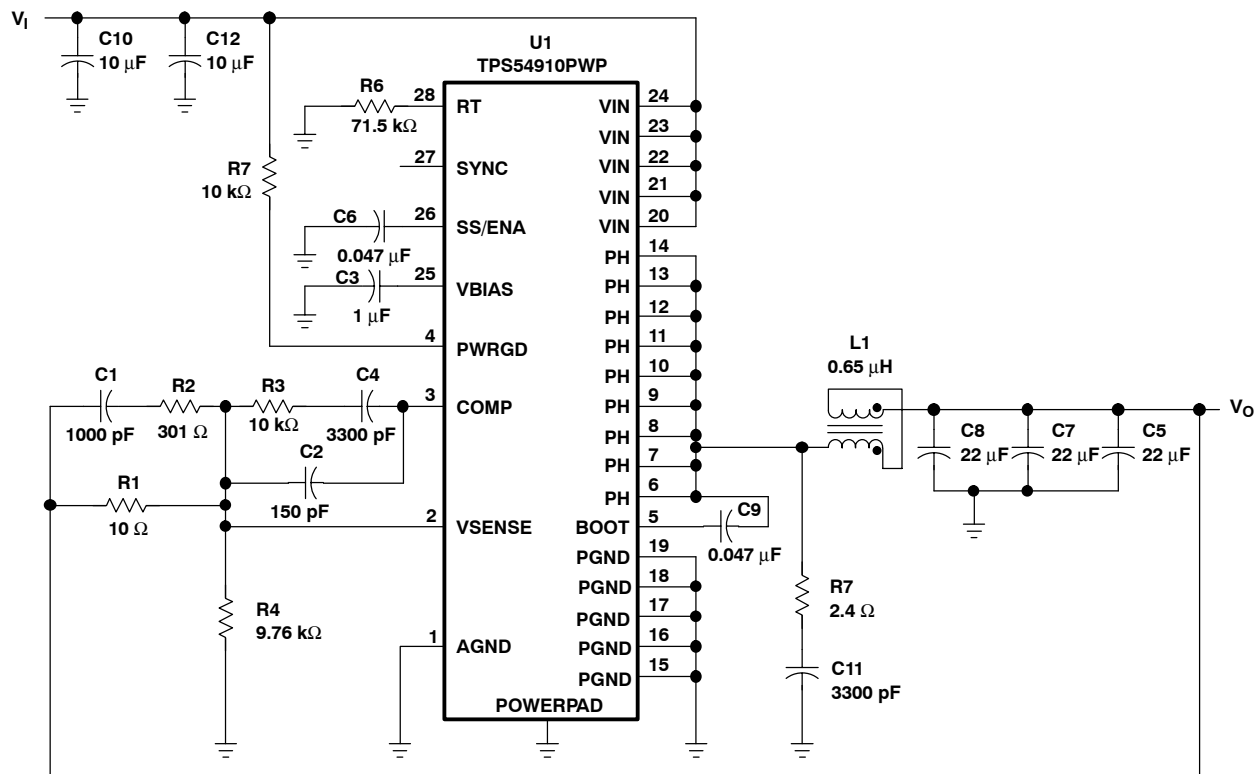
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APPLICATION INFORMATION

Figure 10 shows the schematic diagram for a typical TPS54910 application. The TPS54910 (U1) can provide up to 9 A of output current at a nominal output voltage of 1.8 V. For proper thermal performance, the exposed

thermal PowerPAD underneath the integrated circuit, TPS54910, package must be soldered to the printed-circuit board.



Analog and Power Grounds Are Tied at the Pad Under the Package of IC

Figure 10. Application Circuit

COMPONENT SELECTION

The values for the components used in this design example were selected for best load transient response and small PCB area. Additional design information is available at www.ti.com.

INPUT FILTER

The input voltage is a nominal 3.3 VDC. The input filter (C10) is a 10-μF ceramic capacitor (Taiyo Yuden). C12 is also a 10-μF ceramic capacitor (Taiyo Yuden) that provides high-frequency decoupling of the TPS54910 from the input supply. C12 must be located as close as possible to the device. Ripple current is carried in both C10 and C12, and the return path to PGND must avoid the current circulating in the output capacitors C5, C7, and C8.

FEEDBACK CIRCUIT

The values for these components are selected to provide fast transient response times.

The resistor divider network of R1 and R4 sets the output voltage for the circuit at 1.8 V. R1 along with R2, R3, C1, C2, and C4 forms the loop compensation network for the circuit. For this design, a Type-3 topology is used.

OPERATING FREQUENCY

In the application circuit, RT is grounded through a 71.5-kΩ resistor to select the operating frequency of 700 kHz. To set a different frequency, place a 68-kΩ to 180-kΩ resistor between RT (pin 28) and analog ground or leave RT floating to select the default of 350 kHz. The resistance can be approximated using the following equation:

$$R = \frac{500 \text{ kHz}}{\text{Switching Frequency}} \times 100 \text{ [k}\Omega\text{]} \quad (1)$$

OUTPUT FILTER

The output filter is composed of a 0.65- μ H inductor and 3 x 22- μ F capacitor. The inductor is a low dc-resistance (.017 Ω) type, Pulse Engineering PA0277. The capacitors used are 22- μ F, 6.3-V ceramic types with X5R dielectric. The feedback loop is compensated so that the unity gain frequency is approximately 75 kHz.

PCB LAYOUT

Figure 11 shows a generalized PCB layout guide for the TPS54910. The VIN pins should be connected together on the printed circuit board (PCB) and bypassed with a low ESR ceramic bypass capacitor. Care should be taken to minimize the loop area formed by the bypass capacitor connections, the VIN pins, and the TPS54910 ground pins. The minimum recommended bypass capacitance is 10 μ F ceramic with a X5R or X7R dielectric and the optimum placement is closest to the VIN pins and the PGND pins.

The TPS54910 has two internal grounds (analog and power). The analog ground ties to all of the noise-sensitive signals, while the power ground ties to the noisier power signals. Noise injected between the two grounds can degrade the performance of the TPS54910, particularly at higher output currents. Ground noise on an analog ground plane can also cause problems with some of the control and bias signals. For these reasons, separate analog and power ground traces are recommended. There should be an area of ground on the top layer directly under the IC, with an exposed area for connection to the PowerPAD. Use vias to connect this ground area to any internal ground planes. Use additional vias at the ground side of the input and output filter capacitors as well. The AGND and PGND pins should be tied to the PCB ground by connecting them

to the ground area under the device as shown. The only components that should tie directly to the power ground plane are the input capacitors, the output capacitors, the input voltage decoupling capacitor, and the PGND pins of the TPS54910. Use a separate wide trace for the analog ground signal path. This analog ground should be used for the voltage set point divider, timing resistor RT, slow start capacitor, and bias capacitor grounds. Connect this trace directly to AGND (Pin 1).

The PH pins should be tied together and routed to the output inductor. Since the PH connection is the switching node, the inductor should be located very close to the PH pins and the area of the PCB conductor minimized to prevent excessive capacitive coupling.

Connect the boot capacitor between the phase node and the BOOT pin as shown. Keep the boot capacitor close to the IC and minimize the conductor trace lengths.

Connect the output filter capacitor(s) as shown between the VOUT trace and PGND. It is important to keep the loop formed by the PH pins, Lout, Cout and PGND as small as practical.

Place the compensation components from the VOUT trace to the VSENSE and COMP pins. Do not place these components too close to the PH trace. Due to the size of the IC package and the device pinout, the components will have to be routed somewhat close, but maintain as much separation as possible while still keeping the layout compact.

Connect the bias capacitor from the VBIAS pin to analog ground using the isolated analog ground trace. If a slow-start capacitor or RT resistor is used, or if the SYNC pin is used to select 350 kHz operating frequency, connect them to this trace as well.

Figure 11. TPS54910 PCB Layout

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PERFORMANCE GRAPHS

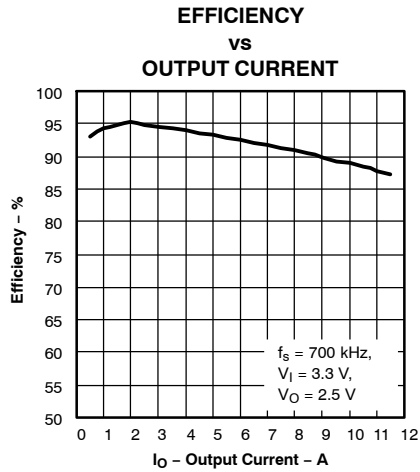


Figure 13

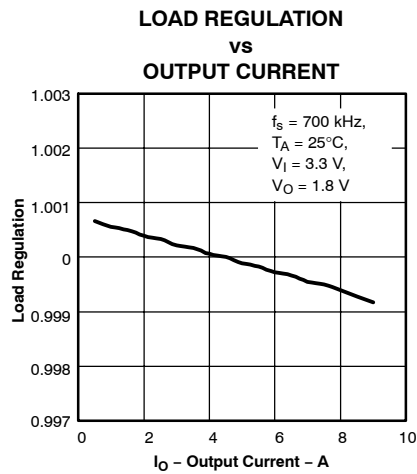


Figure 14

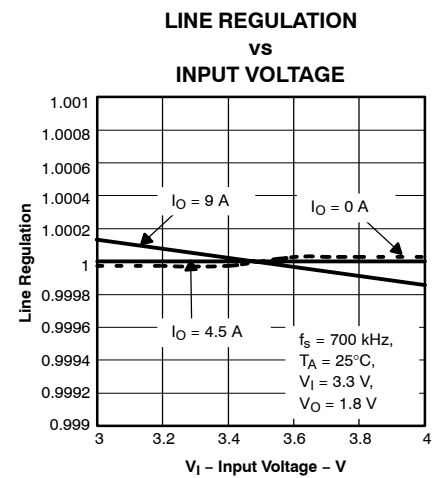


Figure 15

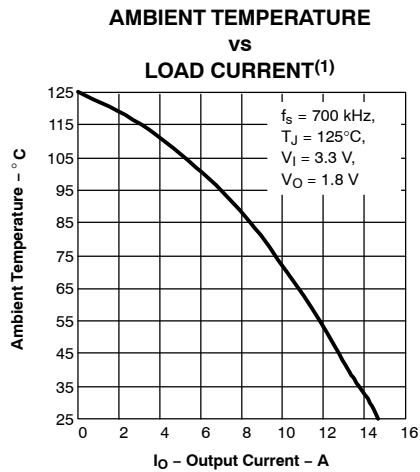


Figure 16

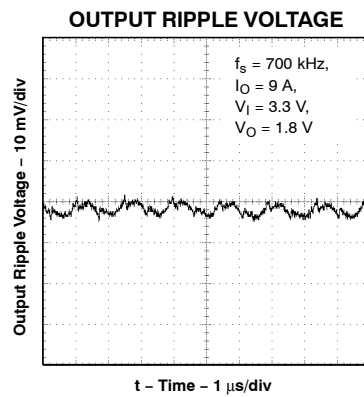


Figure 17

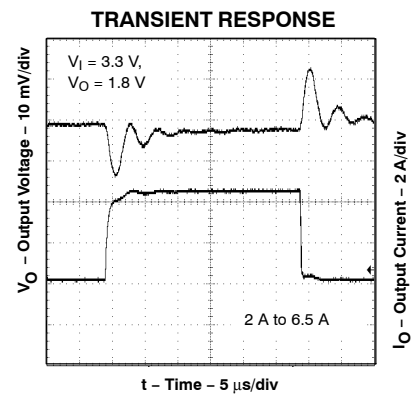


Figure 18

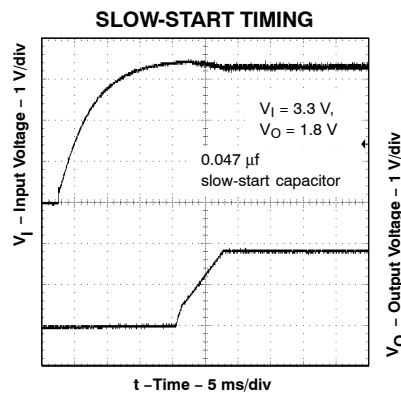


Figure 19

⁽¹⁾ Safe operating area is applicable to the test board conditions in the Dissipation Ratings

DETAILED DESCRIPTION

UNDERVOLTAGE LOCK OUT (UVLO)

The TPS54910 incorporates an under voltage lockout circuit to keep the device disabled when the input voltage (VIN) is insufficient. During power up, internal circuits are held inactive until VIN exceeds the nominal UVLO threshold voltage of 2.95 V. Once the UVLO start threshold is reached, device start-up begins. The device operates until VIN falls below the nominal UVLO stop threshold of 2.8 V. Hysteresis in the UVLO comparator, and a 2.5-μs rising and falling edge deglitch circuit reduce the likelihood of shutting the device down due to noise on VIN.

SLOW-START/ENABLE (SS/ENA)

The slow-start/enable pin provides two functions. First, the pin acts as an enable (shutdown) control by keeping the device turned off until the voltage exceeds the start threshold voltage of approximately 1.2 V. When SS/ENA exceeds the enable threshold, device start-up begins. The reference voltage fed to the error amplifier is linearly ramped up from 0 V to 0.891 V in 3.35 ms. Similarly, the converter output voltage reaches regulation in approximately 3.35 ms. Voltage hysteresis and a 2.5-μs falling edge deglitch circuit reduce the likelihood of triggering the enable due to noise.

The second function of the SS/ENA pin provides an external means of extending the slow-start time with a low-value capacitor connected between SS/ENA and AGND.

Adding a capacitor to the SS/ENA pin has two effects on start-up. First, a delay occurs between release of the SS/ENA pin and start-up of the output. The delay is proportional to the slow-start capacitor value and lasts until the SS/ENA pin reaches the enable threshold. The start-up delay is approximately:

$$t_d = C_{(SS)} \times \frac{1.2 \text{ V}}{5 \text{ } \mu\text{A}} \quad (2)$$

Second, as the output becomes active, a brief ramp-up at the internal slow-start rate may be observed before the externally set slow-start rate takes control and the output rises at a rate proportional to the slow-start capacitor. The slow-start time set by the capacitor is approximately:

$$t_{(SS)} = C_{(SS)} \times \frac{0.7 \text{ V}}{5 \text{ } \mu\text{A}} \quad (3)$$

The actual slow-start time is likely to be less than the above approximation due to the brief ramp-up at the internal rate.

VBIAS REGULATOR (VBIAS)

The VBIAS regulator provides internal analog and digital blocks with a stable supply voltage over variations in junction temperature and input voltage. A high quality, low-ESR, ceramic bypass capacitor is required on the VBIAS pin. X7R or X5R grade dielectrics are recommended because their values are more stable over temperature. The bypass capacitor must be placed close to the VBIAS pin and returned to AGND.

External loading on VBIAS is allowed, with the caution that internal circuits require a minimum VBIAS of 2.70 V, and external loads on VBIAS with ac or digital switching noise may degrade performance. The VBIAS pin may be useful as a reference voltage for external circuits.

VOLTAGE REFERENCE

The voltage reference system produces a precise V_{ref} signal by scaling the output of a temperature stable bandgap circuit. During manufacture, the bandgap and scaling circuits are trimmed to produce 0.891 V at the output of the error amplifier, with the amplifier connected as a voltage follower. The trim procedure adds to the high precision regulation of the TPS54910, since it cancels offset errors in the scale and error amplifier circuits.

OSCILLATOR AND PWM RAMP

The oscillator frequency can be set to internally fixed values of 350 kHz or 550 kHz using the SYNC pin as a static digital input. If a different frequency of operation is required for the application, the oscillator frequency can be externally adjusted from 280 to 700 kHz by connecting a resistor between the RT pin to ground and floating the SYNC pin. The switching frequency is approximated by the following equation, where R is the resistance from RT to AGND:

$$\text{Switching Frequency} = \frac{100 \text{ k}\Omega}{R} \times 500 \text{ [kHz]} \quad (4)$$

External synchronization of the PWM ramp is possible over the frequency range of 330 kHz to 700 kHz by driving a synchronization signal into SYNC and connecting a resistor from RT to AGND. Choose a RT resistor that sets the free running frequency to 80% of the synchronization signal. The following table summarizes the frequency selection configurations:

SWITCHING FREQUENCY	SYNC PIN	RT PIN
350 kHz, internally set	Float or AGND	Float
550 kHz, internally set	$\geq 2.5 \text{ V}$	Float
Externally set 280 kHz to 700 kHz	Float	$R = 68 \text{ k}\Omega$ to $180 \text{ k}\Omega$
Externally synchronized frequency	Synchronization signal	$R = \text{RT value for 80\%}$ of external synchro- nization frequency

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SLVS421C – MARCH 2002 – REVISED FEBRUARY 2005

ERROR AMPLIFIER

The high performance, wide bandwidth, voltage error amplifier sets the TPS54910 apart from most dc/dc converters. The user is given the flexibility to use a wide range of output L and C filter components to suit the particular application needs. Type-2 or Type-3 compensation can be employed using external compensation components.

PWM CONTROL

Signals from the error amplifier output, oscillator, and current limit circuit are processed by the PWM control logic. Referring to the internal block diagram, the control logic includes the PWM comparator, OR gate, PWM latch, and portions of the adaptive dead-time and control-logic block. During steady-state operation below the current limit threshold, the PWM comparator output and oscillator pulse train alternately reset and set the PWM latch. Once the PWM latch is set, the low-side FET remains on for a minimum duration set by the oscillator pulse width. During this period, the PWM ramp discharges rapidly to its valley voltage. When the ramp begins to charge back up, the low-side FET turns off and high-side FET turns on. As the PWM ramp voltage exceeds the error amplifier output voltage, the PWM comparator resets the latch, thus turning off the high-side FET and turning on the low-side FET. The low-side FET remains on until the next oscillator pulse discharges the PWM ramp.

During transient conditions, the error amplifier output could be below the PWM ramp valley voltage or above the PWM peak voltage. If the error amplifier is high, the PWM latch is never reset, and the high-side FET remains on until the oscillator pulse signals the control logic to turn the high-side FET off and the low-side FET on. The device operates at its maximum duty cycle until the output voltage rises to the regulation set-point, setting VSENSE to approximately the same voltage as VREF. If the error amplifier output is low, the PWM latch is continually reset and the high-side FET does not turn on. The low-side FET remains on until the VSENSE voltage decreases to a range that allows the PWM comparator to change states. The TPS54910 is capable of sinking current continuously until the output reaches the regulation set-point.

If the current limit comparator trips for longer than 100 ns, the PWM latch resets before the PWM ramp exceeds the error amplifier output. The high-side FET turns off and low-side FET turns on to decrease the energy in the output inductor and consequently the output current. This process is repeated each cycle in which the current limit comparator is tripped.

DEAD-TIME CONTROL AND MOSFET DRIVERS

Adaptive dead-time control prevents shoot-through current from flowing in both N-channel power MOSFETs

during the switching transitions by actively controlling the turnon times of the MOSFET drivers. The high-side driver does not turn on until the voltage at the gate of the low-side FET is below 2 V. While the low-side driver does not turn on until the voltage at the gate of the high-side MOSFET is below 2 V.

The high-side and low-side drivers are designed with 300-mA source and sink capability to quickly drive the power MOSFETs gates. The low-side driver is supplied from VIN, while the high-side drive is supplied from the BOOT pin. A bootstrap circuit uses an external BOOT capacitor and an internal 2.5-Ω bootstrap switch connected between the VIN and BOOT pins. The integrated bootstrap switch improves drive efficiency and reduces external component count.

OVERCURRENT PROTECTION

The cycle-by-cycle current limiting is achieved by sensing the current flowing through the high-side MOSFET and comparing this signal to a preset overcurrent threshold. The high side MOSFET is turned off within 200 ns of reaching the current limit threshold. A 100-ns leading edge blanking circuit prevents current limit false tripping. Current limit detection occurs only when current flows from VIN to PH when sourcing current to the output filter. Load protection during current sink operation is provided by thermal shutdown.

THERMAL SHUTDOWN

The device uses the thermal shutdown to turn off the power MOSFETs and disable the controller if the junction temperature exceeds 150°C. The device is released from shutdown automatically when the junction temperature decreases to 10°C below the thermal shutdown trip point, and starts up under control of the slow-start circuit.

Thermal shutdown provides protection when an overload condition is sustained for several milliseconds. With a persistent fault condition, the device cycles continuously; starting up by control of the soft-start circuit, heating up due to the fault condition, and then shutting down upon reaching the thermal shutdown trip point. This sequence repeats until the fault condition is removed.

POWER-GOOD (PWRGD)

The power good circuit monitors for under voltage conditions on VSENSE. If the voltage on VSENSE is 10% below the reference voltage, the open-drain PWRGD output is pulled low. PWRGD is also pulled low if VIN is less than the UVLO threshold or SS/ENA is low. When VIN ≥ UVLO threshold, SS/ENA ≥ enable threshold, and VSENSE > 90% of V_{ref}, the open drain output of the PWRGD pin is high. A hysteresis voltage equal to 3% of V_{ref} and a 35 μs falling edge deglitch circuit prevent tripping of the power good comparator due to high frequency noise.

PACKAGING INFORMATION

Orderable part number	Status (1)	Material type (2)	Package Pins	Package qty Carrier	RoHS (3)	Lead finish/ Ball material (4)	MSL rating/ Peak reflow (5)	Op temp (°C)	Part marking (6)
TPS54910PWP	Obsolete	Production	HTSSOP (PWP) 28	-	-	Call TI	Call TI	-40 to 85	TPS54910
TPS54910PWPR	Active	Production	HTSSOP (PWP) 28	2000 LARGE T&R	Yes	NIPDAU NIPDAU	Level-2-260C-1 YEAR	-40 to 85	TPS54910
TPS54910PWPRG4	Active	Production	HTSSOP (PWP) 28	2000 LARGE T&R	Yes	NIPDAU	Level-2-260C-1 YEAR	-40 to 85	TPS54910

⁽¹⁾ **Status:** For more details on status, see our [product life cycle](#).

⁽²⁾ **Material type:** When designated, preproduction parts are prototypes/experimental devices, and are not yet approved or released for full production. Testing and final process, including without limitation quality assurance, reliability performance testing, and/or process qualification, may not yet be complete, and this item is subject to further changes or possible discontinuation. If available for ordering, purchases will be subject to an additional waiver at checkout, and are intended for early internal evaluation purposes only. These items are sold without warranties of any kind.

⁽³⁾ **RoHS values:** Yes, No, RoHS Exempt. See the [TI RoHS Statement](#) for additional information and value definition.

⁽⁴⁾ **Lead finish/Ball material:** Parts may have multiple material finish options. Finish options are separated by a vertical ruled line. Lead finish/Ball material values may wrap to two lines if the finish value exceeds the maximum column width.

⁽⁵⁾ **MSL rating/Peak reflow:** The moisture sensitivity level ratings and peak solder (reflow) temperatures. In the event that a part has multiple moisture sensitivity ratings, only the lowest level per JEDEC standards is shown. Refer to the shipping label for the actual reflow temperature that will be used to mount the part to the printed circuit board.

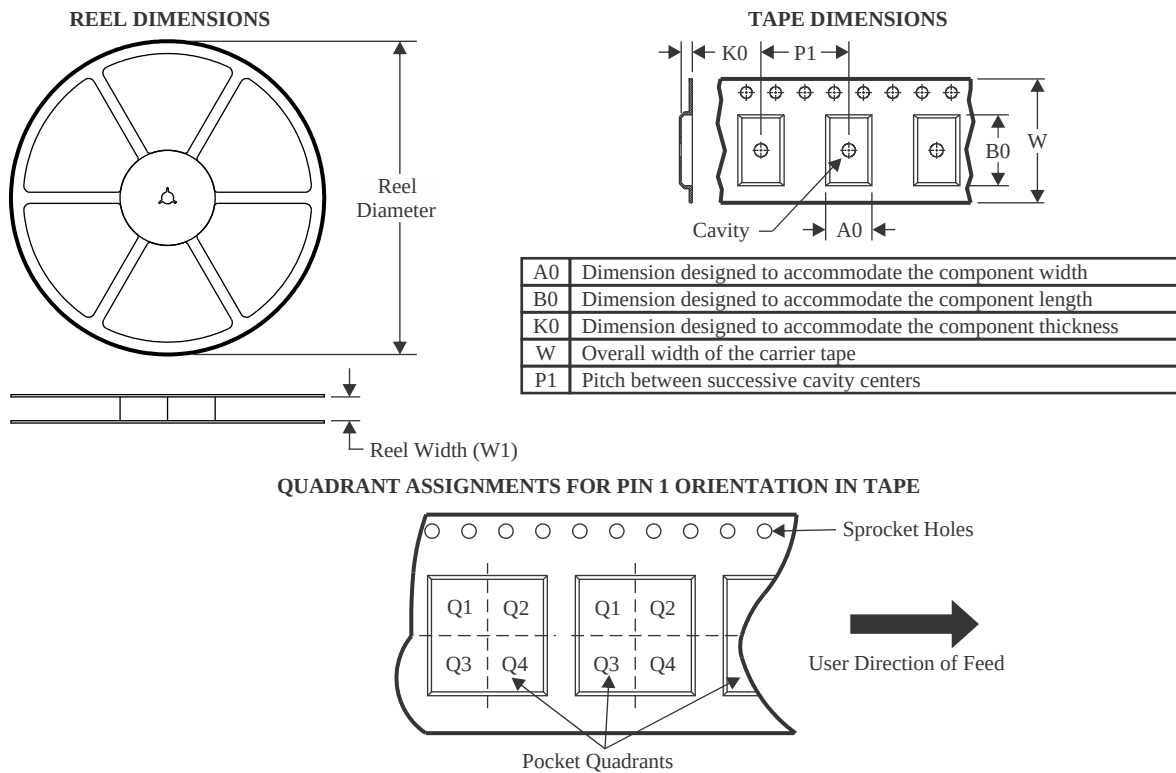
⁽⁶⁾ **Part marking:** There may be an additional marking, which relates to the logo, the lot trace code information, or the environmental category of the part.

Multiple part markings will be inside parentheses. Only one part marking contained in parentheses and separated by a "-" will appear on a part. If a line is indented then it is a continuation of the previous line and the two combined represent the entire part marking for that device.

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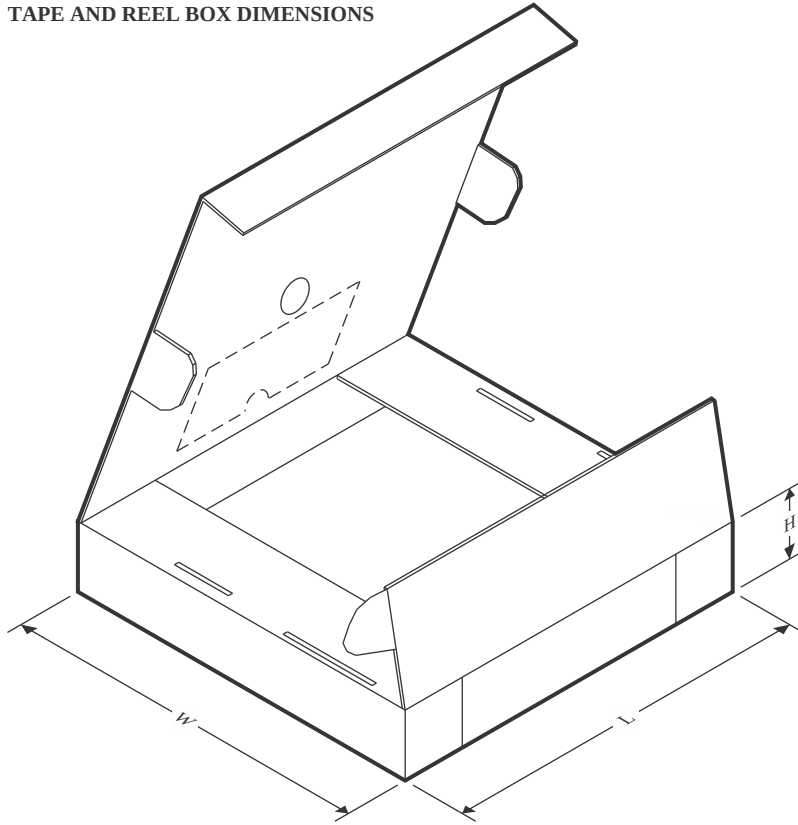
TAPE AND REEL INFORMATION



*All dimensions are nominal

Device	Package Type	Package Drawing	Pins	SPQ	Reel Diameter (mm)	Reel Width W1 (mm)	A0 (mm)	B0 (mm)	K0 (mm)	P1 (mm)	W (mm)	Pin1 Quadrant
TPS54910PWPR	HTSSOP	PWP	28	2000	330.0	16.4	6.9	10.2	1.8	12.0	16.0	Q1
TPS54910PWPR	HTSSOP	PWP	28	2000	330.0	16.4	6.9	10.2	1.8	12.0	16.0	Q1

TAPE AND REEL BOX DIMENSIONS



*All dimensions are nominal

Device	Package Type	Package Drawing	Pins	SPQ	Length (mm)	Width (mm)	Height (mm)
TPS54910PWPR	HTSSOP	PWP	28	2000	356.0	356.0	35.0
TPS54910PWPR	HTSSOP	PWP	28	2000	350.0	350.0	43.0

GENERIC PACKAGE VIEW

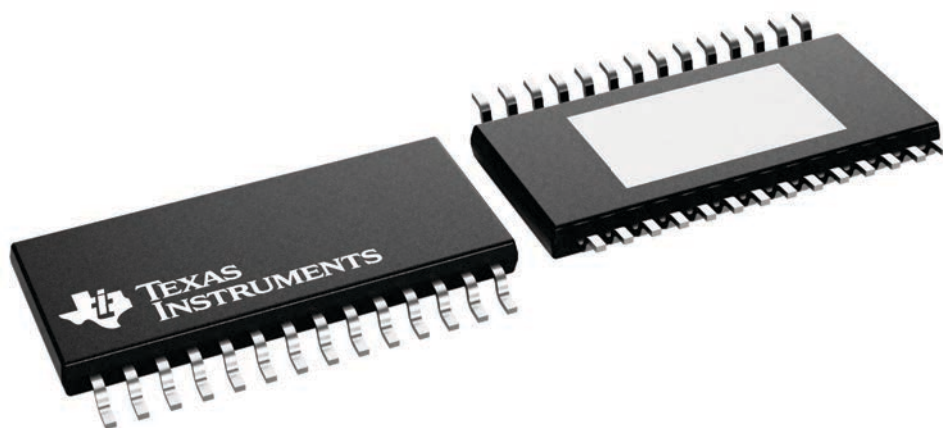
PWP 28

PowerPAD™ TSSOP - 1.2 mm max height

4.4 x 9.7, 0.65 mm pitch

SMALL OUTLINE PACKAGE

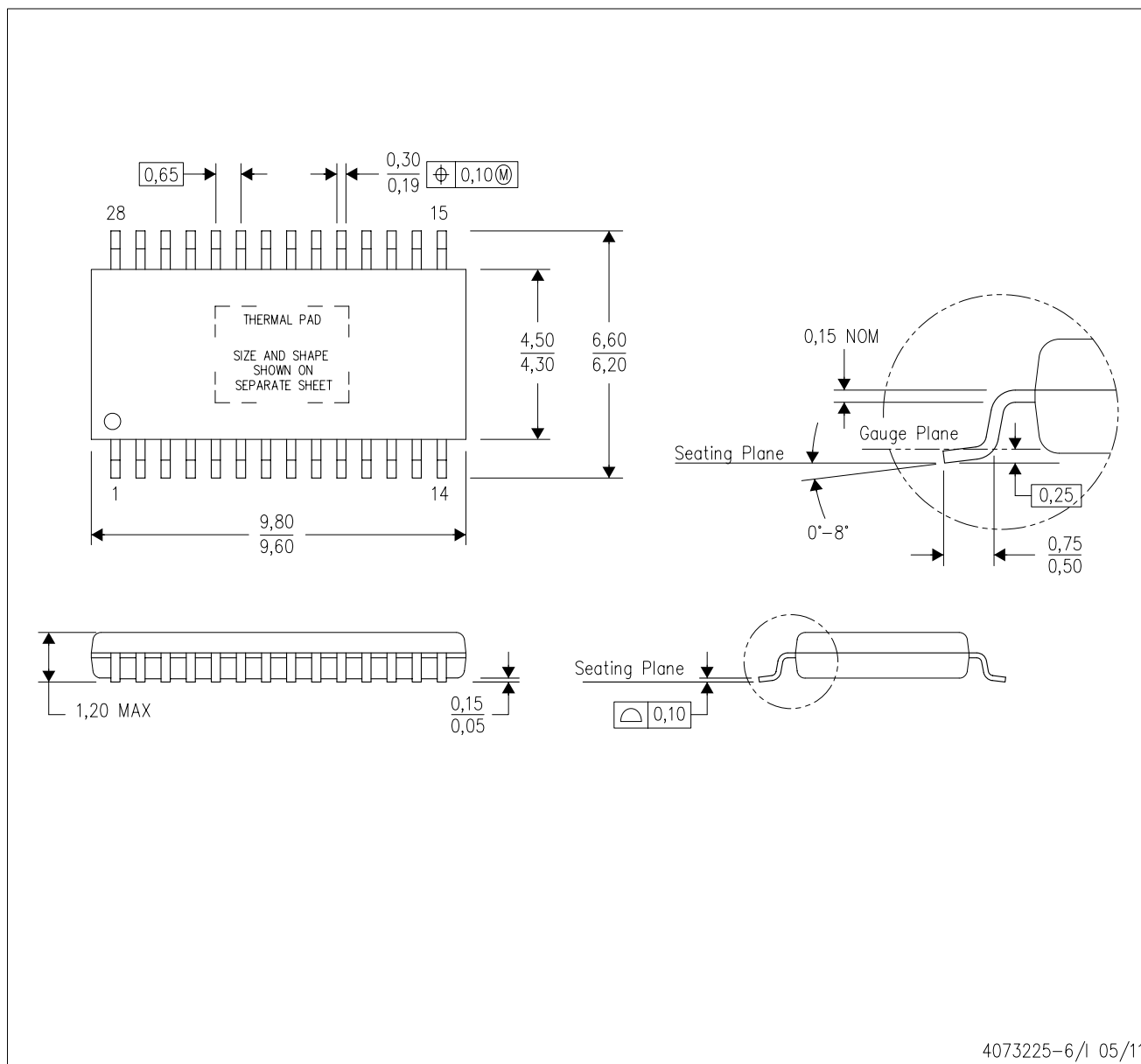
This image is a representation of the package family, actual package may vary.
Refer to the product data sheet for package details.



4224765/B

PWP (R-PDSO-G28)

PowerPAD™ PLASTIC SMALL OUTLINE



- NOTES:
- A. All linear dimensions are in millimeters.
 - B. This drawing is subject to change without notice.
 - C. Body dimensions do not include mold flash or protrusions. Mold flash and protrusion shall not exceed 0.15 per side.
 - D. This package is designed to be soldered to a thermal pad on the board. Refer to Technical Brief, PowerPad Thermally Enhanced Package, Texas Instruments Literature No. SLMA002 for information regarding recommended board layout. This document is available at www.ti.com <<http://www.ti.com>>.
 - E. See the additional figure in the Product Data Sheet for details regarding the exposed thermal pad features and dimensions.
 - E. Falls within JEDEC MO-153

PowerPAD is a trademark of Texas Instruments.

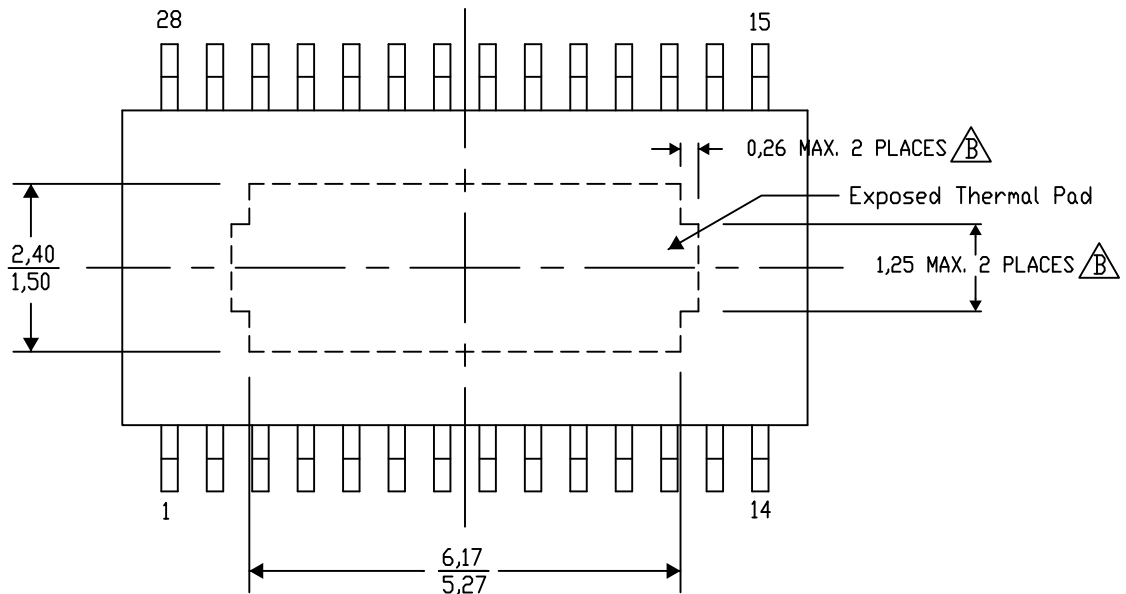
PWP (R-PDSO-G28) PowerPAD™ SMALL PLASTIC OUTLINE

THERMAL INFORMATION

This PowerPAD™ package incorporates an exposed thermal pad that is designed to be attached to a printed circuit board (PCB). The thermal pad must be soldered directly to the PCB. After soldering, the PCB can be used as a heatsink. In addition, through the use of thermal vias, the thermal pad can be attached directly to the appropriate copper plane shown in the electrical schematic for the device, or alternatively, can be attached to a special heatsink structure designed into the PCB. This design optimizes the heat transfer from the integrated circuit (IC).

For additional information on the PowerPAD package and how to take advantage of its heat dissipating abilities, refer to Technical Brief, PowerPAD Thermally Enhanced Package, Texas Instruments Literature No. SLMA002 and Application Brief, PowerPAD Made Easy, Texas Instruments Literature No. SLMA004. Both documents are available at www.ti.com.

The exposed thermal pad dimensions for this package are shown in the following illustration.



4206332-33/AO 01/16

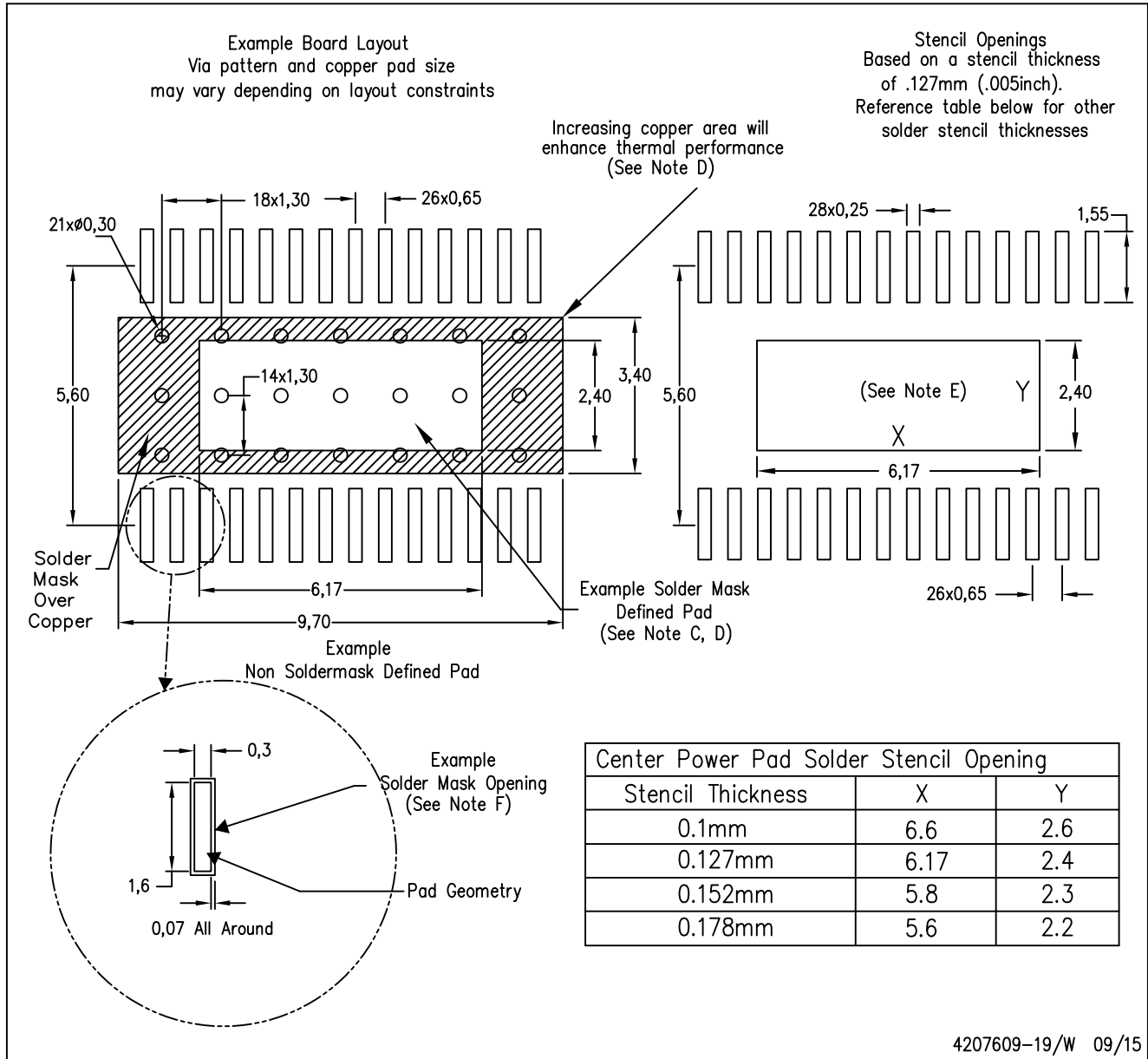
NOTE: A. All linear dimensions are in millimeters

B. Exposed tie strap features may not be present.

PowerPAD is a trademark of Texas Instruments

PWP (R-PDSO-G28)

PowerPAD™ PLASTIC SMALL OUTLINE



NOTES:

- All linear dimensions are in millimeters.
- This drawing is subject to change without notice.
- Customers should place a note on the circuit board fabrication drawing not to alter the center solder mask defined pad.
- This package is designed to be soldered to a thermal pad on the board. Refer to Technical Brief, PowerPad Thermally Enhanced Package, Texas Instruments Literature No. SLMA002, SLMA004, and also the Product Data Sheets.
- For specific thermal information, via requirements, and recommended board layout. These documents are available at www.ti.com <<http://www.ti.com>>. Publication IPC-7351 is recommended for alternate designs. Laser cutting apertures with trapezoidal walls and also rounding corners will offer better paste release. Customers should contact their board assembly site for stencil design recommendations. Example stencil design based on a 50% volumetric metal load solder paste. Refer to IPC-7525 for other stencil design.
- Customers should contact their board fabrication site for solder mask tolerances between and around signal pads.

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